

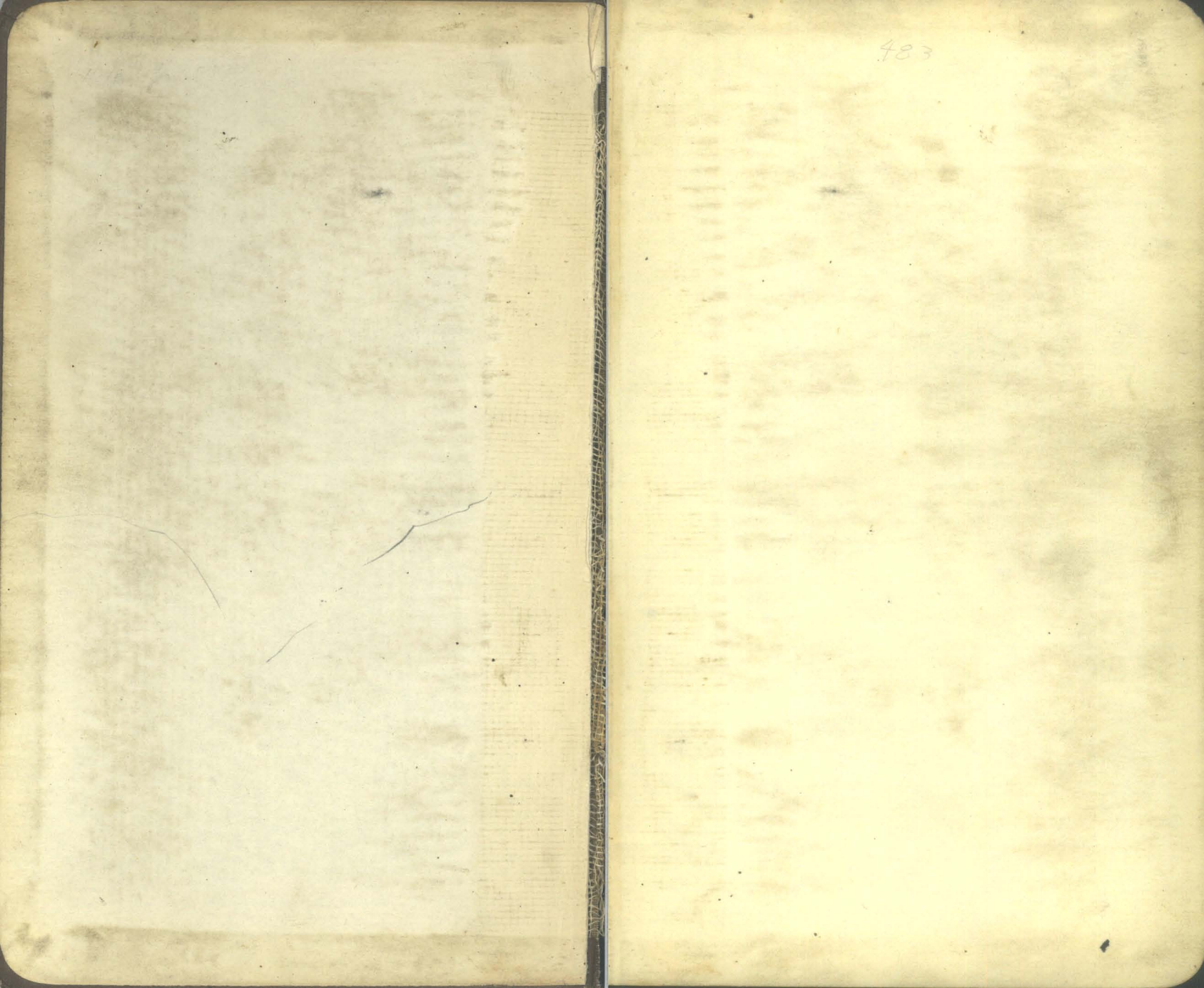
OIL DENSITY
PROCTOR DENSITY

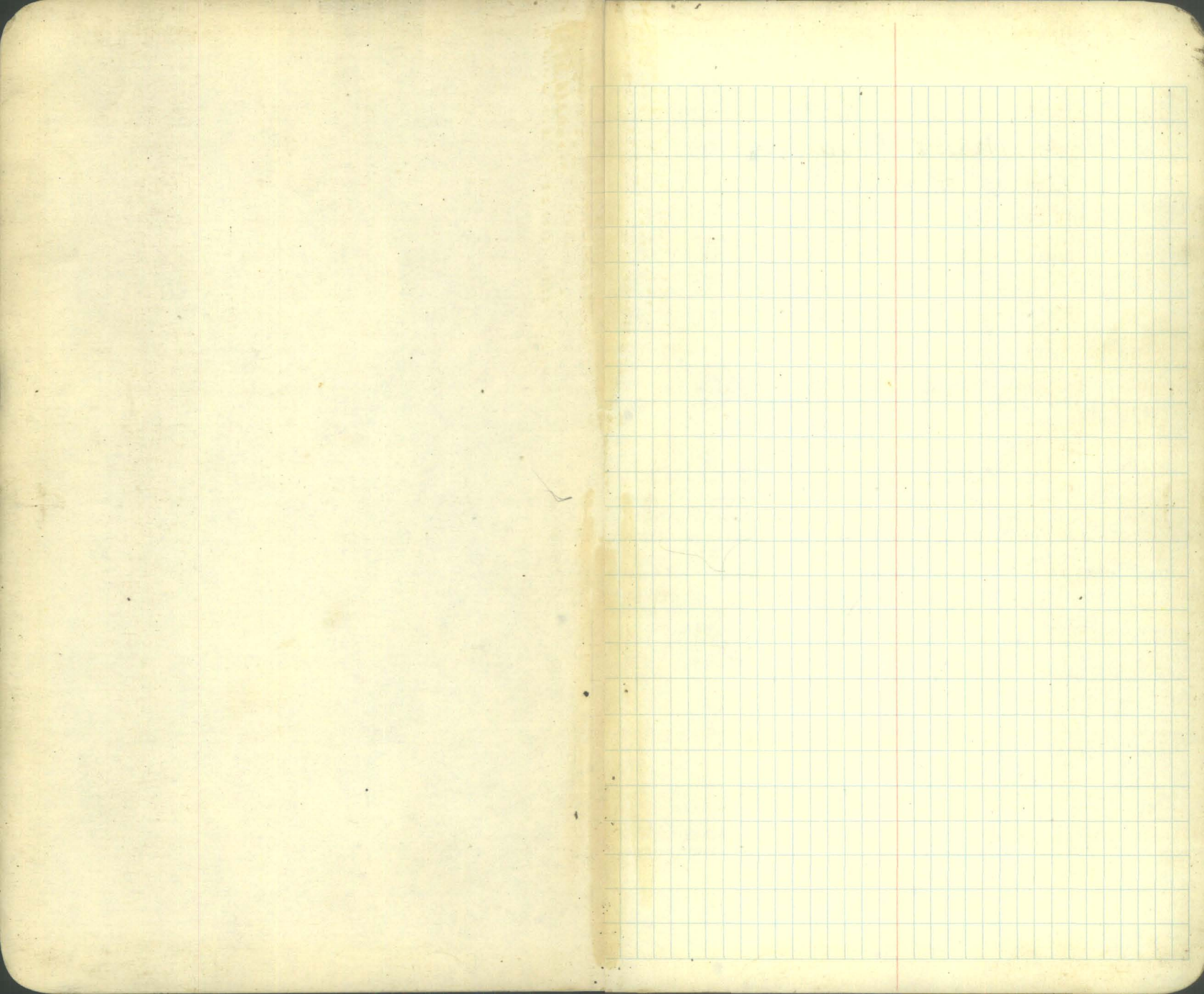
1958-59

CO. ROAD A & H & X

Oil Density 1958-59
Proctor Density
Co. Rd. "A" + H + X

1220





Co. Rd. "H" U.S. 63 E. 6 miles
Co. Rd "A" U.S. 13 E. To Eagle Center
Co. Rd "L"

N.A.T.X. 9647

July 9, 1958

Copy. 9950 Gal.
M.C. 4 9414 Gal. @ 60°

Length = 32-1'

Diam. = 7-3' = 87

Zo = 23½"

C = .6'

Temp. = 126°

N.A.T.X. 9590

Copy. 9978 Gal. M.C. - 4 9373 Gal. @ 60°

Length 32.4'

Diam. 7-5" = 89"

Zo 7½" @ 60° - 9299 Gal.

C .6'

Temp. 125°

N.A.T.X. 9737

Copy. 9737 M.C. - 0 9649 Gal @ 60°

Length. 30.4'

Diam. 20" @ 60° - 9596 Gals

Zo = 3¼"

C .45'

Temp. 88°

Taken from job
550 Gal. @ 100°

N.A.T.X.	1546	9776	Copy 10144	M.C.O
L'	26'			
D.	8'	oil 7.62'		
Zo	3 3/4"			
C				
Temp	98°			

N.A.T.X	4023	9853	Copy 10223	M.C.-O
Length	26'			
Diam	8'	oil 7.75		
Zo	3 7/8"			
C				
Temp.	102°			

N.A.T.X	9688	9416	Copy 9930	M.C.-4
Length	33'			
Diam.	7'-3"	oil		
Zo	2 7/8"	6'-11 1/2"		
C				
Temp	197°			

N.A.T.X 9590 9408 Copy. 9978 M.C-4
 Length 23.75'
 Diam. 7'-3"
 Zo 5 1/4" 6'-9"
 Temp 196°

N.A.T.X. 9086 Copy. 8012 M.C-4
 Length 32'-1"
 Diam. 6'-2" = 74"
 Zo 3 1/4"
 Temp. 144°

N.A.T.X. 9694 Copy. 7933
 Length 32.66
 Diam. 783
 Zo 64'
 Temp. 136°

3

32.75
 3.52
 6550
 14075
 98351
 1150800

8012

115

11.

7897

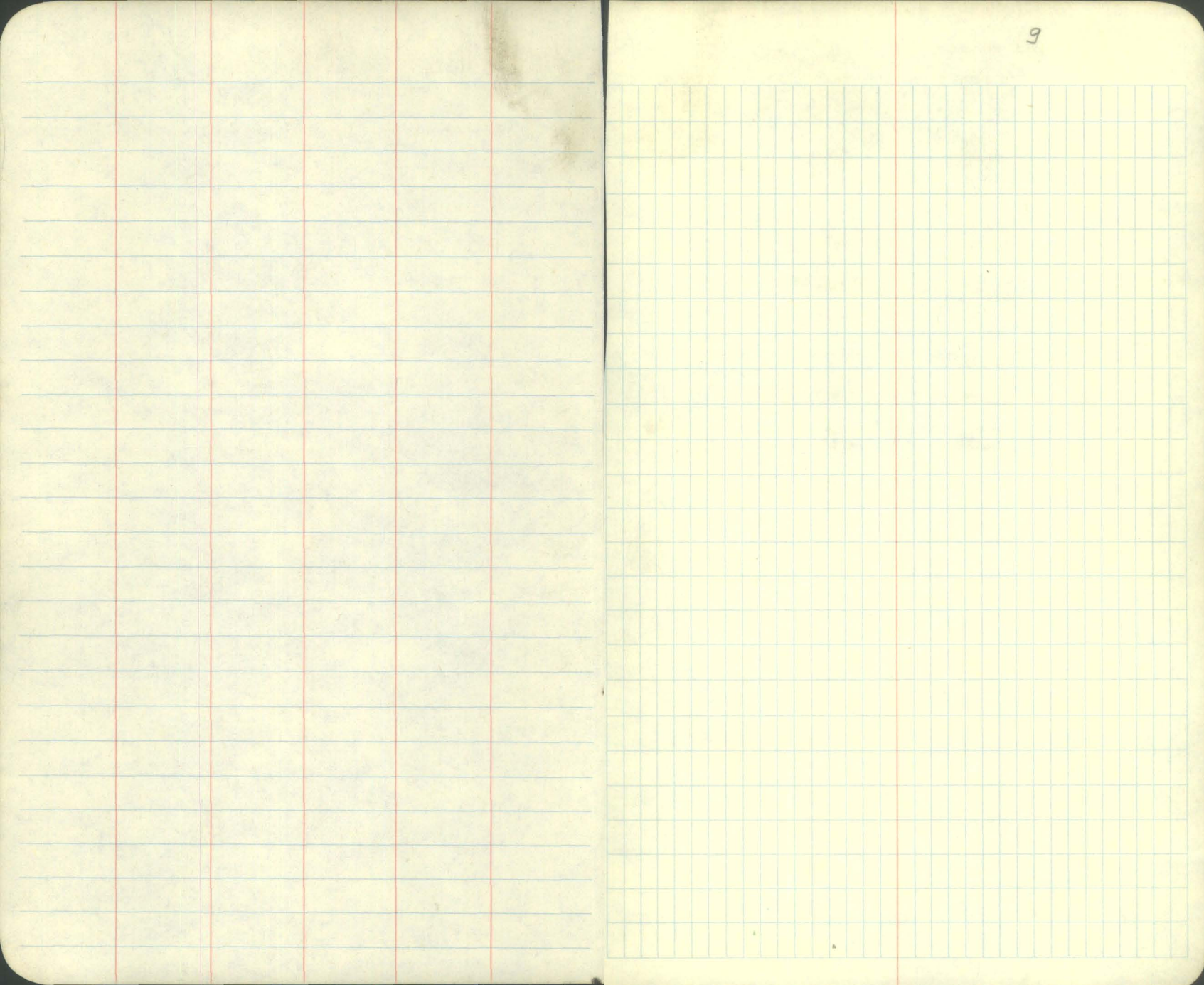
.971

7897

55279

78083

7,668981



Sta.	250+99		250+99			
Test No.	1	2	1	2	3	4
Wt. of sample						
H ₂ O Added	310	50	250	30	30	40
Wet wt. of spec.	2108	2088	2025	2060	2081	
Par. No.	1	2	1	2	3	4
Wet wt. of Par. Sample	629	647	629	846	833	
Dry wt. of Par. Sample	577	590	600	768	753	
Wt. of Par. Dry	129	147	129	147	150	
Wt. of Sample Moisture	448	443	471	621	603	
Loss	52	57	29	78	80	
% Moisture	11.6	12.9	6.2	10.	10.6	
Calc. Dry wt.	1889	1849	1907	1873	1885	
Wt. of 2b						
Per Cu. Ft.	124.8	122.2	126.0	123.6	124.6	
Wet wt. 2b						
Per Cu. Ft.	139.3	132.0	133.8			
Proctor Density						
75% of						

251+00

1	2	3	4	5	6
2445	2445	2445	2445	2445	2445
120	169	218	267	316	365
1856	1938	1958	2070	2109	2073

04.9%	06.9	08.9	10.9	12.9	14.9
1769	1813	1798	1867	1868	1804
116.9	119.8	118.8	123.4	124.6	119.2
122.64	128.1	129.4	136.8	139.4	137.0

277+63

2898

552+00

1

2-2

3

1

2

3

4

2850

2850

2850

2489

278

338

398

174

⁵⁰
224⁵⁰
274⁵⁰
324

2059

2132

2120

2120

1927

2068

2118

2138

9.8

11.9

14.0

77.

97.

117.

137.

1845

1905

1860

1801

1897

1908

1892

123.9

125.9

122.9

119.0

125.4

126.1

125.0

136.1

140.9

140.1

1.99

2.02

1.97

1.91

2.01

2.02

2.00

1.92

11.7%

62.4

305+00

1	2	3	4
2564	2564	2564	2564
205	⁵¹ 256	⁵² 308	⁵² 360
2000	2086	2125	2100

8%	10%	12%	14%
1852	1896	1897	1842
122.4	125.3	125.4	121.7

¹⁰ 19.6	2.01	2.01	1.95
--------------------	------	------	------

Wet	728
Dry	622
Loss	106
	17%

622 / 122.4 = 5.08

331+00

1	2	3	f
3068	3068	3068	
245	⁶² 307	⁶¹ 368	⁶² 430
2066	2166	2133	

8%	10%	12%
1913	1969	1904
126.4	130.1	125.8

2.03	2.08	2.02
------	------	------

Wet	400	655	150
Dry	350	589	
Loss	50	66	
	14.3%	12.5%	

2714

150

2564

542100

354100

1

2

3

4

2583

50

50

50

180

230

280

330

1991

2084

2127

2096

7%

9%

11%

13%

1861

1912

1916

1855

123.0

126.3

126.6

122.6

1.97

2.02

2.03

1.96

See Page 17 for Sta 552100

W 761

D 671

L 90

13.4%

Base on East mile
Co. Rd. "H"

20

164

1	2	3	
2581	2581	2581	2581
	52	52	26
206	258	310	336
1930	2081	2194	2188

8%	10%	12%	13%
1782	1892	1959	1936
118.1	125.0	129.5	127.9
1.89	2.0	2.08	2.05

Co. Rd. "A"

Base

Void

21

91+00

1	2	3	4	5	6	7
3867	3586	3214	2846	2482	2482	2482
202	34	32	28	25	25	25
1962	1926	2011	2075	2174	2178	2168
1	2	3	4	5		6
546	547	549	549			646
527	524	522	518			598
146	147	149	149			146
381	377	373	369			452
19	23	27	31			48
5%	6.1%	7.2%	8.4%	9.5%	10.6%	10.6%
1867	1881	1876	1914	1986	1969	
123.4	124.3	124.0	126.4	131.2	129.0	
1.98	1.99	1.99	2.03	2.10	2.07	

100+00 Aug. 22, 1958

1	2	3	4	5	6	7
4670	4296	3926	3559	3196	2832	2475
327	43	39	36	32	28	25
1882	1927	2001	2027	2061	2099	2101
1	2	3	4	5	6	1
546	547	549	549	549	546	546
517	515	513	511	512?	500	502
146	147	149	149	149	146	146
371	368	364	362	363	354	356
29	32	36	38	36?	46	44
7.8%	8.7%	9.9%	10.5	11.7%	13.7.	13.6
1746	1777	1821	1825	1845	1857	1863
115.4	117.4	120.3	120.6	121.9	122.7	123.1
1.85	1.88	1.92	1.93	1.97		
				95%		
				1.87		

150+00

Aug. 27, 1958

2234

266	25	22	22	22	22	22
1877	1907	1957	2001	2027	2045	2031

2

1147

1002

147

855

145

11.9	13	14	14.5	15	16	17
------	----	----	------	----	----	----

1748	1763	1763	1736
------	------	------	------

115.5	116.5	116.5	114.7
-------	-------	-------	-------

1.85	1.87	1.87	1.84
------	------	------	------

35%	35%
1.78	1.75

Sta. 160+00

1 2 3

2391 2391 2391 2391

263 48 48 24

1891 1989 2029 2029

1

1006

889

146

743

217

117. 137. 157. 15.9%

1703 1760 1764 1751

112.5 116.3 116.6 115.7

1.87

1.78

Base Co. Rd. "A"

25

283

1

~~2895~~

4146 4146 4146 4146

~~231~~

298 41 41 41

~~2/22~~

2074 2217 2276 2260

4

949

881

149

732

68

~~8.0%~~

7%

8%

8.7

9%

9.37

10%

1938

2053

2088

2055

128.1

135.7

138.0

2.17

2.21

26

223400

116.70
1.87

sta. 229+00
To 239+50

27

223+00

235+00

11

2208 5480 5030 4570 4160

27 550 180 92 82

2003 1897 1999 2036 2000

6 1 2 3 4

904 646 647 649 649

778 599 589 584 579

146 146 147 149 149

652 453 442 435 430

106 47 58 65 70

15.6% 10.4 13.1 14.9 16.3

1718 1768 1772

11709

1.87

Sta 200+00 To 216+00

28

208+00

1	2	3	4	5	6
5720	5270	4830	4395	3965	3540
356	53	48	44	40	35
1925	1904	2025	2046	2058	2037
1	2	3	4	5	6
646	647	649	649	649	646
595	594	594	593	582	577
146	147	149	149	149	146
449	447	445	444	433	431
51	53	55	56	67	69
11.4	^{11.8} 12.6	³ 12.3	⁴ 12.3	15.5	16.0
1728	1775	1707	1790	1782	
114.18	116.43				
1.83	1.85		1.93		
			1.83		

Sta. 184+00 To 200+00

29

172

1 2 3 4

4417 3968 3528 3098

456 80 70 62

1852 1942 2004 2015

1 2

646 647 649 649

597 591 586 577

146 147 149 149

451 444 437 428

49 56 63 72

10.8% 12.6% 14.4% 16.8

1672 1725 1752 1725

110.5 114.0 115.8 114.0

1.77 1.83 1.86 1.83

1.77

255+00 To 266+00

266 To 293

30

258+00

280+00

1	2	3		
3817	3634	3364	3101	2690
382	72	70	62	50
1725	1815	1906	1983	2005
1	2	3	4	5
346	447	449	649	649
829	417	412	580	575
146	147	149	149	149
183	270	263	431	426
17	30	37	69	74
9.3	11.1	14.1	16.0	17.4
1578	1634	1662	1709	1708
		109.8	112.9	
		1.76	1.81	
			1.72	

1	2	3	4	
5663	4855	4159	3479	
665	75	42	35	
1969	2014	2050	2046	
1	2	3	4	
946	947	949	949	
866	846	855	845	
146	147	149	149	
720	699	706	696	
80	101	94	104	
11.1	12.6	13.8	15.0	
1748	1789	1801	1779	
117.5	116.2	117	117.6	
1.88	1.89	1.91	1.88	
		1.81		

183 Sta 240 To 255

48 June 11, 1959 " "
Base Co. Rd A
194700

1	2	3	4
4542	4170	3792	3471
317	42	38	35
2067	2178	2276	2267
1	2	3	4
546	547	549	647
519	518	517	605
148	147	149	149
373	371	368	456
27	29	32	45
7.2%	7.8%	8.7%	9.9%
1928	2020	2074	
127.4	133.5	138.4	
204	2.12	2.22	2.18

July 31, 1959

32

506100 Co. Rd "X"

1 2 3 4 5 6

5449 4989 4540 4095 3655 3215

448 100 45 41 37 32

1884 1993 2035 2082 2090 2087

1 2 3 4 5 6

646 647 649 649 649 646

609 602 602 600 572 590

146 142 149 149 149 146

463 455 453 451 443 444

37 45 47 49 57 56

8.0%. 9.9% 10.4% 10.9% 12.8% 12.6%

1744 1816 1843 1877 1853

115.24 120.00 121.79 124.03 122.4

1.99

1.89

Base Co. Rd. "X" Aug 18, 1958

33

1	2	
5735		
526	57	25
2188	2245	2243
1	2	
646	647	649
603	602	601
146	147	149
457	455	452
43	45	48
9.47%	9.97%	10.67%
2000	2043	2028
132.2	134.9	134.0
2.12	2.16.0	2.15

1 2 3 4 5 6



8-30-61	8-30-61	8-30-61	8-29-61	8-29-61
129+00	106+00	99+00	69+00	52+00
10' R	10' L	10' R	10' L	10' R
7"	5"	7½"	5"	7"
1421	851	1338	1750	1272
1346	796	1266	1662	1224
			82	48

75	55	72	88	48
5.67%	6.9%	5.7%	5.3%	4.0%

6	5	4	3	2	1
12.00	1205	1212	1202	1202	1245
	692	906	699	569	795
	513	306	503	633	450
	76°	76°	74°	85°	80°
	8704	8704	8710	8672	8689
	584	351	578	730	518
	2.29	2.27	2.17	2.28	2.38

9-5-59	9-5-59	9-5-59	9-3-59	9-3-59	9-3-59	9-2-59	9-2-59
412+00	404+00	396+00	428+00	444+00	444+00	380+00	388+00
11' Lt	11' Rt	11' Lt	11' Lt	11' Lt	11' Rt	11' Lt	11' Rt
5 1/2"	4 1/2"	5 1/2"	5"	6"	5 1/2"	6"	7"
1445	960	972	1159	1476	1203	1154	1460
—	—	—	—	—	—	—	—
1368	899	907	1085	1386	1123	1084	1368
77	61	65	74	90	80	70	92
			6.8%	6.5%	7.1%	6.4%	6.7%

2	1	6	5	4	3	2	1	6	5
1224	1229	1210	1238	1230	1249	1215	1229	1179	1253
		656	891	885	824	776	776	760	711
		554	347	345	425	546	419	419	542
		79°	78°	79°	86°	69°	62°	72°	72°
		8674	8678	8674	8668	8733	8718	8718	8718
		637	398	396	490	624	518	480	621
		2.16	2.26	2.28	2.28	2.23	2.18	2.27	2.21

9-2-57	9-1-57	9-1-57	9-1-57	9-1-57	9-1-57	8-31-57	8-31-57	8-31-57	8-31-57
396+00	404+00	412+00	420+00	436+00	444+00	420+00	428+00	436+00	444+00
11' Lt	11' Rt	11' Lt	11' Rt	11' Lt	11' Rt	11' Rt	11' Lt	11' Rt	11' Lt
5 1/8"	4"	6 1/4"	5"	5 1/4"	6"	6"	6"	6 1/4"	6 1/2"
1112	1018	1481	1345	1512	1437	1341	1429	1424	1386
937	954	1409	1292	1433	1366	1252	1353	1359	1326
175	64	72	83	79	71	89	76	65	60
16.2%	6.4%	5.1%	6.4%	5.5%	5.2%	7.1%	5.6%	4.8%	4.5%
4	3	2	1	6	5	4	3	2	1
1232	1239	1215	1228	1164	1249	1224	1256	1230	1221
818	859	630	733	608	661	746	696	692	679
414	380	585	495	556	578	478	560	538	542
62°	77°	76°	66°	66°	66°	74°	74°	71°	71°
8755	8701	8704	8740	8790	8740	8710	8710	8722	8722
474	436	670	566	637	659	549	642	615	621
1.97	2.18	2.10	2.28	2.26	2.08	2.28	2.11	2.21	2.14

See
Page

43 Rt

See
Page

43 Rt

Co. Rd. X
Base

45

8-25-59	8-25-59	8-25-59	8-25-59	8-22-59	8-22-59	8-22-59	8-22-59	8-21-59	8-21-59
452	460+00	468+00	476+00	484+00	492+00	500+00	513	528	508+00
11' RT	11' Lt	11' RT	11' Lt	11' RT	11' Lt	11' RT	11' RT	11' RT	11 1/2' Lt
5 1/2"	6"	5"	6 1/2"	5"	6"	6 1/4"	6 1/4"	6"	5 1/2"
1753	1889	1423	1997	1440	1533	1689	1544	1354	1187

1622	1771	1326	1850	1348	1472	1574	1521	1290	1131
131	119	97	147	92	61	115	53	64	55
8.1%	6.7%	7.3%	8.0%	6.8%	4.1%	7.3	3.5%	5.0%	4.9%
6	5	4	3	2	1	6	5	4	3
1154	1238	1225	1251	1223	1220	1165	1219	1221	1235
534	557	719	530	712	667	563	666	735	811
620	681	506	721	511	553	602	553	486	424
88°	87°	86	85	82°	82°	81°	80°	89°	88°
8661	8665	8668	8668	8652	8682	8686	8689	8658	8661
720	789	585	833	590	649	695	639	550	490
2.27	2.25	2.27	2.22	2.28	2.30	2.27	2.38	2.34	2.30

Base
Co. Rd. X

Subbase
Co. Rd. X

2

46

Subbase 3"

8-21-57	8-21-59	8-19-57	8-19-59	8-19-57	8-19-59	8-13-57	8-13-59	8-13-57	8-13-59
520+30	513+00	421+00	427+00	456+00	459+00	377+00	385+00	391+00	397+00
7' Lt	11' Rt	12 1/2' Lt	12 1/2' Rt	12 1/2' R	12 1/2' Lt	12 1/2' Lt	12 1/2' Rt	12 1/2' Rt	12 1/2' Lt
6"	7"	4"	4"	4"	4"	4"	4"	4"	4"
1406	1914	1532	931	1117	1099	1304	1049	1012	906
1340	1817	1391	860	1021	993	1187	973	929	827
66	97					120	76	85	79
4.9	5.3%							9.2%	9.5%
2	1	6	5	4	3	2	1	6	5
1198	1215	1183	1221	1192	1212	1183	1122	1179	1222
698	414	532	831	724	773	668	698	778	850
500	801	651	390	468	419	515	424	401	372
89°	89°	88°	88°	86°	86°	76°	75°	72°	72°
8658	8658	8661	8661	8668	8668	8704	8708	8718	8718
579	928	753	450	538	484	591	488	460	427
8.32	1.76	1.84	1.91	1.91	2.05	2.02	2.00	2.02	1.93

See
Page
45 RT

Rt 179

8-12-59	8-12-59	8-12-59	8-11-59	8-11-59	8-10-59	8-10-59	8-10-59	8-10-59	8-10-59
403+00	903+00	415+00	421+00	458+00	427+00	439+00	440+00	446+00	458+00
12½ Rt	12' Lt	12' Rt	12½ Lt	12½ Lt	12½ Rt	12½ Lt	12½ Rt	4"	12½ Rt
4"	4"	4"	4"	4"	4"	4"	4"	4"	4"
1331	934	1065	993	1144	549	691	892	786	815
—	—	—	—	—	514	—	—	—	—
—	—	—	—	—	0	0	0	0	—
1222	878	988	926	1042	514	658	842	745	721
109	56	77	67	102	35	33	50	41	84
8.3	6.4%	7.8%	7.2%	9.8	6.8%	5.0%	5.9%	5.5%	11.6%
4	3	2	1	6	5	4	3	2	1
1233	1226	1209	1213	1169	1207	1221	1220	1240	1221
736	825	795	752	665	959	965	836	925	874
497	401	414	461	504	248	256	384	315	347
82°	79°	78°	74°	74°	86	88°	87°	87°	74°
.8682	.8693	.8697	.8710	.8710	8668	8661	8665	8665	.8712
573	461	475	529	579	287	276	444	363	398
2.13	1.90	2.07	1.75	1.81	1.79	2.22	1.90	2.05	1.81

6=3

Co. Rd. "L" Base

48

7-27-59	7-27-59	7-27-59	7-27-59	7-24-59
131+00	124+00	89+00	95+00	100+00
¢	11' RT	11' RT	11' LT	¢
6"	4 1/2"	5 1/4"	4 1/2"	5 1/2"
1226	987	1046	1052	1202
1160	951	1005	1009	1140
66	36	43	43	62
	3.87%	4.37%	4.37%	5.57%

1	6	5	4	3	2	1
1192	1153	1196	1210	1220	1221	1213
	755	847	840	833	784	
	441	363	380	388	429	
	86°	86°	80°	71°	80°	
	8668	8668	8689	8715	8689	
	510	419	438	444	473	
	2.27	2.28	2.30	2.27	2.32	

Base Co. Rd. "L"		Base Co. Rd. "L"	Subbase Co. Rd. "L"		Co. Rd. "L" subbase		Base 49. Co. Rd. A		
7-24-59	7-24-59	7-24-59	7-18-59	7-18-59	7-14-59	7-14-59	7-14-59	7-6-59	7-6-59
106+00	113+00	124+00	130+00	123+00	89+00	96+00	110+00	250+00	243+00
11 1/2 R	11' Lt	11 1/2 Rt	12 1/2 Rt	12 1/2 Lt	12 1/2 Lt	12 1/2 Rt	12 1/2 Lt	\$	\$
6"	6 1/4"	9 3/4	4"	4"	4"	4"	4"	5"	6"
1335	1198	1172	938	877	931	1101	1242	1184	1292
1278	1156	1104	859	805	872	1030	1178	1122	1223
	3.2	115	99	104	92	97	100	115	99
57	42.	68	79	72	59	71	64	100.7	112.9
4.5%	3.6%	6.1%	9.2	8.9				6.2	6.9
6	5	4	3	2	1	6	5	4	3
1147	1193	1220	1213	1230	1220	1178	1222	1227	1230
661	741	764	857	889	826	717	748	836	776
486	452	456	356	341	394	461	474	391	454
78°	78°	72°	86°	84°	82	82°	80°	64°	64°
.8697	.8697	.8718	.8689	.8675	.8682	.8682	.8689	.8798	.8798
559	521	521	410	392	453	532	544	453	519
2.28	2.22	2.13	2.07	2.05	1.93	1.94	2.16	2.22	2.18

Co. Rd. "A"
Base

Co. Rd. "A"
Base

50

7-3-59	7-3-59	7-2-59	7-2-59	7-2-5	7-1-59	7-1-59	7-1-59	7-1-59	6-25-59
252+00	246+50	252+00	246+50	241	330+00	320+00	252+00	245+00	228-00
11' Lt	4	11' L	4	11' R	11' Lt	11' Rt	4	11' Rt	11' Lt
6"	6"	6 1/4	6	5 1/2	5	5"	6"	6"	6"
17907	1331	1582	1497	1648	1372	1430	1316	1622	1647
1804	1244	1491	1402	1563	1268	1331	1228	1505	1554
104	92	93	100	115	99	104	92	93	100
1700	1152	1398	1302	1448	1169	1227	1136	1412	1454
		91	95	85	106	99	88	117	93
		6.5	7.3	5.9	9.1%	8.0%	7.8%	8.3%	6.4%
2	1	6	5	4	3	2	1	6	5
1227	1226	1180	1210	1212	1213	1213	1250	1168	1248
57.2	739	611	676	648	748	737	792	602	698
655	487	569	534	564	465	476	458	566	550
68°	66°	78°	74°	72°	62°	63°	63	64°	98°
.8733	.8740	.8697	.8710	.8718	.8755	.8752	.8752	.8748	.8625
749	559	656	612	646	532	545	523	645	638
2.27	2.07	2.13	2.13	2.25	2.20	2.25	2.16	2.19	2.28

Same

Co. Rd. A
Base

Co. Rd. A
Base

51

6-25-59	6-25-59	6-25-59	6-24-59	6-24-59	6-24-59	6-24-59	6-23-59	6-23-59	6-22-59
221-00	215+00	299+00	305-00	312+00	249-00	282+00	295+00	270+00	265+00
3' Lt	11' Lt	11' Rt	4'	11' Lt	11' Rt	11' Lt	4'	11' Rt	11' Lt
6"	7 3/4"	6"	7"	7 3/4"	6 1/2"	4 3/4"	5"	4 3/4"	5 3/4"
1510	2302	1663	2059	2151	2012	1690	1280	1186	1581
1441	2178	1569	1926	2026	1734	1627	1210	1134	1527
115	99	104	92	93	100	115	99	104	92
1326	2079	1465	1834	1933	1834	1512	1111	1030	1435
69	124			125	78	71	70	52	54
5.2%	6%			6.1	4.3	4.7	6.3%	5.0%	3.8%

4	3 ²²⁸	2	1 ⁸⁴	6+5	4	3	2	1
1213	1212 ¹²²⁸	1213	<u>1183</u> ¹²¹³	<u>1175</u> ¹¹⁹⁸	1208 ¹²¹²	1214	1226	1231
720	2440 ⁵⁹¹	645	<u>2396</u> ²³⁷¹	<u>1622</u> ²⁴²⁶	610	772	789	642
493	<u>1634</u> ¹⁶³⁴	568	<u>1670</u>	<u>749</u> ¹⁷²⁹	598	442	437	579
98°	97°	92°	91°	91°	86°	84°	60°	58°
.8625	.8629	.8647	.8650	.8650	.8668	.8675	.8762	.8769
572	932	655	839	865	805	690	505	500
2.32	2.23	2.24	2.28	2.23	2.27	2.19	2.18	2.06

Co. Rd. 'A'
Base

Co. Rd. "A"
Base

52

6-22-59	6-22-59	6-22-59	6-22-59	6-22-59	6-22-59	6-22-59	6-22-59	6-19-59	6-19-59
275+00	270+00	265+00	200+00	255+00	228+00	222+00	215+00	253+00	253+00
£	11' R	11' L	£	11' RT	11' RT	3' RT	11' RT	11' LT	11' RT
4 3/4"	4 1/2"	5"	6 1/4"	6 1/2"	7"	5 1/4"	6"	4 1/2"	6"
1514	1472	1719	1660	1715	2129	1557	1235	1500	2007
1415	1400	1658	1590	1644	2048	1497	1199	1426	1918
93	100	115	99	104	92	93	100	115	99
1322	1300	1543	1491	1540	1956	1404	1097	1311	1819
99	72	61	70	71	81		36	74	89
7.5%	5.1%	3.9%	4.7%	4.6	4.1		3.3%	4.9	4.9%
6	5	4	3	2	1-4	6	5	4	3-6
1157	1175	1231	1204	1197	1201	1147	1201	1183	1151
631	667	606	636	619	637	604	775	642	2354
526	528	625	568	578	752	543	426	541	1578
79°	78°	76°	72°	70°	68°	67°	69°	84	76°
.8693	.8697	.8764	.8716	.8725	.8733	.8736	.8729	.8675	.8704
604	607	718	650	660	861	622	484	626	890
2.19	2.15	2.16	2.29	2.33	227	2.26	2.27	2.10	2.04

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.8675
8668

Co. Rd "A"

Base

6-17-59	6-19-59	6-17-59	6-17-59	6-16-59
249+00	241+00	253+00	232+00	236+00
11' LT	11' RT	11' RT	11' LT	10' RT
6 3/4	5 1/2	6"	6"	8"
1755	1689	1282	1265	1761
1668	1604	1217	1220	1685
104	92	92	100	115
1564	1512	1125	1120	1570
87	85	65	45	76
5.5%	5.6%	5.7%	4.0	4.8

2	1	6	5	4
1213	1190	1168	1214	1229
617	585	676	784	611
600	605	472	430	618
76°	75°	68°	66°	88
.8704	.8708	.8733	.8733	.8661
688	694	540	472	701
2.29	2.18	2.09	2.28	2.24

See Rt.
Side Page
52

Co. Rd. "A"

Base

53

6-16-59	6-16-59	6-16-59	6-15-59	6-15-59
227+00	218+00	209+10	209+00	201+00
4	11' LT	11' RT	11' RT	4
5"	7"	6"	6"	5 1/2"
1479	1789	1323	1685	1312
1431	1720	1284	1630	1264
99	104	92	92	100
1332	1616	1492	1538	1164
48	69	39	55	48
3.6%	4.3%	3.3%	3.6%	4.1%

3	2	1	6	5
1238	1263	1239	1176	1252
667	584	765	537	791
571	679	474	639	461
86"	82°	80°	67°	65°
.8668	.8682	.8689	.8736	.8744
660	781	545	734	528
2.02	2.06	2.18	2.10	2.22

See
Page
52 RT

See
Sta 215
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52 RT

Co. Rd. A
Base

Co. Rd. A
Subbase

Co. Rd. A
Subbase

54

6-15-59	6-15-59	6-10-59	6-10-59	6-10-59	6-5-59	6-5-59	6-5-59	6-5-59	6-8-59
174+00	185+00	333+00	323+00	315+00	307+00	298+00	289+00	280+00	271+00
11' Lt	11' Rt	12 1/2 Lt	12 1/2 Rt	4'	12 1/2 Rt	12 1/2 Lt	4'	12 1/2 Rt	12 1/2 Lt
5	6"	4"	4"	4"	9"	4"	4"	4"	4"
1334	1529	1024	1058	990	1127	1168	1043	1000	1141
1289	1465	939	968	899	1048	1110	958	997	1053
115	99	104	92	92	100	115	99	104	92
1174	1366	835	876	807	948	995	859	893	981
45	64					58	85	63	88
3.8%	4.7%					5.8	9.9	7.1	9.0
5.4	3	2	1	6	5	4	3	2	1
1258	1268	1173	1147	1156	1204	1207	1214	1220	1211
793	722	776	744	772	784	778	1303	798	763
465	546	397	403	394	420	429	411	422	448
65°	65°	82°	80°	78°	78°	77°	78°	78°	77°
.8744	.8744	.8682	.8689	.8697	.8697	.8701	.8710	.8718	.8722
531	622	459	464	453	483	493	472	484	514
2.21	2.20	1.82	1.88	1.79	1.97	2.05	1.82	1.87	1.81
2.22	2.22						1.81	1.81	1.81

Co. Rd. "A"
Subbase

Co. Rd. A
Subbase

55

6-3-59	6-3-59	6-3-59	6-3-59	6-3-59	5-27-59	5-27-59	5-27-59	5-25-59
257+00	253+00	244+00	241+00	265+00	209+00	203+00	194+00	187+00
12 1/2 Lt	♀	12 1/2 Rt	12 1/2 Lt	12 1/2 Rt	12 1/2 Rt	12 1/2 Lt	12 1/2 Rt	12 1/2 Lt
				4"	4"	4"	4"	4"
1153	1108	1133	1232	1135	1147	1389	1147	1419
1015	997	991	1120	1016	1073	1248	1009	1244
100	115	99	104	92	100	115	99	104
945	882	892	1016	924	973	1133	910	1140
138	111	142	112	119	74	141	138	175
15.1	12.6%	15.7%	11.0%	12.9		12.4	15.2	15.4

5	4	3	2	1	6	5	4	3	2
1183	1193	1211	1240	1211	1154	1213	1196	1175	1217
746	798	780	795		726	743	661	743	642
437	395	431	445		428	470	535	452	575
74°	72°	72°	68		74°	72°	72°	72	70°
8790	8922	8922	8933		8710	8710	8710	8710	8725
510.1	483	494	510		492	538	614	518	659
1.82	1.55	1.81	1.99		1.88	1.81	1.85	1.76	1.73
1.92	1.93	1.93	1.87		1.92	1.83	1.83	1.78	1.79
						✓	✓	✓	✓

Subbase
1 1/2"

Subbase

Subbase

56

Base

5-25-59	5-25-59	5-25-59	5-15-59	5-15-59	5-14-59	5-14-59	9-20-58	9-20-58
199+00	203+00	209+00	234+00	288+00	232+00	215+00	183+00	177+00
4	12 1/2 Rt	12 1/2 Lt	4	11 1/2 Rt	11 1/2 Lt	11 1/2 Rt	11' Lt	11' Rt
4"	4"	4"	4"	4"	4"	4"	6'	6"
1462	1558	1178	1472	1132	1287	13.16	1820	2118
1295	1382	1043	1384	1049	1146	1205	1718	2030
92	92	100	115	99	104	92	92	98
1203	1290	942	1269	950	1042	1113	1626	1930
167	176	135	88	83	141	111	102	88
147	13.6	12.8	6.9	8.7	13.5	10.70	6.37	4.67
1	6	5	4	3	2	1	1	6
1198	1215	1245	1251	1238	1216	1217	1235	1190
627	580	771	623	769	706	669	618	635
578	635	474	628	467	510	548	617	644
70	68°	67°	46°	46°	50°	51°	60°	60°
8725	8733	8736	8812	8812	8798	8794	8783	8783
645	727	543	710	532	577	622	703	896
1.87	1.77	1.73	1.79	1.78	1.81	1.79	2.31	2.16
1.77	1.83	1.83	1.78	1.78	1.78			

See Page
55-Rt.

9-20-58	9-20-58	9-18-58	9-18-58	9-18-58	9-18-58	9-18-58	9-18-58	9-13-59	9-13-58
171+00	165+00	125+00	159+00	152+00	146+00	140+00	134+00	128+00	122+00
11' Lt	11' Rt	11' Rt	11' Lt	11' Rt	11' Lt	11 1/2 Rt	11 1/2 Lt	11 1/2 Rt	11 1/2 Lt
6"	6"	6"	5"	6 1/2"	7 1/4"	7"	6"	4 3/4"	6"
1600	1360	1919	2030	2546	2069	2331	1660	1510	1675
1510	1293	1829	1936	2425	1973	2217	1574	1454	1590
115	99	102	92	102	92	92	100	115	99
139.5	1194	1727	1844	2323	1881	2125	1474	1339	1491
90	67	90	94	121	96	114	86	56	85
6.5%	5.6%	5.2%	5.1%	5.2%	5.1%	5.4%	5.8%	4.2%	5.7%
4	3	2	1	2-3	1	6-4	5	4	3
1226	1254	1236	1212	³⁻¹²³⁶ 1254	1256	⁴⁻¹²⁷² 1203	1231	1240	1254
699	788	582	488	²⁵⁰⁷ 1576	517	²⁴⁷⁵ 1620	658	713	652
527	466	754	731	911	739	847	573	527	602
56°	56°	67'	66°	60°	56°	56°	56°	58°	55°
.8797	.8797	.8761	.8765	.8703	.8790	.8797	.8797	.8790	.8801
599	530	861	836	1040	841	961	652	600	685
2.33	2.25	2.01	2.22	2.23	2.24	2.21	2.25	2.23	2.18

Subbase 58

[illegible]

9-2-58	9-2-58	9-2-58	9-2-58	9-2-58	8-29-58	8-29-58	8-29-58	8-29-58	8-29-58
128+00	122+00	116+00	110+00	85+00	182+00	104+00	97+00	91+00	85+00
1 1/2 Rt	1 1/2 Lt	1 1/2 Rt	1 1/2 Lt	4	1 1/2 Lt	4	1 1/2 Rt	1 1/2 Lt	4
4"	4"	4"	4	4"	4"	4"	4"	4"	4"
1237	1137	1305	1180	1051	1290	1162	1376	973	1368
1142	1035	1201	1091	966	1154	1056	1223	909	1217
100	115	99	102	92	92	100	115	99	102
1042	920	1102	989	874	1062	956	1108	810	1115
95	102	104	89	85	136	116	153	64	151
9.1%	11.5%	9.4%	9.0%	9.7%	12.8	12.1%	13.8%	7.9%	13.8%
5	4	3	2	1	6	5	4	3	2
1228	1255	1257	1272	1253	1179	1230	1235	1254	1210
766	843	759	838	858	704	780	714	913	659
462	412	498	434	395	475	450	521	341	551
84°	83°	66°	66°	64°	82°	80°	81°	81	78°
8696	8699	8761	8761	8769	8703	8710	8706	8706	8717
531	473	569	496	451	546	516	597	392	631
1.92	1.94	1.94	1.99	1.94	1.95	1.86	1.85	2.06	1.78
				2 nd Test					See Lt Side of Page
1.87	1.87	1.87	1.87	1.87		1.87	1.87	1.87	1.87

Co. Road "A" Subbase
C-816

Co. Road "A" Subbase 60

8-29-58	8-29-58	8-29-58	8-29-58	8-29-58	8-28-58	8-28-58	8-28-58	8-28-58	8-28-58
175+00	168+00	162+00	140+00	134+00	120+00	128+00	106+00	99+00	93+00
1 1/2 RT	L	1 1/2 LT	1 1/2 LT	1 1/2 RT	1 1/2 RT	1 1/2 LT	1 1/2 LT	1 1/2 RT	1 1/2 LT
4"	5"	4	4"	4"	4"	4"	4"	4"	4"
1295	1435	1385	1292	1229	255	1043	1507	1191	1379
1175	1303	1259	1161	1128	785	959	1366	1070	1268
92	92	100	115	99	102	92	92	100	115
1083	1211	1159	1046	1029	683	867	1274	970	1153
120	132	126	131	101	70	84	141	121	111
					10.0%	9.5%	11.1%	13.5%	9.2%
1	6	5	4	3	2	1	6	5	4
1237	1187	1205	1204	1225	1209	1221	1166	1229	1203
747	625	676	701	775	884	817	593	762	653
490	562	529	503	450	325	404	571	467	550
75°	75°	74°	73°	73°	84°	84°	69°	67°	66°
8728	8728	8732	8736	8736	8696	8696	8751	8758	8761
560	645	605	578	514	323	465	652	535	629
1.94	1.88	1.92	1.82	2.00	1.83	1.86	1.95	1.82	1.84
1.1	1.1	1.1	1.78	1.87	1.87	1.87	1.87	1.87	1.87

X

SEC
Sta 91

County Road
"A"
Subbase

County Road
"H"

Base

61

8-28-58	8-28-58	8-27-58	8-18-58	8-18-58	8-18-58	8-18-58	8-18-58	8-18-58	8-18-58
87400	81400	150400	277400	241400	247400	257400	267400	277400	287400
4"	11 1/2" RT	11 1/2" LT	11 1/2" LT	11 1/2" LT	11 1/2" RT	11 1/2" LT	11 1/2" RT	11 1/2" LT	11 1/2" RT
4"	4"	4"	6"	.	6 1/2"	5"	6 1/2"	6 1/4"	5"
1476	1109	1247	2030	1629	2118	1238	1697	1430	1249
1320	1493	1600	1941	1559	2008	1171	1622	1370	1199
99	102	92	92	100	115	99	102	92	92
1221	1391	1008	1849	1459	1893	1072	1520	1278	1107
156	106	147	89	80	110	67	75	60	50
12.8%	7.6%	14.6%	4.8%	5.5%	5.7%	6.3%	4.9%	4.7%	4.5%
3	2	1	6	5	4-5	3	2	1	6
1213	1202	1218	1172	1226	1244 1250	1260	1253	1249	1198
634	579	716	437	594	2494 1210	833	601	680	744
585	623	502	735	632	784	427	652	569	454
66°	64°	64°	96°	85°	82°	76°	76°	75°	72°
8761	8769	8769	8654	8692	8703	8725	8725	8728	8740
669	712	572	850	730	900	483	748	650	518
1.83	1.95	1.76	2.18	2.00	2.10	2.22	2.04	1.96	2.15
1.87	1.87	1.78							

See sta
152400
Rt. side
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Subbase

Base

Sub-
Base

Base

62

8-13-58	8-13-58	8-13-58	8-12-58	8-12-58	8-12-58	8-12-58	8-12-58	8-12-58	8-12-58
258+00	295+00	301+00	240+50	244+00	246+00	271+00	241+00	241+00	240+00
11 1/2 RT	11 1/2 LT	11 1/2 PT.	2	9 RT.	9 LT	11 1/2 RT.	11 1/2 RT	11 1/2 RT	4
4"	7"	7"	6"	8"	6"	4"	3 3/4"	6 1/2"	3"
990	1776	1800	1883	2378	1550	968	1208	1670	1238
909	1406	1713	1787	2224	1460	890	1138	1566	1153
700	115	99	102	92	92	100	115	99	102
809	1591	1614	1685	2132	1368	790	1023	1467	1057
81	70	87	96	154	90	78	70	104	85
10.7%	4.4%	5.4%	5.7%	7.2%	6.6%	9.9%	6.8%	7.1%	8.1%

5	4	3	2	1-4	6	5	4	3	2
1255	1240	1234	1200	4-1225 1-1212	1140	1214	1216	1230	1217
877	568	532	535	2437 1485	599	869	785	599	803
378	672	705	665	952	591	345	431	631	414
70°	70°	66°	92°	92°	73°	93°	91°	90°	84°
8747	8747	8761	8668	8668	8664	8664	8671	8675	8696
482	771	805	769	1100	685	399	498	730	476
1.84	2.07	2.02	2.19	1.94	2.00	1.98	2.06	2.02	2.22

22.8

22.4

Subbase

Base

Subbase

8-12-58	8-12-58	8-12-58	8-11-58	8-11-58	8-11-58	8-11-58	8-11-58	8-11-58
240+00	241+00	241+00	258+50	268+00	268+00	257+00	273+00	278+00
£	11' RT	11' RT	11½' RT	11½' LT	£	11½' LT	11½' LT	11½' RT
6½"	3½"	7"	4"	4	4"	4"	4"	4"
1833	1179	2169	1145	1206	1164	1386	1404	1264
1707	1090	2006	1028	1137	1084	1226	1286	1167
92	100	115	99	102	92	92	92	100
1615	990	1891	929	1035	994	1134	1194	1067
126	89	163	117	69	80	160	118	97
7.8%	9.0%	8.6%	12.6%	6.7%	8.0%	14.1	10.0%	9.1%

6	5	4-1	3	2	1	1	6	5
1177	1227	1-1211 4-1227	1258	1221	1235	1221	1189	1221
490	821	2438 1586	788	743	794	661	682	755
687	406	852	470	448	441	560	507	466
83°	78°	79°	84°	83°	83°	77°	77°	78°
8699	8717	8714	8696	8699	8699	8721	8721	8717
790	465	979	541	515	509	641	579	511
2.04	2.13	1.94	1.71	2.02	1.97	1.76	2.07	2.09

see page
62

see page
62

Subbase

4

2

8-11-58	8-11-58	8-11-58	8-9-58	8-9-58	8-8-58	8-9-58	8-9-58	8-8-58	8-8-58
284+00	290+00	252+10	243+00	258+50	259+	268+00	269+00	259+	279+00
±	14 1/2 ft.	±	±	10' RT.		10' RT.	±		±
4"	4"	4"	4"	4"	4"	4"	4"	4"	1163
1593	1333	1350	1198	1081	1110	1222	1120	1296	1040
1974	1216	1254	1096	935	1015	1123	1046	1457	
115	99	102	92	92	100	115	99	102	92
1359	1112	1152	1004	843	915	1008	947	1055	948
1119	422	96	82	146	95	99	74	139	123
10.2%	11.0%	8.4	8.1	17.6%	10.2	9.8%	7.8%	13.2	13.0%
4	3	2	1	6	5	4	3	2	1
1225	1234	1205	1213	1181	1220	1241	1227	1201	1224
269	268	678	773	740	760	785	782	664	780
550	466	523	440	441	460	456	445	537	442
74'	77°	76°	83°	75°	701°	76°	72°	96°	95°
8721	8721	8721	8699	8728	8636	8721	8740	8654	8657
634	534	600	507	505	531	522	509	620	511
2.12	2.08	1.92	1.98	1.65	1.79	1.93	1.87	1.70	1.85

See 258
Page 62

See Sta. 258
on Page 62

✓

✓

Subbase

Base

65

8-8-58	8-7-58	8-8-58	8-8-58	8-7-58	8-6-58	8-6-58	8-6-58	8-6-58	8-6-58
252+00	264+00	239+00	247+00	288+00	337+00	307+00	313+00	321+00	329+00
4"	11 Rt.	11 1/2 Lt.	11 1/2 Rt.	11 1/2 Lt.	11 1/2' Lt.	11 1/2' Lt.	11 1/2' Rt.	11 1/2' Lt.	11 1/2 Rt.
4"	4"	4"	4"	4"	6 1/2"	6 1/4"	6 1/2"	6"	5 3/4"
1294	986	1280	1187	1725	2745	1627	1956	1753	1390
1201	859	1202	1106	1588	2589	1526	1834	1654	1310
92	100	115	99	102	92	102	92	92	100
1109	759	1087	1007	1486	2497	1424	1742	1562	1210
93	127	78	81	137	176	101	122	99	80
8.8%	16.8%	7.2%	8.0%	9.2	4.5%	7.1%	7.0%	6.3%	6.6%

6	5	4	3	2	1-6	2	1	6	5
1178	1222	1227	1227	1215	1180 1210	1202	1237	1211	1180
685	777	762	786	494	2390 330	614	530	560	702
49.3	44.5	46.5	44.7	721	1060	588	707	651	478
97°	84°	92°	92°	82°	86°	85°	85°	84°	76°
8650	8696	8668	8668	8703	8689	8692	8692	8696	8725
570	511	537	510	830	1221	678	812	750	547
1.80	1.48	2.03	1.98	1.79	2.04	2.11	2.12	2.09	2.21
See Page #64				See s'm. 284 Page 64 Lt.	270 Test				

1100

1 = 486
6 = 842
1330

23.1

23.3

22.8

22.7

Base		Subbase	Base		Subbase	Base		Subbase	66
									Base
8-6-58	8-6-58	8-4-58	8-4-58	8-4-58	8-2-58	8-1-58	8-1-58	8-1-58	8-1-58
337+00	385+00	286+00	345+00	353+00	361+00	294+00	300+00	306+00	369+00
11 1/2' Lt.	11 1/2' Lt.	11 1/2' Rt.	11 1/2' Rt.	11 1/2' Lt.	11 1/2' Rt.	11 1/2' Lt.	11 1/2' R.	11 1/2' L.	11 1/2' L.
6 3/4"	6"	4"	7 1/2"	6"	6"	4"	4"	4"	7 1/2"
1710	1737	1757	1519	1752	1515	1537	1546	1355	2510
1617	1641	1651	1436	1683	1431	1413	1435	1252	2351
115	99	102	100	92	92	115	99	102	91
1502	1542	1549	1336	1591	1339	1298	1336	1150	2260
93	96	106	83	69	84	124	111	103	159
6.2%	6.2%	6.8%	6.1%	4.3%	6.3%	9.6%	8.3%	9.0%	7.1%
4	3	2 ⁻³	5	6	1	4	3	2	1-5
1206	1243	1225 1207 2432 1614	1204	1189	1224	1197	1230	1218	8-1215 1-1239
54N	608		619	519	685	619	661	715	2454 1498
662	635	818	588	670	539	578	569	503	956
87°	76°	76°	76°	72°	78°	82°	79°	78°	78°
8685	8725	8725	8725	8740	8717	8703	8714	8717	8717
765	728	935	671	715	618	662	652	579	1091
1.92	2.13	1.66	1.98	2.23	2.18	1.96	2.07	1.99	2.07
See Page 65			✓						
22.8	23.1		23.1	23.1	23.2				

Subbase						Base				67 Base
Base										
8-1-58	7-31-58	7-31-58	7-30-58	7-30-58	7-30-58	7-30-58	7-30-58	7-30-58	7-30-58	7-30-58
377400	312400	319400	327400	335400	343400	393400	402400	409400	417400	
11 1/2' R	11 1/2 Rt	11 1/2 Lt	11 1/2 Rt	11 1/2 Lt	11 1/2 Rt	11 1/2' Rt	11 1/2 Lt	11 1/2 Rt	11 1/2 Lt	
4 3/4"	4"	4"	4"	4"	4"	5 1/4"	5"	5"	4 3/4"	
1723	1352	1187	1213	1162	936	1616	1419	1292	1483	
1628	1258	1107	1143	1082	848	1522	1334	1216	1409	
92	100	115	99	102	91	92	100	115	99	
1536	1158	992	1044	980	757	1430	1234	1101	1310	
95	94	80	70	80	88	92	85	76	74	
6.2%	8.1	8.1%	6.7%	8.2%	11.6%	6.4%	6.9%	6.9%	5.6%	
6	5	4	3	2	1	6	5	4	3	
1158	1204	1203	1225	1209	1224	1197	1222	1234	1240	
562	699	773	795	792	880	622	702	798	710	
596	505	430	430	417	344	555	520	436	530	
73°	86°	86°	76°	74°	74°	67°	66°	66°	65°	
8736	8689	8689	8725	8723	8723	8758	8761	8761	8765	
681	581	495	491	478	394	629	592	497	605	
2.25	1.99	2.00	2.13	2.05	1.92	2.28	2.08	2.22	2.17	
						22.4	21.5	22.6'	22'	

Subbase

Base

Subbase

7-28-58	7-28-58	7-28-58	7-28-58	7-25-58	7-25-58	7-25-58	7-25-58	7-23-58	7-23-58
367+85	352+00	360+00	368+00	425+00	433+00	441+00	449+00	376+00	384+00
11 1/2 LT	11 1/2 LT	11 1/2 RT	11 1/2 LT	11 1/2 RT	11 1/2 LT	11 1/2 RT	11 1/2 LT	11 1/2 R	11 1/2 L
4"	4"	4"	4"	4 1/4"	5"	5 1/4"	6 1/4"	4"	4"
1556	1414	1402	1195	1406	1594	1512	1689	1222	1070
1424	1300	1270	1080	1327	1516	1425	1598	1153	974
102	91	92	100	115	99	102	91	115	109
1322	1209	1178	980	1212	1417	1323	1507	1038	874
132	114	132	115	79	78	87	91	69	96
	9.4%	10.2%	11.7%	6.5%	5.5%	6.5%	6.0%	6.6%	11.0%
2	1	6	5	4	3	2	1	4	5
1224	1230	1189	1218	1233	1222	1213	1226	1222	1225
652	720	676	595	754	656	682	607	780	823
572	510	513	643	479	566	531	619	442	402
78°	75°	71°	69°	77°	74°	69°	68°	80°	73°
8717	8728	8743	8751	8721	8732	8751	8754	8710	8736
658	584	587	735	549	649	609	708	508	460
2.02	2.07	2.00	1.33%	2.22	2.18	2.18	2.22	2.04	1.90

?

24'

24

23.3

23.2

1214

755

463

530

1.85

subbase

Base

7-23-58	7-17-58	7-17-58	7-17-58	7-12-58	7-12-58	7-12-58	7-12-58	7-10-58	7-10-58
392+00	400+00	408+00	424+00	462+00	486+00	470+00	478+00	551+00	555+00
11 1/2 R	11 1/2 Lt	11 1/2 Lt	11 1/2 Rt	11 1/2 L	11 1/2 R	11 1/2 R	11 1/2 L	11 1/2 L	11 1/2 L
4"	4"	4"	4"	6 3/4"	7 1/2"	8 1/2"	5 1/2"	6"	5"
1160	1762	1492	1358	2073	2210	2342	1756	1708	1368
1081	1628	1377	1205	1958	2061	2180	1641	1587	1275
92	99	102	91	102	91	102	91	102	91
989	1529	1275	1114	1856	1970	2078	1550	1485	1184
279	134	115	153	115	149	162	115	121	93
8.0%	8.8%	9.0%	13.8%	6.2%	7.4%	7.8%	7.4%	8.1%	7.8%
6	3	2	1	295	186	223	1	2	1
1173	1238	1224	1215	1221	1183	1246			
711	627	690	719	1215	1223	1238	1229	1228	1232
462	611	534	496	2436	2406	2484			
				1642	1580	1612	568	628	751
70°	65°	64°	62°	794	826	872	661	600	481
8747	8765	8769	8776	800	77°	72°	66°	78'	78°
529	699	610	568	8710	8714	8723	8744	8700	8700
1.90	2.18	2.08	1.96	910	945	1000	755	690	553
				2.03	2.08	2.08	2.05	2.16	2.15

Base		Subbase		Base		Subbase		Base		70
										Base
7-7-58	7-9-58	7-8-58	7-8-58	7-8-58	7-7-58	7-7-58	7-7-58	7-7-58	7-7-58	
55 1+00	555+00	416+00	424+00	520+00	541+00	452+00	456+00	549+00	555+00	
11 1/2 L	11 1/2 L	11 1/2 L	11 1/2 R	11 1/2 R	11 1/2 L	11 1/2 R	11 1/2 R	11 1/2 R	11 1/2 L	
7"	7"	4"	4"	4"	8"	4"	4"	8 1/2"	6 3/4"	
1877	1776	1810	1403	1602	1636	1577	1688	2340	2635	
1758	1662	1671	1274	1508	1563	1475	1477	2225	2482	
115	99	102	91	115	115	99	102	91	92	
1643	1573	1569	1183	1393	1448	1376	1375	2134	2390	
119	114	139	129	93	73	102	219	115	153	
7.2%	7.2%	8.9%	10.9%	6.7%	5.0%	7.5%	15.3%	5.4%	6.4%	
4	3	2	1	4	4	3	2	1 1/2	6 1/2	
1217	1221	1210	1214	1233	1240	1201	1206	1187	1226	
520	520	515	661	666	659	598	545	1652	1557	
697	701	695	553	567	590	603	661	2939	2387	
85°	80°	78°	76°	72°	80°	81°	81°	1557	1283	
8674	8692	8700	8708	8723	8727	8689	8689	882	1104	
805	808	799	672	648	680	695	762	79°	73°	
2.04	1.95	1.97	1.76	2.15	2.13	1.98	1.80	8696	8696	
See Page 69-R1		See Page 69-R1						1013	1275	
								2.12	1.88	
								See list of Page 69-R1		
23.3'	24.0'			23.4'						

Co. Rd. "H"

Base

Subbase

1-7-58	7-7-58	7-7-58	7-7-58	7-1-58	7-1-58	7-1-58	7-1-58	7-1-58	7-1-58
494+00	502+00	512+00	520+00	527+00	527+00	432+00	439+00	446+00	456+00
11 1/2 L	11 1/2 R	11 1/2 L	11 1/2 R	2	6	11 1/2 R	11 1/2 L	11 1/2 R	11 1/2 R
7"	5 1/2"	6"	3 3/4"	7"	7"	4"	4"	4"	4"
2675	1765	2060	1477	1910	1828	2098	1659	1716	1509
2513	1663	1953		1822	1747	1988	1528	1567	1323
100	115	99		91	92	115	99	103	91
2413	1548	1854		1731	1655	1873	1429	1464	1232
162	102	107		88	81	110	131	149	176
6.7	6.6	5.8		5.1%	4.9%	5.8%	5.3%	9.9%	14.3%

546	4	3	2	1	6	485	3	2	1
1159-6									
1229-5	1230	1224	1224	1189	1201	2506	1208	1197	1202
2380				508					
1387	613	496			513	1695	607	547	614
993	617	728		681	688	811	601	650	588
76°	76°	74°	76°	83°	83°	78°	77	76°	75°
8708	8708	8715		8681	8681	8700	8704	8708	8712
1140	708	832		785	791	935	689	746	667
2.12	2.20	2.22		2.21	2.09	2.00	2.08	1.98	1.85

Base Co. Rd. "H"

Sub base

6-28-58	6-28-58	6-28-58	6-28-58	6-26-58	6-26-58	6-26-58	6-26-58	6-26-58	6-23-58
532+00	540+00	548+00	555+00	452+00	452+00	462+00	468+00	474+00	468+00
11' Lt.	♀	11' Rt.	11' Lt.	11 1/2 Lt.	11 1/2 Rt.	♀	11 1/2 Lt.	11' Rt.	11 1/2 Lt.
6"	5 1/4"	6 1/2"	7"	4"	4"	4"	4"	4"	4"
2170	1495	1641	2134	1850	1583	1358	1492	1464	1177
2075	1417	1549	2015	1731	1393	1273	1353	1317	1062
115	99	103	91	115	99	102	90	92	105
1985	1318	1446	1924	1616	1294	1171	1263	1225	957
195	78	82	119	719	190	85	139	147	115
4.8%	5.3%	6.3	6.2%	7.4%	14.7%	7.5	11.0%	12.0%	10.8%
4.5	3	2	1.46	4	3	2	1	6	5
2488	1208	1220	2378	1214	1170	1228	1226	1197	1214
1861	609	639	1462	566	549	720	658	635	760
821	599	581	916	648	621	508	568	562	435
83°	83°	77°	69°	76°	75°	75°	74°	73°	73°
2068	8681	8704	8733	8709	8742	8712	8715	8719	8717
250	691	663	1024	741	712	581	649	645	500
206	1.89	2.17	1.92	2.17	1.82	202	1.96	1.90	1.84

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See Page 70
Page 69-71.

Same place

Rock
June 20 - 1960

10.670

Co. Rd. "H" Subbase

6-23-58	6-20-58	6-20-58	6-20-58	6-18-58
474+00	480+00	510+00	516+00	498+00
11 1/2 R	♀	11 1/2 L	♀	♀
4"	4"	4"	4"	4"
1248	1462	1124	1402	1151
1124	1366	1002	1288	1076
145	99	102	90	90
1009	1267	900	1198	986
124	96	122	114	75
12.3%	7.6%	13.6	9.6	7.6%

4	3	2	1	.1
1221	1235	1235	1238	1290
737	670	826	721	840
484	565	409	517	450
73	67	63°	62°	82°
8712	8741	8755	8760	8685
553	648	467	589	520
182	1.96	1.93	2.03	1.90

see Right
side of
Page 72

Rock
June 19 9.6%

6-18-58	6-18-58	6-18-58	6-18-58
492+00	486+00	510+25	510700
11 1/2 L	11 1/2 R	11 1/2 L	11 1/2 L
4"	4"	4"	4"
1167	1321	1332	1138
1086	1177	1160	987
109	115	99	102
977	1062	1061	885
81	144	172	151
8.3%	13.5%	15.2%	17.0%

5	4	3	2
1267	1276	1264	1289
851	773	742	847
416	503	522	442
82°	86°	73°	70°
8685	8670	8719	8732
480	581	600	508
2.03	1.83	1.76	1.75

see left of
Page

Rock
1697
1535
162

June 18 Rock 12.6%

Co. Rd. "H"

Subbase ✓

6/18/58 6-17-58 6-17-58 6-17-58 6-17-58
 516+00 504+00 510+00 516+00 522+00

£ 11½ R 11½ L £ 11½ R
 4" 4" 4" 4" 4"

1181 1116 1046 1293 1251
 1059 1006 937 1201 1134
 90 92 100 105 99
 969 914 837 1086 1035
 122 110 109 92 117
 12.6% 11.0% 13.0% 7.7% 10.7

1 6 5 4 3

1269 1223 1264 1249 1267
 805 808 859 701 817
 464 415 405 548 450
 68° 66° 64° 64° 66°
 .8737 .8745 .8752 .8752 .8745
 530 474 462 669 513
 1.84 1.92 1.81 1.63 2.01

See Left
 Side of
 Page 73

See Left
 Side Page
 #73

74

Co. Rd. "H"

6-17-58 6-17-58 6-17-58 6-17-58 June 58
 528+00 534+00 540+00 546+00 552+00

11½ L £ 11½ R 11½ L £
 4" 4" 4" 4" 4"

1322 1272 1120 1238 1285
 1203 1153 1048 1156 1163
 102 90 99 102 115
 1101 1063 949 1054 1048
 119 119 72 82 122
 10.7% 11.2% 7.6% 5.7% 11.1%

2 1 3 2 4

1268 1262 1244 1255 1259
 781 759 837 822 802
 487 503 407 433 457
 62° 62° 72° 62° 66°
 .8763 .8763 .8728 .8763 .8745
 545 578 466 495 522
 2.04 1.84 2.03 2.13 2.00

Dents

Sta.
 Distance
 From £

Depth
 Wet. Wt. Pan
 of Sample
 Dry Wt. Pan
 & Sample

Wt. Pan

Dry

Loss
 % of Dry

Oil
 Bottle

Full Wt.
 Wt. of B. Pan
 after used

Wt. used

Temp.

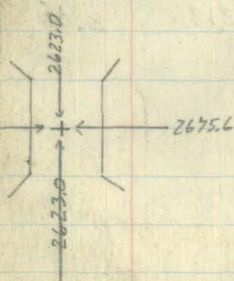
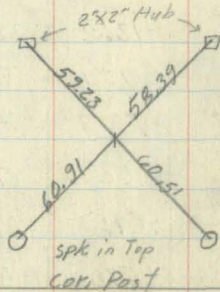
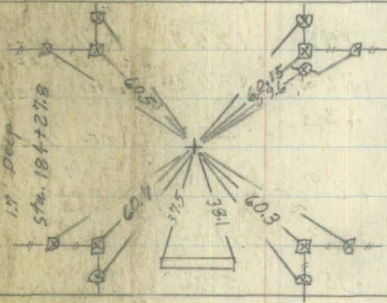
Cor.

Cor.

100%
 of Product

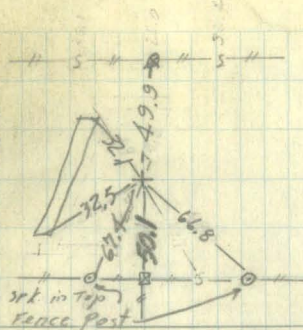
N¹/₄ Cor. 24-87-14
Sta. 157452.2

sta. 345+54.5



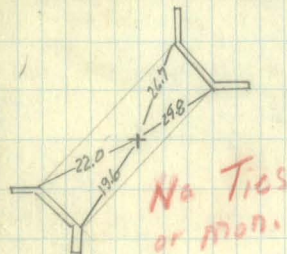
N 1/4 cor, 21-87-13

Sta. 319+26.2



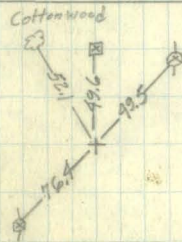
N.E. Cor. 20-07-13

sta 292+98.5



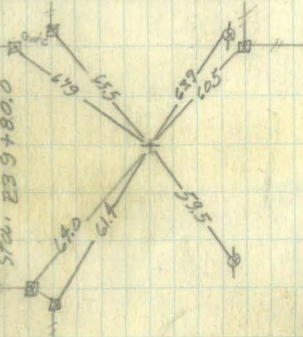
N. 1/4 Cor 20-87-13

Star. 266 + 39.9

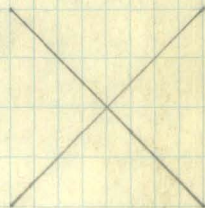
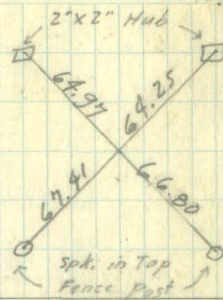


N. E. Cor. 19-87-13

15" Deep
Stew, 239+80.0



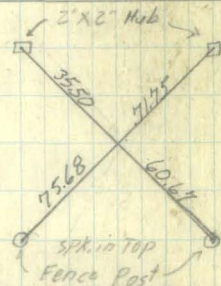
75



No Ties
or Mon.

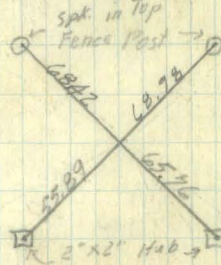
N. 1/4 Cor 20-87-13

Star. 266 + 39.9

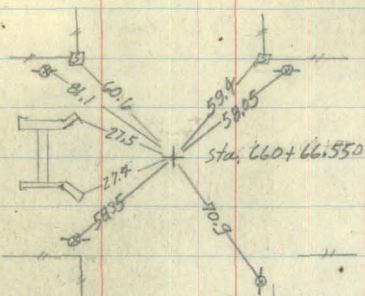


N. E. Cor. 19-87-13

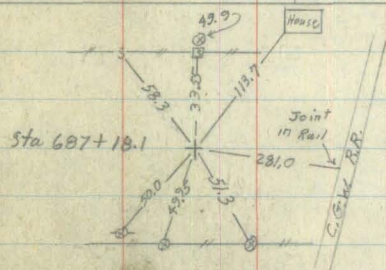
15" Deep
Stew, 239+80.0



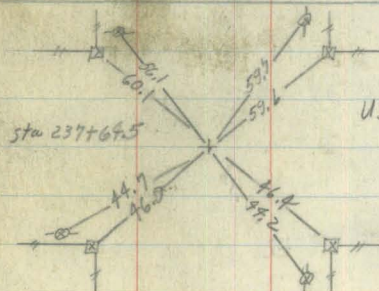
N.E. Cor. 31-90-11



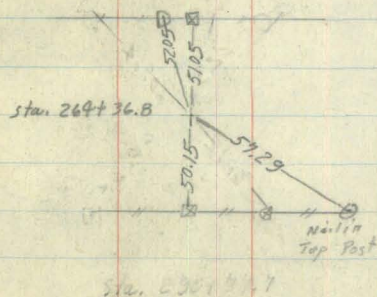
N 1/4 Cor. 32-90-11



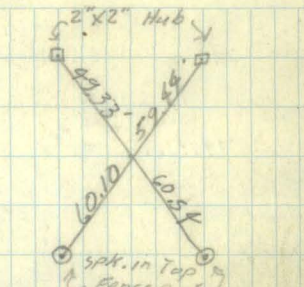
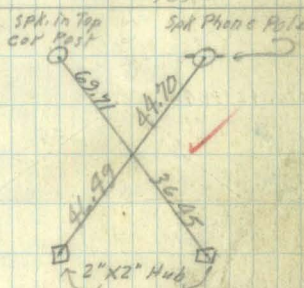
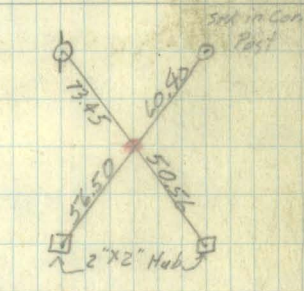
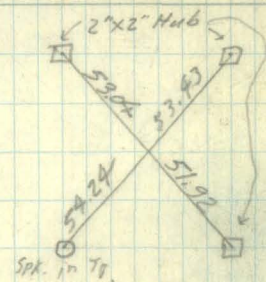
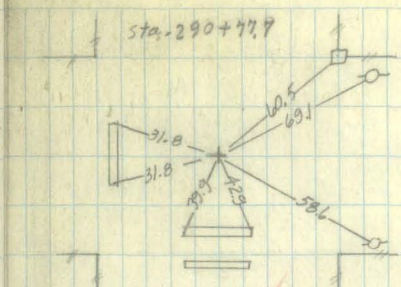
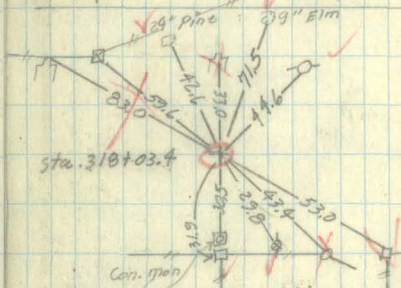
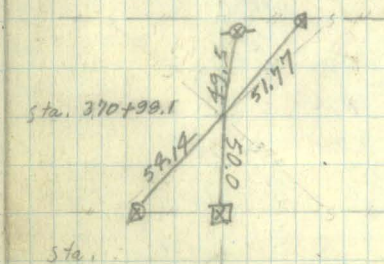
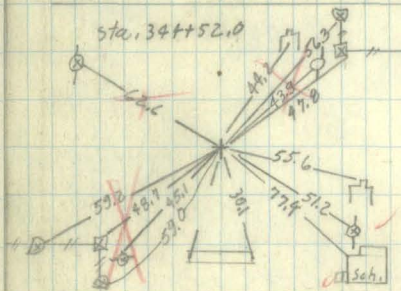
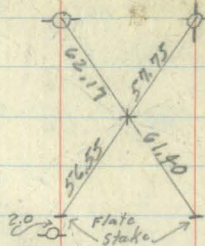
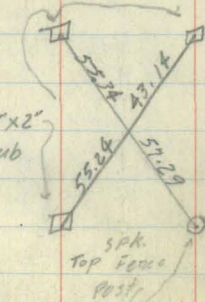
N.E. Cor. 35-90-13



N 1/4 Cor. 36-90-13



US #63

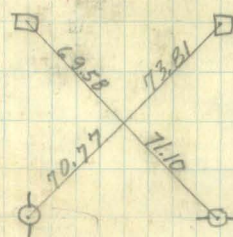
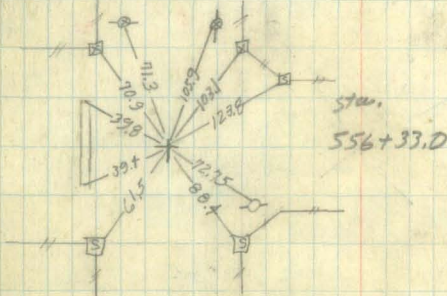
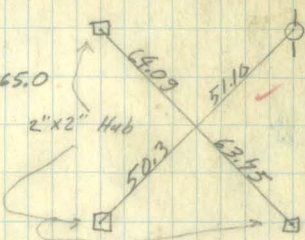
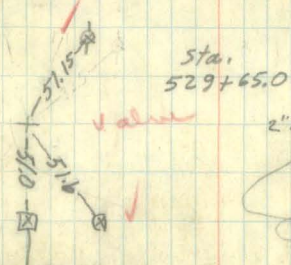
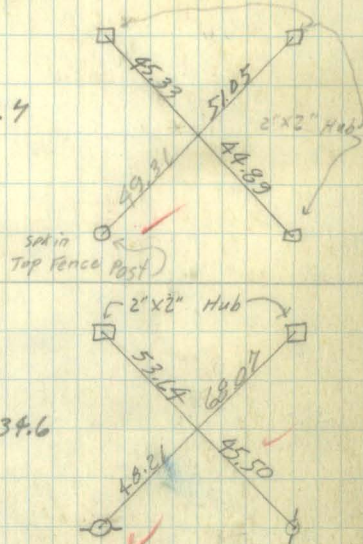
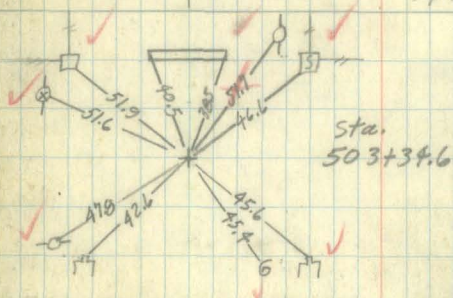
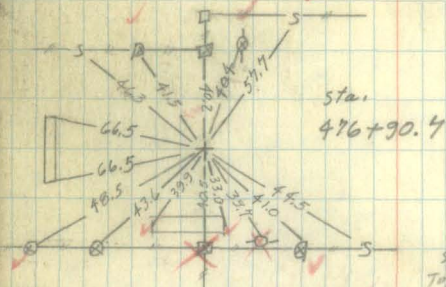
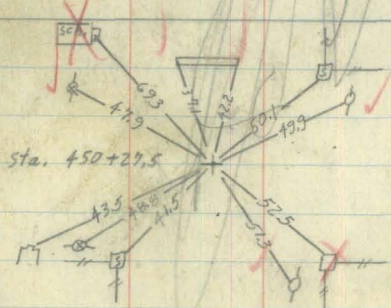
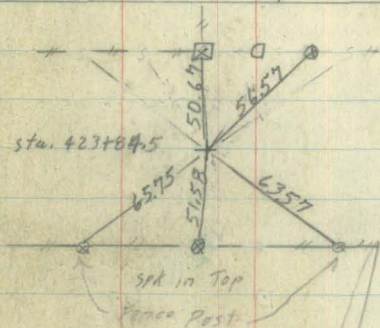
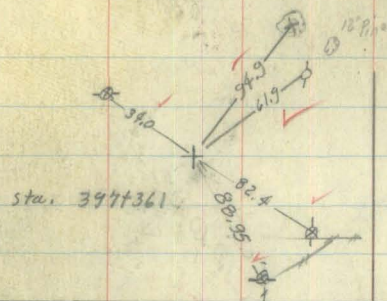


N 1/4 Cor. 32-90-12

N.E. Cor. 31-90-12

N 1/4 Cor. 31-90-12

N.E. Cor. 36-90-13



IMPROVED TABLES AND INFORMATION

HORIZONTAL STADIA CORRECTIONS

2°—00' — 0.1	21°—00' — 12.3	33°—00' — 29.7
3°—00' — 0.3	21°—30' — 13.4	33°—15' — 30.1
4°—00' — 0.5	22°—00' — 14.0	33°—30' — 30.5
5°—00' — 0.8	22°—30' — 14.7	33°—45' — 30.9
6°—00' — 1.1	23°—00' — 15.3	34°—00' — 31.3
7°—00' — 1.5	23°—30' — 15.9	34°—15' — 31.7
8°—00' — 1.9	24°—00' — 16.5	34°—30' — 32.1
9°—00' — 2.5	24°—30' — 17.2	34°—45' — 32.5
10°—00' — 3.0	25°—00' — 17.9	35°—00' — 32.9
10°—30' — 3.3	25°—30' — 18.6	35°—15' — 33.3
11°—00' — 3.6	26°—00' — 19.2	35°—30' — 33.7
11°—30' — 4.0	26°—30' — 19.9	35°—45' — 34.1
12°—00' — 4.3	27°—00' — 20.6	36°—00' — 34.6
12°—30' — 4.7	27°—30' — 21.3	36°—15' — 35.0
13°—00' — 5.1	28°—00' — 22.0	36°—30' — 35.4
13°—30' — 5.5	28°—30' — 22.8	36°—45' — 35.8
14°—00' — 5.9	29°—00' — 23.5	37°—00' — 36.2
14°—30' — 6.3	29°—30' — 24.3	37°—15' — 36.6
15°—00' — 6.7	30°—00' — 25.0	37°—30' — 37.1
15°—30' — 7.2	30°—15' — 25.4	37°—45' — 37.5
16°—00' — 7.6	30°—30' — 25.8	38°—00' — 37.9
16°—30' — 8.1	30°—45' — 26.2	38°—15' — 38.3
17°—00' — 8.5	31°—00' — 26.5	38°—30' — 38.7
17°—30' — 9.0	31°—15' — 26.9	38°—45' — 39.1
18°—00' — 9.5	31°—30' — 27.3	39°—00' — 39.6
18°—30' — 10.1	31°—45' — 27.7	39°—15' — 40.0
19°—00' — 10.6	32°—00' — 28.1	39°—30' — 40.5
19°—30' — 11.2	32°—15' — 28.5	
20°—00' — 11.7	32°—30' — 28.9	
20°—30' — 12.3	32°—45' — 29.3	

Chains to Feet

1	66
2	132
3	198
4	264
5	330
6	396
7	462
8	528
9	594
10	660

Feet to Chains

100	1.515
200	3.030
300	4.545
400	6.060
500	7.575
600	9.090
700	10.606
800	12.121
900	13.636
1,000	15.151

DIRECTIONS FOR USE OF TABLES

TABLE No. 1.

Distance of slope stake from side or shoulder stake for any width roadway, slope $1\frac{1}{2}$ to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

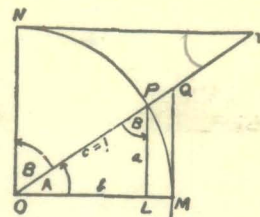
TABLE No. 9.

To find Tangent and External for curve of any other degree, divide by degree of curve and add correction found in column of corrections.

Degree of curve with a given I may be found by dividing tangent, (or external), opposite I by given tangent, (or external).

The distance from a point on the tangent to the curve is very nearly the square of the tangent length divided by twice the radius.

$$\begin{array}{r}
 211 \\
 692 \overline{)1353} \\
 \underline{1264} \\
 690 \\
 \underline{642} \\
 480 \\
 \underline{211} \\
 730 \overline{)1550} \\
 \underline{1460} \\
 900 \\
 \underline{730} \\
 170
 \end{array}$$



$$\begin{array}{r}
 992 \\
 493 \\
 \hline
 1485
 \end{array}$$

TABLE II

TRIGONOMETRIC FORMULÆ.

$$\angle A = \angle MOP \quad \angle B = \angle PON = \angle OPL$$

$$R = OP = c = 1$$

$$\sin A = \frac{a}{c} = \frac{a}{1} = a = \cos B = LP$$

$$\cos A = \frac{b}{c} = \frac{b}{1} = b = \sin B = OL$$

$$\tan A = \frac{a}{b} = \frac{MQ}{OM} = \frac{MQ}{1} = MQ = \cot B = MQ$$

$$\cot A = \frac{NT}{ON} = \frac{NT}{1} = NT = \tan B = NT$$

$$\sec A = \frac{OQ}{OM} = \frac{OQ}{1} = OQ = \csc B = OQ$$

$$\csc A = \frac{OT}{ON} = \frac{OT}{1} = OT = \sec B = OT$$

$$\text{vers } A = \frac{LM}{OP} = LM = \text{covers } B \#$$

$$\text{covers } A = \frac{OP - LP}{OP} = OP - LP = \text{vers } B$$

$$\text{exsec } A = PQ = \text{coexsec } B$$

$$\text{coexsec } A = PT = \text{exsec } B$$

$$\sin \frac{1}{2} A = \sqrt{\frac{1 - \cos A}{2}} \quad \cos \frac{1}{2} A = \sqrt{\frac{1 + \cos A}{2}}$$

$$\sin 2A = 2 \sin A \cos A \quad \cos 2A = \cos^2 A - \sin^2 A$$

$$\text{Law of Sines} \quad \frac{\sin A}{a} = \frac{\sin B}{b} = \frac{\sin C}{c}$$

$$\text{Law of Cosines} \quad c^2 = a^2 + b^2 - 2ab \cos C$$

$$\text{Law of Tangents} \quad \frac{a+b}{a-b} = \frac{\tan \frac{1}{2}(A+B)}{\tan \frac{1}{2}(A-B)}$$

$$\begin{array}{r}
 2135 \\
 621 \overline{)1326} \\
 \underline{1242} \\
 840 \\
 \underline{621} \\
 219 \\
 \underline{1883} \\
 3270 \\
 \underline{3255}
 \end{array}$$

TABLE II—Continued
TRIGONOMETRIC FORMULAE (continued)

In any triangle:

Given a, b, C; to find c, B, A.

Use Law of Sines.

Given A, B, c; to find a, b, C.

Use Law of Sines.

Given a, b, c; to find A, B, C.

$$\text{Let } \frac{a+b+c}{2} = s, \sqrt{\frac{(s-a)(s-b)(s-c)}{s}} = r$$

$$\cos \frac{1}{2} A = \sqrt{\frac{s(s-a)}{bc}}$$

$$\tan \frac{1}{2} A = \frac{r}{s-a}$$

$$\tan \frac{1}{2} B = \frac{r}{s-b}$$

$$\tan \frac{1}{2} C = \frac{r}{s-c}$$

Area of a triangle:

$$\text{Area} = \frac{1}{2} ab \sin C$$

$$\text{Area} = \sqrt{s(s-a)(s-b)(s-c)}$$

PRISMOIDAL FORMULA.

$$\text{Vol.} = \frac{h}{6} (B + b + 4M)$$

h = altitude; b, B = bases; M = midsection

TABLE III
INCHES AND FRACTIONS OF AN INCH IN DECIMALS OF A FOOT

	0	1	2	3	4	5	6	7	8	9	10	11	
$\frac{1}{16}$	.0052	.0885	.1719	.2552	.3385	.4219	.5052	.5885	.6719	.7552	.8385	.9219	$\frac{1}{16}$
$\frac{1}{8}$	.0104	.0938	.1771	.2604	.3438	.4271	.5104	.5938	.6771	.7604	.8438	.9271	$\frac{1}{8}$
$\frac{3}{16}$	.0156	.0990	.1823	.2656	.3490	.4323	.5156	.5990	.6823	.7656	.8490	.9323	$\frac{3}{16}$
$\frac{1}{4}$	.0208	.1042	.1875	.2708	.3542	.4375	.5208	.6042	.6875	.7708	.8542	.9375	$\frac{1}{4}$
$\frac{5}{16}$	.0260	.1094	.1927	.2760	.3594	.4427	.5260	.6094	.6927	.7760	.8594	.9427	$\frac{5}{16}$
$\frac{3}{8}$	.0313	.1146	.1979	.2813	.3646	.4479	.5313	.6146	.6979	.7813	.8646	.9479	$\frac{3}{8}$
$\frac{7}{16}$	.0365	.1198	.2031	.2865	.3698	.4531	.5365	.6198	.7031	.7865	.8698	.9531	$\frac{7}{16}$
$\frac{1}{2}$	.0417	.1250	.2083	.2917	.3750	.4583	.5417	.6250	.7083	.7917	.8750	.9583	$\frac{1}{2}$
$\frac{9}{16}$	.0469	.1302	.2135	.2969	.3803	.4635	.5469	.6302	.7135	.7969	.8802	.9635	$\frac{9}{16}$
$\frac{5}{8}$	.0521	.1354	.2188	.3021	.3854	.4688	.5521	.6354	.7188	.8021	.8854	.9688	$\frac{5}{8}$
$\frac{11}{16}$	.0573	.1406	.2240	.3073	.3906	.4740	.5573	.6406	.7240	.8073	.8906	.9740	$\frac{11}{16}$
$\frac{3}{4}$	.0625	.1458	.2292	.3125	.3958	.4792	.5625	.6458	.7292	.8125	.8958	.9792	$\frac{3}{4}$
$\frac{7}{8}$	.0677	.1510	.2344	.3177	.4010	.4844	.5677	.6510	.7344	.8177	.9010	.9844	$\frac{7}{8}$
$\frac{15}{16}$	.0729	.1563	.2396	.3229	.4063	.4896	.5729	.6563	.7396	.8229	.9063	.9896	$\frac{15}{16}$
1	.0781	.1615	.2448	.3281	.4115	.4948	.5781	.6615	.7448	.8281	.9115	.9948	1
	.0833	.1667	.2500	.3333	.4167	.5000	.5833	.6667	.7500	.8333	.9167	1.000	
	0	1	2	3	4	5	6	7	8	9	10	11	

TABLE IV
USEFUL RELATIONS.

Lineal feet	×.00019	= miles
Lineal yards	×.0006	= miles
Square inches	×.007	= square feet
Square feet	×.111	= square yards
Square yards	×.0002067	= acres
Acres	×4840	= square yards
Cubic inches	×.00058	= cubic feet
Cubic feet	×.03704	= cubic yards
Links	×.22	= yards
Links	×.66	= feet
Feet	×1.5	= links

$$360^\circ = 21600' = 1296000''$$

$$\text{Radius} = \text{arc of } 57.2957790^\circ$$

$$\text{Arc of } 1^\circ (\text{radius} = 1) = .017453292$$

$$\text{Arc of } 1' (\text{radius} = 1) = .000290888$$

$$\text{Arc of } 1'' (\text{radius} = 1) = .000004848$$

$$\pi = 3.141592654$$

$$\sqrt{\frac{1}{\pi}} = 0.564190$$

$$\frac{\pi}{4} = 0.785398163$$

$$\sqrt{\frac{6}{\pi}} = 1.240700982$$

$$\frac{\pi}{6} = 0.523598776$$

$$\pi^2 = 9.869604401$$

$$\sqrt{\frac{4}{\pi}} = 1.128379167$$

$$\frac{1}{\pi^2} = 0.101321184$$

$$\frac{\pi}{6} = 0.523598776$$

$$\sqrt{\pi} = 1.772453851$$

$$\frac{4\pi}{3} = 4.188790205$$

$$\frac{1}{\pi} = 0.3183099$$

Curvature of Earth's surface = about 0.7 feet in 1 mile

Curvature in feet = 0.667 (Dist. in miles)²

Difference between arc and chord length, 0.05 feet in $11\frac{1}{2}$ miles

$$\text{Probable error of a single observation} = 0.6754 \sqrt{\frac{\sum v^2}{n-1}}$$

Error in chaining of 0.01 feet in 100 feet:

Due to—

1. Length of tape error of 0.01 feet
2. Alignment. One end 1.4 feet out of line
3. Sag of tape at centre of 0.61 feet.
4. Temperature difference of 15°
5. Difference of pull of 15 lbs.

STADIA REDUCTION FORMULAE

Horizontal Distance = $R - R \sin^2 a + C \cos a$

Vertical Distance = $R \frac{1}{2} \sin 2a + C \sin a$

$R = \text{Reading} \times \frac{\text{distance from Object glass to cross hairs}}{\text{distance between cross hairs}}$

C = distance from Object glass to cross hairs + distance from Object glass to center of instrument.

a = angle of elevation for mid Reading

144
00058
11 52
720
08358
144
12
288
144
1728
00058
13824
8540
99224

TABLE VI (continued)
SINES, COSINES, TANGENTS, COTANGENTS (continued)

deg	sin 0'	tan 0'	sin 10'	tan 10'	sin 20'	tan 20'	sin 30'	tan 30'	sin 40'	tan 40'	sin 50'	tan 50'	deg
46	7193	1.0355	7214	1.0416	7234	1.0477	7254	1.0533	7274	1.0599	7294	1.0661	43
47	314	.0724	333	.0786	353	.0850	373	.0913	392	.0977	412	.1041	42
48	431	.1106	451	.1171	470	.1237	490	.1303	509	.1369	528	.1436	41
49	547	.1504	566	.1571	585	.1640	604	.1708	623	.1778	642	.1847	40
50	660	1.1918	7679	1.1988	7698	1.2059	7716	1.2131	7735	1.2203	7753	1.2276	39
51	771	.2349	790	.2423	808	.2497	826	.2572	844	.2647	862	.2723	38
52	880	.2799	898	.2876	916	.2954	934	.3032	951	.3111	969	.3190	37
53	986	.3270	8004	.3351	8021	.3452	8039	.3514	8056	.3597	8073	.3680	36
54	8090	.3764	107	.3848	124	.3934	141	.4019	158	.4106	175	.4193	35
55	192	.4281	208	.4370	225	.4460	241	.4550	258	.4641	274	.4733	34
56	290	.4826	307	.4919	323	.5013	339	.5108	355	.5204	371	.5301	33
57	387	.5399	403	.5497	418	.5597	434	.5697	450	.5798	465	.5900	32
58	480	.6003	496	.6107	511	.6212	526	.6319	542	.6426	557	.6534	31
59	572	.6643	587	.6753	601	.6864	616	.6977	631	.7090	646	.7205	30
60	660	1.7321	8675	1.7437	8689	1.7556	8704	1.7675	8718	1.7797	8732	1.7917	29
61	746	.8040	760	.8165	774	.8291	788	.8418	802	.8546	816	.8676	28
62	829	.8807	843	.8940	857	.9074	870	.9210	884	.9347	897	.9486	27
63	910	.9626	923	.9768	936	.9912	949	2.0057	962	2.0204	975	2.0353	26
64	988	2.0503	9001	2.0655	9013	2.0809	9026	.0965	9038	.1123	9051	.1283	25
65	9063	.1445	075	.1609	088	.1775	100	.1943	112	.2113	124	.2286	24
66	135	.2460	147	.2637	159	.2817	171	.2998	182	.3183	194	.3369	23
67	205	.3559	216	.3750	228	.3945	239	.4142	250	.4342	261	.4545	22
68	272	.4751	283	.4960	293	.5172	304	.5386	315	.5605	325	.5826	21
69	336	.6051	346	.6279	356	.6511	367	.6746	377	.6985	387	.7228	20
70	397	2.7475	9407	2.7725	9417	2.7980	9426	2.8239	9436	2.8502	9446	2.8770	19
71	455	.9042	465	.9319	474	.9600	483	.9887	492	3.0178	502	3.0475	18
72	511	3.0777	520	3.1084	528	3.1397	537	3.1716	546	.2041	555	.2371	17
73	563	.2709	572	.3052	580	.3402	588	.3759	596	.4124	605	.4495	16
74	613	.4874	621	.5261	628	.5656	636	.6059	644	.6470	652	.6891	15
75	659	.7321	667	.7760	674	.8208	681	.8657	689	.9136	696	.9617	14
76	703	4.0108	710	4.0611	717	4.1126	724	4.1653	730	4.2193	737	4.2747	13
77	744	.3315	750	.3897	757	.4494	763	.5107	769	.5736	775	.6382	12
78	781	.7046	787	.7729	793	.8430	799	.9152	805	.9894	811	5.0658	11
79	816	.1446	822	5.2257	827	5.3093	833	5.3955	838	5.4845	843	.5764	10
80	9848	5.6713	9853	5.7694	9858	5.8708	9863	5.9758	9868	6.0844	9872	6.1970	9
81	877	6.3138	881	6.4348	886	6.5606	890	6.6912	894	.8269	899	.9682	8
82	903	7.1154	907	7.2687	911	7.4287	914	7.5958	918	7.7704	922	7.9530	7
83	925	8.1443	929	8.3450	932	8.5555	936	8.7769	939	9.0098	942	9.2553	6
84	945	9.5144	948	9.7882	951	10.078	954	10.385	957	10.711	959	11.059	5
85	962	11.430	964	11.826	967	12.250	969	12.706	971	13.197	974	13.727	4
86	976	14.300	978	14.924	980	15.605	981	16.350	983	17.169	985	18.075	3
87	986	19.081	988	20.206	989	21.470	990	22.903	992	24.542	993	26.432	2
88	994	28.636	995	31.242	996	34.368	997	38.189	997	42.964	998	49.104	1
89	9998	57.290	9999	68.750	9999	85.940	9999	114.58	1.000	171.88	1.000	343.77	0
90	60'	60'	50'	50'	40'	40'	30'	30'	20'	20'	10'	10'	deg
90	cos	cot	cos	cot	cos	cot	cos	cot	cos	cot	cos	cot	deg

TABLE VII
RODS IN FEET, 10THS AND 100THS OF FEET

Rods	Feet	Rods	Feet	Rods	Feet	Rods	Feet	Rods	Feet
1	16.50	21	346.50	41	676.50	61	1006.50	81	1336.50
2	33.00	22	363.00	42	693.00	62	1023.00	82	1353.00
3	49.50	23	379.50	43	709.50	63	1039.50	83	1369.50
4	66.00	24	396.00	44	726.00	64	1056.00	84	1386.00
5	82.50	25	412.50	45	742.50	65	1072.50	85	1402.50
6	99.00	26	429.00	46	759.00	66	1089.00	86	1419.00
7	115.50	27	445.50	47	775.50	67	1105.50	87	1435.50
8	132.00	28	462.00	48	792.00	68	1122.00	88	1452.00
9	148.50	29	478.50	49	808.50	69	1138.50	89	1468.50
10	165.00	30	495.00	50	825.00	70	1155.00	90	1485.00
11	181.50	31	511.50	51	841.50	71	1171.50	91	1501.50
12	198.00	32	528.00	52	858.00	72	1188.00	92	1518.00
13	214.50	33	544.50	53	874.50	73	1204.50	93	1534.50
14	231.00	34	561.00	54	891.00	74	1221.00	94	1551.00
15	247.50	35	577.50	55	907.50	75	1237.50	95	1567.50
16	264.00	36	594.00	56	924.00	76	1254.00	96	1584.00
17	280.50	37	610.50	57	940.50	77	1270.50	97	1600.50
18	297.00	38	627.00	58	957.00	78	1287.00	98	1617.00
19	313.50	39	643.50	59	973.50	79	1303.50	99	1633.50
20	330.00	40	660.00	60	990.00	80	1320.00	100	1650.00

TABLE VIII
LINKS IN FEET, 10THS AND 100THS OF FEET

Links	Feet	Links	Feet	Links	Feet	Links	Feet	Links	Feet	Links	Feet
1	0.66	18	11.88	35	23.10	52	34.32	69	45.54	86	56.76
2	1.32	19	12.54	36	23.76	53	34.98	70	46.20	87	57.42
3	1.98	20	13.20	37	24.42	54	35.64	71	46.86	88	58.08
4	2.64	21	13.86	38	25.08	55	36.30	72	47.52	89	58.74
5	3.30	22	14.52	39	25.74	56	36.96	73	48.18	90	59.40
6	3.96	23	15.18	40	26.40	57	37.62	74	48.84	91	60.06
7	4.62	24	15.84	41	27.06	58	38.28	75	49.50	92	60.72
8	5.28	25	16.50	42	27.72	59	38.94	76	50.16	93	61.38
9	5.94	26	17.16	43	28.38	60	39.60	77	50.82	94	62.04
10	6.60	27	17.82	44	29.04	61	40.26	78	51.48	95	62.70
11	7.26	28	18.48	45	29.70	62	40.92	79	52.14	96	63.36
12	7.92	29	19.14	46	30.36	63	41.58	80	52.80	97	64.02
13	8.58	30	19.80	47	31.02	64	42.24	81	53.46	98	64.68
14	9.24	31	20.46	48	31.68	65	42.90	82	54.12	99	65.34
15	9.90	32	21.12	49	32.34	66	43.56	83	54.78	100	66.00
16	10.56	33	21.78	50	33.00	67	44.22	84	55.44	101	66.66
17	11.22	34	22.44	51	33.66	68	44.88	85	56.10	102	67.32

TABLE IX. TANGENTS AND EXTERNALS TO A 1° CURVE

I	T	E	I=10°	I	T	E	I=20°	I	T	E	I=30°
1°	50.00	.218	+	11°	551.70	26.500	+	21°	1061.9	97.577	+
10'	58.34	.297	5° C.	10'	560.11	27.313	5° C.	10'	1070.6	99.155	5° C.
20'	66.67	.388		20'	568.53	28.137		20'	1079.2	100.75	
30'	75.01	.491		30'	576.95	28.974		30'	1087.8	102.35	T
40'	83.34	.606	.03	40'	585.36	29.824	.06	40'	1096.4	103.97	.10
50'	91.68	.733	E	50'	593.79	30.686	E	50'	1105.1	105.60	E
2°	100.01	.873	.001	12°	602.21	31.561	.006	22°	1113.7	107.24	.013
10'	108.35	1.024		10'	610.64	32.447		10'	1122.4	108.90	
20'	116.68	1.188		20'	619.07	33.347		20'	1131.0	110.57	
30'	125.02	1.364		30'	627.50	34.259		30'	1139.7	112.25	
40'	133.36	1.552		40'	635.93	35.183		40'	1148.4	113.95	
50'	141.70	1.752		50'	644.37	36.120		50'	1157.0	115.66	
3°	150.04	1.964	10° C.	13°	652.81	37.070	10° C.	23°	1165.7	117.38	10° C.
10'	158.38	2.188	T	10'	661.25	38.031	T	10'	1174.4	119.12	T
20'	166.72	2.425	.06	20'	669.70	39.006	.13	20'	1183.1	120.87	.19
30'	175.06	2.674	.03	30'	678.15	39.993	.13	30'	1191.8	122.63	E
40'	183.40	2.934	.003	40'	686.60	40.992	.011	40'	1200.5	124.41	E
50'	191.74	3.207		50'	695.06	42.004		50'	1209.2	126.20	.025
4°	200.08	3.492		14°	703.51	43.029		24°	1217.9	128.00	
10'	208.43	3.790		10'	711.97	44.066		10'	1226.6	129.82	
20'	216.77	4.099		20'	720.44	45.116		20'	1235.3	131.65	
30'	225.12	4.421		30'	728.90	46.178		30'	1244.0	133.50	
40'	233.47	4.755		40'	737.37	47.253		40'	1252.8	135.35	
50'	241.81	5.100	15° C.	50'	745.85	48.341	15° C.	50'	1261.5	137.23	15° C.
5°	250.16	5.459	T	15°	754.32	49.441	T	25°	1270.2	139.11	T
10'	258.51	5.829	.09	10'	762.80	50.554	.19	10'	1279.0	141.01	.29
20'	266.86	6.211		20'	771.29	51.679		20'	1287.7	142.93	E
30'	275.21	6.606	.004	30'	779.77	52.818	.017	30'	1296.5	144.85	.038
40'	283.57	7.013		40'	788.26	53.969		40'	1305.3	146.75	
50'	291.92	7.432		50'	796.75	55.132		50'	1314.0	148.75	
6°	300.28	7.863		16°	805.25	56.309		26°	1322.8	150.71	
10'	308.64	8.307		10'	813.75	57.498		10'	1331.6	152.69	
20'	316.99	8.762		20'	822.25	58.699		20'	1340.4	154.69	
30'	325.35	9.230	20° C.	30'	830.76	59.914	20° C.	30'	1349.2	156.70	20° C.
40'	333.71	9.710	T	40'	839.27	61.141	T	40'	1358.0	158.72	T
50'	342.08	10.202	.13	50'	847.78	62.381	.26	50'	1366.8	160.76	.39
7°	350.44	10.707	E	17°	856.30	63.634	E	27°	1375.6	162.81	E
10'	358.81	11.224	.006	10'	864.82	64.900	.022	10'	1384.4	164.86	.051
20'	367.17	11.753		20'	873.35	66.178		20'	1393.2	166.95	
30'	375.54	12.294		30'	881.88	67.470		30'	1402.0	169.04	
40'	383.91	12.847		40'	890.41	68.774		40'	1410.9	171.15	
50'	392.28	13.413		50'	898.95	70.091		50'	1419.7	173.27	
8°	400.66	13.991		18°	907.49	71.421		28°	1428.6	175.41	
10'	409.03	14.582	25° C.	10'	916.03	72.764	25° C.	10'	1437.4	177.55	25° C.
20'	417.41	15.184	T	20'	924.58	74.119	T	20'	1446.3	179.72	T
30'	425.79	15.799	.16	30'	933.13	75.488	.32	30'	1455.1	181.89	.49
40'	434.17	16.426	E	40'	941.69	76.869	E	40'	1464.0	184.08	E
50'	442.55	17.065		50'	950.25	78.264		50'	1472.9	186.29	
9°	450.93	17.717	.007	19°	958.81	79.671	.028	29°	1481.8	188.51	.065
10'	459.32	18.381		10'	967.38	81.092		10'	1490.7	190.74	
20'	467.71	19.058		20'	975.96	82.525		20'	1499.6	192.99	
30'	476.10	19.746		30'	984.53	83.972		30'	1508.5	195.25	
40'	484.49	20.447		40'	993.12	85.431		40'	1517.4	197.53	
50'	492.88	21.161	30° C.	50'	1001.7	86.904	30° C.	50'	1526.3	199.82	30° C.
10°	501.28	21.887	T	20°	1010.3	88.389	T	30°	1535.3	202.12	T
10'	509.68	22.624	.19	10'	1018.9	89.888	.39	10'	1544.2	204.44	.59
20'	518.08	23.375	E	20'	1027.5	91.399	E	20'	1553.1	206.77	.80
30'	526.48	24.138		30'	1036.1	92.924		30'	1562.1	209.12	E
40'	534.89	24.913	.008	40'	1044.7	94.462	.034	40'	1571.0	211.48	.141
50'	543.29	25.700		50'	1053.3	96.013		50'	1580.0	213.86	.078

T = R tan ½ I

E = R exsec ½ I

TABLE IX. TANGENTS AND EXTERNALS TO A 1° CURVE

I	T	E	I=40°	I	T	E	I=50°	I	T	E	I=60°
31°	1589.0	216.3	+	41°	2142.2	387.4	+	51°	2732.9	618.4	+
10'	1598.0	218.7	5° C.	10'	2151.7	390.7	5° C.	10'	2743.1	622.8	5° C.
20'	1606.9	221.1		20'	2161.2	394.1		20'	2753.4	627.2	
30'	1615.9	223.5	T	30'	2170.8	397.4	T	30'	2763.7	631.7	T
40'	1624.9	226.0	.13	40'	2180.3	400.8	.17	40'	2773.9	636.2	.21
50'	1633.9	228.4	E	50'	2189.9	404.2	E	50'	2784.2	640.7	E
32°	1643.0	230.9	.023	42°	2199.4	407.6	.037	52°	2794.0	645.2	.056
10'	1652.0	233.4		10'	2209.0	411.1		10'	2804.9	649.7	
20'	1661.0	235.9		20'	2218.6	414.5		20'	2815.2	654.3	
30'	1670.0	238.4		30'	2228.1	418.0		30'	2825.6	658.8	
40'	1679.1	241.0		40'	2237.7	421.4		40'	2835.9	663.4	
50'	1688.1	243.5		50'	2247.3	425.0		50'	2846.3	668.0	
33°	1697.2	246.1	10° C.	43°	2257.0	428.5	10° C.	53°	2856.7	672.7	10° C.
10'	1706.3	248.7	T	10'	2266.6	432.0	T	10'	2867.1	677.3	T
20'	1715.3	251.3	.26	20'	2276.2	435.6	.34	20'	2877.5	682.0	.42
30'	1724.4	253.9	E	30'	2285.9	439.2	E	30'	2888.0	686.7	E
40'	1733.5	256.5	.046	40'	2295.6	442.8	.075	40'	2898.4	691.4	.112
50'	1742.6	259.1		50	2305.2	446.4		50'	2908.9	696.1	
34°	1751.7	261.8		44°	2314.9	450.0		54°	2919.4	700.9	
10'	1760.8	264.5		10'	2324.6	453.6		10'	2929.9	705.7	
20'	1770.0	267.2		20'	2334.3	457.3		20'	2940.4	710.5	
30'	1779.1	269.9		30'	2344.1	461.0		30'	2951.0	715.3	
40'	1788.2	272.6		40'	2353.8	464.6		40'	2961.5	720.1	
50'	1797.4	275.3	15° C.	50'	2363.5	468.4	15° C.	50'	2972.1	725.0	15° C.
35°	1806.6	278.1	T	45°	2373.3	472.1	T	55°	2982.7	729.9	T
10'	1815.7	280.8	.40	10'	2383.1	475.8	.51	10'	2993.3	734.8	.63
20'	1824.9	283.6	E	20'	2392.8	479.6	E	20'	3003.9	739.7	E
30'	1834.1	286.4	.070	30'	2402.6	483.4	.116	30'	3014.5	744.6	.168
40'	1843.3	289.2		40'	2412.4	487.2		40'	3025.2	749.6	
50'	1852.5	292.0		50'	2422.3	491.0		50'	3035.8	754.6	
36°	1861.7	294.9		46°	2432.1	494.8		56°	3046.5	759.6	
10'	1870.9	297.7		10'	2441.9	498.7		10'	3057.2	764.6	
20'	1880.1	300.6		20'	2451.8	502.5		20'	3067.9	769.7	
30'	1889.4	303.5	20° C.	30'	2461.7	506.4	20° C.	30'	3078.7	774.7	20° C.
40'	1898.6	306.4	T	40'	2471.5	510.3	T	40'	3089.4	779.8	T
50'	1907.9	309.3	.53	50'	2481.4	514.3	.68	50'	3100.2	784.9	.84
37°	1917.1	312.2	E	47°	2491.3	518.2	E	57°	3110.9	790.1	E
10'	1926.4	315.2	.093	10'	2501.2	522.2	.151	10'	3121.7	795.2	.225
20'	1935.7	318.1		20'	2511.2	526.1		20'	3132.6	800.4	
30'	1945.0	321.1		30'	2521.1	530.1		30'	3143.4	805.6	
40'	1954.3	324.1		40'	2531.1	534.2		40'	3154.2	810.9	
50'	1963.6	327.1		50'	2541.0	538.2		50'	3165.1	816.1	
38°	1972.9	330.2		48°	2551.0	542.2		58°	3176.0	821.4	
10'	1982.2	333.2	25° C.	10'	2561.0	546.3	25° C.	10'	3186.9	826.7	25° C.
20'	1991.5	336.3	T	20'	2571.0	550.4	T	20'	3197.8	832.0	T
30'	2000.9	339.3	.67	30'	2581.0	554.5	.85	30'	3208.8	837.3	.105
40'	2010.2	342.4	E	40'	2591.0	558.6	E	40'	3219.7	842.7	E
50'	2019.6	345.5	.117	50'	2601.1	562.8	.189	50'	3230.7	848.1	.283
39°	2029.0	348.6		49°	2611.2	566.9		59°	3241.7	853.5	
10'	2038.4	351.8		10'	2621.2	571.1		10'	3252.7	858.9	
20'	2047.8	354.9		20'	2631.3	575.3		20'	3263.7	864.3	
30'	2057.2	358.1		30'	2641.4	579.5		30'	3274.8	869.8	
40'	2066.6	361.3		40'	2651.5	583.8		40'	3285.8	875.3	
50'	2076.0	364.5		50'	2661.6	588.0		50'	3296.9	880.8	
40°	2085.4	367.7	30° C.	50°	2671.8	592.3	30° C.	60°	3308.0	886.4	30° C.
10'	2094.9	371.0	T	10'	2681.9	596.6	T	10'	3319.1	892.0	T
20'	2104.3	374.2	.80	20'	2692.1	600.9	1.02	20'	3330.3	897.5	1.27
30'	2113.8	377.5	E	30'	2702.3	605.3	E	30'	3341.4	903.2	E
40'	2123.3	380.8	.141	40'	2712.5	609.6	.227	40'	3352.6	908.8	.340
50'	2132.7	384.1		50'	2722.7	614.0		50'	3363.8	914.5	

TABLE IX. TANGENTS AND EXTERNALS TO A 1° CURVE

I	T	E	I=70°	I	T	E	I=80°	I	T	E	I=90°
61°	3375.0	920.2	+ 5° C. T .25 E	71°	4086.9	1308.2	+ 5° C. T .30 E	81°	4893.6	1805.3	+ 5° C. T .36 E
10'	3386.3	925.9		10'	4099.5	1315.6		10'	4908.0	1814.7	
20'	3397.5	931.6		20'	4112.1	1322.9		20'	4922.5	1824.1	
30'	3408.8	937.3		30'	4124.8	1330.3		30'	4937.0	1833.6	
40'	3420.1	943.1		40'	4137.4	1337.7		40'	4951.5	1843.1	
50'	3431.4	948.9		50'	4150.1	1345.1		50'	4966.1	1852.6	
62°	3442.7	954.8	.080	72°	4162.8	1352.6	.110	82°	4980.7	1862.2	.149
10'	3454.1	960.6		10'	4175.6	1360.1		10'	4995.4	1871.8	
20'	3465.4	966.5		20'	4188.5	1367.6		20'	5010.0	1881.5	
30'	3476.8	972.4		30'	4201.2	1375.2		30'	5024.8	1891.2	
40'	3488.3	978.3		40'	4214.0	1382.8		40'	5039.5	1900.9	
50'	3499.7	984.3		50'	4226.8	1390.4		50'	5054.3	1910.7	
63°	3511.1	990.2	10° C. T .51 E	73°	4239.7	1398.0	10° C. T .61 E	83°	5069.2	1920.5	10° C. T .72 E
10'	3522.6	996.2		10'	4252.6	1405.7		10'	5084.0	1930.4	
20'	3534.1	1002.3		20'	4265.6	1413.5		20'	5099.0	1940.3	
30'	3545.6	1008.3		30'	4278.5	1421.2		30'	5113.9	1950.3	
40'	3557.2	1014.4		40'	4291.5	1429.0		40'	5128.9	1960.2	
50'	3568.7	1020.5		50'	4304.6	1436.8		50'	5143.9	1970.3	
64°	3580.3	1026.6	15° C. T .76 E	74°	4317.6	1444.6	15° C. T .86 E	84°	5159.0	1980.4	15° C. T .96 E
10'	3591.9	1032.8		10'	4330.7	1452.5		10'	5174.1	1990.5	
20'	3603.5	1039.0		20'	4343.8	1460.5		20'	5189.3	2000.6	
30'	3615.1	1045.2		30'	4356.9	1468.4		30'	5204.4	2010.8	
40'	3626.8	1051.4		40'	4370.1	1476.4		40'	5219.7	2021.1	
50'	3638.5	1057.7		50'	4383.3	1484.4		50'	5234.9	2031.4	
65°	3650.2	1063.9	.240	75°	4396.5	1492.4	.332	85°	5250.3	2041.7	.450
10'	3661.9	1070.2		10'	4409.8	1500.5		10'	5265.6	2052.1	
20'	3673.7	1076.6		20'	4423.1	1508.6		20'	5281.0	2062.5	
30'	3685.4	1082.9		30'	4436.4	1516.7		30'	5296.4	2073.0	
40'	3697.2	1089.3		40'	4449.7	1524.9		40'	5311.9	2083.5	
50'	3709.0	1095.7		50'	4463.1	1533.1		50'	5327.4	2094.1	
66°	3720.9	1102.2	20° C. T 1.02 E	76°	4476.5	1541.4	20° C. T 1.12 E	86°	5343.0	2104.7	20° C. T 1.25 E
10'	3732.7	1108.6		10'	4489.9	1549.7		10'	5358.6	2115.3	
20'	3744.6	1115.1		20'	4503.4	1558.0		20'	5374.2	2126.0	
30'	3756.5	1121.7		30'	4516.9	1566.3		30'	5389.9	2136.7	
40'	3768.5	1128.2		40'	4530.4	1574.7		40'	5405.6	2147.5	
50'	3780.4	1134.8		50'	4544.0	1583.1		50'	5421.4	2158.4	
67°	3792.4	1141.4	.321	77°	4557.6	1591.6	.445	87°	5437.2	2169.2	.603
10'	3804.4	1148.0		10'	4571.2	1600.1		10'	5453.1	2180.2	
20'	3816.4	1154.7		20'	4584.8	1608.6		20'	5469.0	2191.1	
30'	3828.4	1161.3		30'	4598.5	1617.1		30'	5484.9	2202.2	
40'	3840.5	1168.1		40'	4612.2	1625.7		40'	5500.9	2213.2	
50'	3852.6	1174.8		50'	4626.0	1634.4		50'	5517.0	2224.3	
68°	3864.7	1181.6	25° C. T 1.28 E	78°	4639.8	1643.0	25° C. T 1.53 E	88°	5533.1	2235.5	25° C. T 1.83 E
10'	3876.8	1188.4		10'	4653.6	1651.7		10'	5549.2	2246.7	
20'	3889.0	1195.2		20'	4667.4	1660.5		20'	5565.4	2258.0	
30'	3901.2	1202.0		30'	4681.3	1669.2		30'	5581.6	2269.3	
40'	3913.4	1208.9		40'	4695.2	1678.1		40'	5597.8	2280.6	
50'	3925.6	1215.8		50'	4709.2	1686.9		50'	5614.2	2292.0	
69°	3937.9	1222.7	.403	79°	4723.2	1695.8	.558	89°	5630.5	2303.5	.756
10'	3950.2	1229.7		10'	4737.2	1704.7		10'	5646.9	2315.0	
20'	3962.5	1236.7		20'	4751.2	1713.7		20'	5663.4	2326.6	
30'	3974.8	1243.7		30'	4765.3	1722.7		30'	5679.9	2338.2	
40'	3987.2	1250.8		40'	4779.4	1731.7		40'	5696.4	2349.8	
50'	3999.5	1257.9		50'	4793.6	1740.8		50'	5713.0	2361.5	
70°	4011.9	1265.0	30° C. T 1.54 E	80°	4807.7	1749.9	30° C. T 1.84 E	90°	5729.7	2373.3	30° C. T 2.20 E
10'	4024.4	1272.1		10'	4822.0	1759.0		10'	5746.3	2385.1	
20'	4036.8	1279.3		20'	4836.2	1768.2		20'	5763.1	2397.0	
30'	4049.3	1286.5		30'	4850.5	1777.4		30'	5779.9	2408.9	
40'	4061.8	1293.6		40'	4864.8	1786.7		40'	5796.7	2420.9	
50'	4074.4	1300.9		50'	4879.2	1796.0		50'	5813.6	2432.9	

$$T = R \tan \frac{1}{2} I$$

$$E = R \operatorname{exsec} \frac{1}{2} I$$

TABLE IX. TANGENTS AND EXTERNALS TO A 1° CURVE

I	T	E	I=100°	I	T	E	I=110°	I	T	E	I=120°
91°	5830.5	2444.9	+ 5° C. T .43 E	101°	6950.6	3278.1	+ 5° C. T .51 E	111°	8336.7	4386.1	+ 5° C. T .62 E
10'	5847.5	2457.1		10'	6971.3	3294.1		10'	8362.7	4407.6	
20'	5864.6	2469.3		20'	6992.0	3310.1		20'	8388.9	4429.2	
30'	5881.7	2481.5		30'	7012.7	3326.1		30'	8415.1	4450.9	
40'	5898.8	2493.8		40'	7033.6	3342.3		40'	8441.5	4472.7	
50'	5916.0	2506.1		50'	7054.5	3358.5		50'	8468.0	4494.6	
92°	5933.2	2518.5	.200	102°	7075.5	3374.9	.268	112°	8494.6	4516.6	.360
10'	5950.5	2531.0		10'	7096.6	3391.2		10'	8521.3	4538.8	
20'	5967.9	2543.5		20'	7117.8	3407.7		20'	8548.1	4561.1	
30'	5985.3	2556.0		30'	7139.0	3424.3		30'	8575.0	4583.4	
40'	6002.7	2568.6		40'	7160.3	3440.9		40'	8602.1	4606.0	
50'	6020.2	2581.3		50'	7181.7	3457.6		50'	8629.3	4628.6	
93°	6037.8	2594.0	10° C. T .86 E	103°	7203.2	3474.4	10° C. T .103 E	113°	8656.6	4651.3	10° C. T 1.25 E
10'	6055.4	2606.8		10'	7224.7	3491.3		10'	8684.0	4674.2	
20'	6073.1	2619.7		20'	7246.3	3508.2		20'	8711.5	4697.2	
30'	6090.8	2632.6		30'	7268.0	3525.2		30'	8739.2	4720.3	
40'	6108.6	2645.5		40'	7289.8	3542.4		40'	8767.0	4743.6	
50'	6126.4	2658.5	.401	50'	7311.7	3559.6	.536	50'	8794.9	4766.9	.721
94°	6144.3	2671.6	15° C. T 1.30 E	104°	7333.6	3576.8	15° C. T 1.56 E	114°	8822.9	4790.4	15° C. T 1.93 E
10'	6162.2	2684.7		10'	7355.6	3594.2		10'	8851.0	4814.1	
20'	6180.2	2697.9		20'	7377.8	3611.7		20'	8879.3	4837.8	
30'	6198.3	2711.2		30'	7399.9	3629.2		30'	8907.7	4861.7	
40'	6216.4	2724.5		40'	7422.2	3646.8		40'	8936.3	4885.7	
50'	6234.6	2737.9		50'	7444.6	3664.5		50'	8965.0	4909.9	
95°	6252.8	2751.3	.604	105°	7467.0	3682.3	.806	115°	8993.8	4934.1	.1.09
10'	6271.1	2764.8		10'	7489.6	3700.2		10'	9022.7	4958.6	
20'	6289.4	2778.3		20'	7512.2	3718.2		20'	9051.7	4983.1	
30'	6307.9	2792.0		30'	7534.9	3736.2		30'	9080.9	5007.8	
40'	6326.3	2805.6		40'	7557.7	3754.4		40'	9110.3	5032.6	
50'	6344.8	2819.4		50'	7580.5	3772.6		50'	9139.8	5057.6	
96°	6363.4	2833.2	20° C. T 1.74	106°	7603.5	3791.0	20° C. T 2.08	116°	9169.4	5082.7	20° C. T 2.52
10'	6382.1	2847.0		10'	7626.6	3809.4		10'	9199.1	5107.9	
20'	6400.8	2861.0		20'	7649.7	3827.9		20'	9229.0	5133.3	
30'	6419.5	2875.0		30'	7672.9	3846.5		30'	9259.0	5158.8	
40'	6438.4	2889.0		40'	7696.3	3865.2		40'	9289.2	5184.5	
50'	6457.3	2903.1		50'	7719.7	3884.0		50'	9319.5	5210.3	
97°	6476.2	2917.3	E .809	107°	7743.2	3902.9	1.08	117°	9349.9	5236.2	E 1.46
10'	6495.2	2931.6		10'	7766.8	3921.9		10'	9380.5	5262.3	
20'	6514.3	2945.9		20'	7790.5	3940.9		20'	9411.3	5288.6	
30'	6533.4	2960.3		30'	7814.3	3960.1		30'	9442.2	5315.0	
40'	6552.6	2974.7		40'	7838.1	3979.4		40'	9473.2	5341.5	
50'	6571.9	2989.2		50'	7862.1	3998.7		50'	9504.4	5368.2	
98°	6591.2	3003.8	25° C. T 2.18	108°	7886.2	4018.2	25° C. T 2.61	118°	9535.7	5395.1	25° C. T 3.16
10'	6610.6	3018.4		10'	7910.4	4037.8		10'	9567.2	5422.1	
20'	6630.1	3033.1		20'	7934.6	4057.4		20'	9598.9	5449.2	
30'	6649.6	3047.9		30'	7959.0	4077.2		30'	9630.7	5476.5	
40'	6669.2	3062.8		40'	7983.5	4097.1		40'	9662.6	5504.0	
50'	6688.8	3077.7	E	50'	8008.0	4117.0	E	50'	9694.7	5531.7	E
99°	6708.6	3092.7	1.02	109°	8032.7	4137.1	1.36	119°	9727.0	5559.4	1.83
10'	6728.4	3107.7	30° C. T 2.62	10'	8057.4	4157.3	30° C. T 3.14	10'	9759.4	5587.4	30° C. T 3.81
20'	6748.2	3122.9		20'	8082.3	4177.5		20'	9792.0	5615.5	
30'	6768.1	3138.1		30'	8107.3	4197.9		30'	9824.8	5643.8	
40'	6788.1	3153.3		40'	8132.3	4218.4		40'	9857.7	5672.3	
50'	6808.2	3168.7		50'	8157.5	4239.0		50'	9890.8	5700.9	
100°	6828.3	3184.1	T 2.62 E 1.22	110°	8182.8	4259.7	T 3.14 E 1.63	120°	9924.0	5729.7	T 3.81 E 2.20
10'	6848.5	3199.6		10'	8208.2	4280.5		10'	9957.5	5758.6	
20'	6868.8	3215.1		20'	8233.7	4301.4		20'	9991.0	5787.7	
30'	6889.2	3230.8		30'	8259.3	4322.4		30'	10025.0	5817.0	
40'	6909.6	3246.5		40'	8285.0	4343.6		40'	10059.0	5846.5	
50'	6930.1	3262.3		50'	8310.8	4364.8		50'	10093.0	5876.1	

TABLE X.
MIDDLE ORDINATES OF RAILS
Length of Rail (feet)

C o /	R Feet	30 Inch	28 Inch	26 Inch	24 Inch	22 Inch	20 Inch	C o	R Feet	30 Inch	28 Inch	26 Inch	24 Inch	22 Inch	20 Inch
0-20	17189	.08	.07	.06	.05	.04	.03	8	716.8	1.88	1.64	1.42	1.20	1.01	.84
0-40	8594	.16	.14	.12	.10	.08	.07	9	637.3	2.12	1.84	1.60	1.35	1.14	.94
1-0	5730	.24	.20	.18	.15	.13	.10	10	573.7	2.36	2.05	1.78	1.50	1.27	1.04
1-20	4297	.31	.27	.23	.20	.17	.13	11	521.7	2.59	2.26	1.95	1.65	1.39	1.15
1-40	3438	.39	.34	.29	.25	.21	.17	12	478.3	2.83	2.47	2.15	1.81	1.54	1.26
2-0	2865	.47	.41	.35	.30	.25	.20	13	441.7	3.05	2.66	2.30	1.96	1.66	1.36
2-20	2456	.55	.48	.41	.35	.29	.23	14	410.3	3.30	2.87	2.48	2.10	1.78	1.46
2-40	2149	.63	.55	.47	.40	.33	.27	15	383.1	3.54	3.08	2.68	2.26	1.91	1.57
3-0	1910	.71	.62	.53	.45	.38	.31	16	359.3	3.76	3.28	2.83	2.40	2.04	1.67
3-20	1719	.78	.68	.59	.50	.42	.35	17	338.3	4.00	3.48	3.02	2.57	2.16	1.78
3-40	1563	.86	.75	.65	.55	.46	.38	18	319.6	4.21	3.67	3.18	2.70	2.28	1.87
4-0	1433	.94	.82	.71	.60	.50	.42	19	302.9	4.45	3.89	3.36	2.86	2.41	1.98
4-20	1323	1.02	.89	.77	.65	.55	.45	20	287.9	4.70	4.09	3.55	3.00	2.54	2.09
4-40	1228	1.10	.96	.83	.70	.59	.48	22	262.0	5.16	4.44	3.84	3.30	2.80	2.29
5	1146	1.18	1.03	.89	.75	.63	.52	24	240.5	5.64	4.92	4.20	3.59	3.04	2.50
6	955.3	1.41	1.23	1.06	.90	.76	.62	26	222.3	6.07	5.29	4.58	3.88	3.29	2.70
7	819.0	1.65	1.44	1.24	1.05	.89	.73								

TABLE XI.
SHORT RADIUS CURVES

Radius Feet	Chord Feet	Central Angle	Deflection Angle	Deflection for 1 Foot
35	10	16-26	8-13	49.3
45	10	12-46	6-23	38.3
50	15	17-16	8-38	34.5
60	15	14-22	7-11	28.8
75	15	11-30	5-45	23.0
100	20	11-30	5-45	17.3
120	20	9-34	4-47	14.3
150	20	7-39	3-49	11.5
190	25	7-32	3-46	9.15
200	25	7-10	3-35	8.6
225	25	6-25	3-12	7.7
240	25	5-58	2-59	7.2
250	25	5-44	2-52	6.9
275	25	5-12	2-36	6.2
288	50	9-58	4-59	6.0
300	50	9-32	4-46	5.7
350	50	8-12	4-06	4.9
376	50	7-40	3-50	4.6
400	50	7-10	3-35	4.3
410	50	7-00	3-30	4.2

To find length of curve divide angle from P. C. to P. T. by central angle of chord, and multiply by length of chord.

TABLE XII.
INCLINED DISTANCE OF 100 FT. REDUCED TO HORIZONTAL

Slope	Horizontal Distance	Correction	Rise Per Foot	Slope	Horizontal Distance	Correction	Rise Per Foot
0°00'	100.000	0.000	0.000	8°00'	99.027	0.973	0.139
15'	99.999	0.001	0.004	15'	98.965	1.035	0.143
30'	99.996	0.004	0.009	30'	98.902	1.098	0.148
45'	99.991	0.009	0.013	45'	98.836	1.164	0.152
1 00	99.985	0.015	0.017	9 00	98.769	1.231	0.156
15	99.976	0.024	0.022	15	98.700	1.300	0.161
30	99.966	0.034	0.026	30	98.629	1.371	0.165
45	99.953	0.047	0.031	45	98.556	1.444	0.169
2 00	99.939	0.061	0.035	10 00	98.481	1.519	0.174
15	99.923	0.077	0.039	15	98.404	1.596	0.178
30	99.905	0.095	0.044	30	98.325	1.675	0.182
45	99.885	0.115	0.048	45	98.245	1.755	0.187
3 00	99.863	0.137	0.052	11 00	98.163	1.837	0.191
15	99.839	0.161	0.057	15	98.079	1.921	0.195
30	99.813	0.187	0.061	30	97.992	2.008	0.199
45	99.786	0.214	0.065	45	97.905	2.095	0.204
4 00	99.756	0.244	0.070	12 00	97.815	2.185	0.208
15	99.725	0.275	0.074	15	97.723	2.277	0.212
30	99.692	0.308	0.078	30	97.630	2.370	0.216
45	99.657	0.343	0.083	45	97.534	2.466	0.221
5 00	99.619	0.381	0.087	13 00	97.437	2.563	0.225
15	99.580	0.420	0.092	15	97.338	2.662	0.229
30	99.540	0.460	0.096	30	97.237	2.763	0.233
45	99.497	0.503	0.100	45	97.134	2.866	0.238
6 00	99.452	0.548	0.105	14 00	97.030	2.970	0.242
15	99.406	0.594	0.109	15	96.923	3.077	0.246
30	99.357	0.643	0.113	30	96.815	3.185	0.250
45	99.307	0.693	0.118	45	96.705	3.295	0.255
7 00	99.255	0.745	0.122	15 00	96.593	3.407	0.259
15	99.200	0.800	0.126	15	96.479	3.521	0.263
30	99.144	0.856	0.131	30	96.363	3.637	0.267
45	99.087	0.913	0.135	45	96.246	3.754	0.271

TABLE XIII.
MINUTES IN DECIMALS OF A DEGREE.

0 30"	.00833	10' 30"	.17500	20' 30"	.34167	30' 30"	.50833	40' 30"	.67500	50' 30"	.84167
1 00	.01667	11 00	.18333	21 00	.35000	31 00	.51667	41 00	.68333	51 00	.85000
30	.02500	30	.19167	30	.35833	30	.52500	30	.69167	30	.85833
2 00	.03333	12 00	.20000	22 00	.36667	32 00	.53333	42 00	.70000	52 00	.86667
30	.04167	30	.20833	30	.37500	30	.54167	30	.70833	30	.87500
3 00	.05000	18 00	.21667	28 00	.38333	38 00	.55000	48 00	.71667	58 00	.88333
30	.05833	30	.22500	30	.39167	30	.55833	30	.72500	30	.89167
4 00	.06667	14 00	.23333	24 00	.40000	34 00	.56667	44 00	.73333	54 00	.90000
30	.07500	30	.24167	30	.40833	30	.57500	30	.74167	30	.90833
5 00	.08333	15 00	.25000	25 00	.41667	35 00	.58333	45 00	.75000	55 00	.91667
30	.09167	30	.25833	30	.42500	30	.59167	30	.75833	30	.92500
6 00	.10000	16 00	.26667	26 00	.43333	36 00	.60000	46 00	.76667	56 00	.93333
30	.10833	30	.27500	30	.44167	30	.60833	30	.77500	30	.94167
7 00	.11667	17 00	.28333	27 00	.45000	37 00	.61667	47 00	.78333	57 00	.95000
30	.12500	30	.29167	30	.45833	30	.62500	30	.79167	30	.95833
8 00	.13333	18 00	.30000	28 00	.46667	38 00	.63333	48 00	.80000	58 00	.96667
30	.14167	30	.30833	30	.47500	30	.64167	30	.80833	30	.97500
9 00	.15000	19 00	.31667	29 00	.48333	39 00	.65000	49 00	.81667	59 00	.98333
30	.15833	30	.32500	30	.49167	30	.65833	30	.82500	30	.99167
10 00	.16667	20 00	.33333	30 00	.50000	40 00	.66667	50 00	.83333	60 00	1.00000

Computed by L. Leland Locke.

237+75

6-19-59

1 = 92
2 = 104
3 = 99
4 = 115
5 = 100
6 = 93

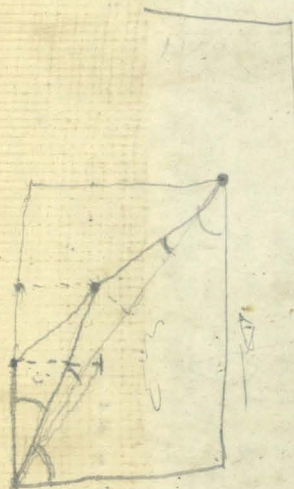


A.D. 24166

2 - 510
3 - 1086
1596

319+26.2

4 - 1154
6 - 471
1628



381+72