

No 9

8

PRIVATE
DIETZGEN
TRADE MARK

1087

No. 412

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

Roadway 16 feet wide.

Side Slopes 1 on 1.

For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	1
2	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	2
3	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	6
7	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	7
8	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	8
9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	9
10	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	10
11	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	11
12	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	12
13	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	13
14	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	14
15	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	15
16	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	16
17	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	17
18	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	18
19	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	19
20	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	20
21	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	21
22	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	22
23	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	23
24	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	24
25	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	25
26	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	27
28	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	31
32	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	32
33	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	33
34	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	34
35	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	35
36	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	36
37	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	37
38	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	38
39	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	39
40	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	40

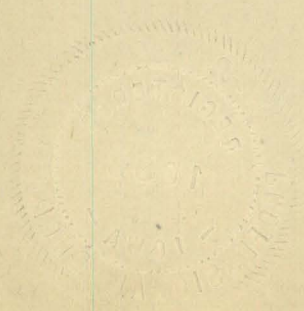
Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be $30.6 + (20 - 16) \div 2$ or 2 ft. added to 30.6 = 32.6. For slopes of 1 on 1½ see inside of back cover.

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FILED
FEB 27 '23
J.W. Bailey
COUNTY CLERK

Index

Line		Page
6-Lt.	Check	1-2
5-Rt.	Check	3-5
c Main	Check	9-11.
12-Lt.	Check	12-12.
11-Lt.	Check	13-13.
K-Rt.	Check	18-18
L	Check	18-18.
J-Rt.	Chk.	19-20
7-Rt.	Chk	21-22
O-Rt.	Chk.	24-29, 26-26.
P	Chk.	27-27
6-K		15.
W-R		54.



J.E. Johnson Private
MARY A.
58.54

Briggs
10/12/21 Hoff

0	8.70	49.84	44.90
0+22	8.69	49.85	45.00
0+50	8.80	49.74	45.10
1	8.92	49.62	45.30
End	7.30		5/24

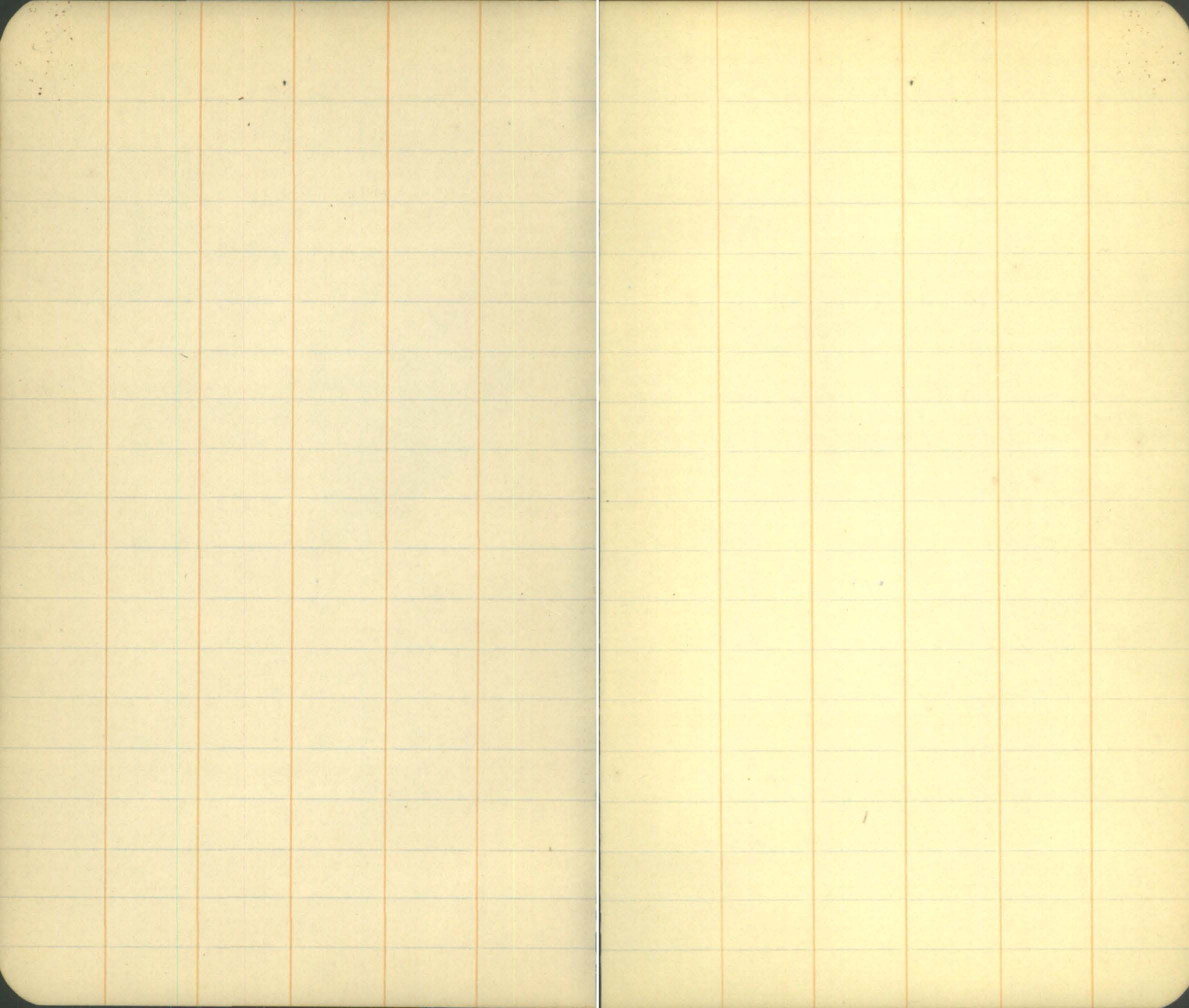
4.94 = 49+80 Mail #1 D#12

4.85

4.64

4.32

2' 0 1 0 2' 0



RA Rodamar - Private

BRH-18-A

7%
80
6.00

11/16/21

Hoff
Bucke

Sta B5 H-1 -5 Elev Cor Col

BMF 3.99 36.79 32.80

T.P. 5.60 37.69 4.70 32.09

Lath/huksin F Cor N Sta 23 Nam J

26.60

0 7.22 30.47 27.00

1 7.17 30.52 27.60

2 6.56 31.13 27.80

3 6.15 31.54 28.20

3+75 End 5.30 32.39 28.80

3.47 = 10+50 BR H-18

3.12 $\frac{0}{0}$

3.33 $\frac{0}{0}$

3.34 $\frac{0}{0}$

3.39 $\frac{0}{0}$

(27.28)

BRH-18-B

0 37.69 7.20 30.49 27.30

1 6.81 30.88 27.80

2 5.93 31.76 28.30

3 End 4.85 32.84 29.30

3.19 = 11+57 BR H-18 (End)

3.08 $\frac{0}{0}$

3.46 $\frac{0}{0}$

3.54 1.00

Br J-1

37.69

0		7.89	29.80	26.30	3.50 = Sta 1425 Main J
1		6.45	31.24	27.80	3.44 $\frac{1.50}{5.00}$
2		5.40	32.29	28.80	3.49
2+58	End	5.01	32.68	29.38	3.30

Br J-2

(26.00)

0	37.69	7.95	29.74	26.60	3.24 = Sta 15748 Main J
1		6.23	31.46	28.00	3.46 $\frac{1.50}{5.00}$
2		5.60	32.09	28.50	3.39
3		5.28	32.41	29.00	3.41
3+50	End	5.06	32.63	29.25	3.38

Br J-3

$$\begin{array}{r} .73 \\ .73 \\ \hline 375 \\ 525 \\ \hline 5625 \end{array}$$

37.69

(26.25)

0	7.30	30.39	26.95	3.64	= Sta 16+50 Main
1	5.59	32.10	28.00	4.10	$\frac{5}{125}$
2 1/2 hole	6.24	31.45	28.75	2.70	$\frac{10}{150}$
2+75	4.92	32.77	29.31	3.46	

Br J-4

37.69

(26.25)

0	6.92	30.77	27.50	3.27	= Sta 17+42 Main
+50	6.05	31.64	27.90	3.74	
1	6.15	31.54	28.30	3.24	$\frac{8}{10}$
2	5.30	32.39	29.80	3.39	$\frac{10}{150}$
3	4.73	32.96	29.70	3.26	$\frac{11}{150}$
3+60 End	4.25	33.44	30.12	3.32	

BR H-27-13

37.69

0		8.05	29.64	26.25	3.39	= 7450	H-27
0+50		7.92	29.77	26.65	3.12		
1		7.20	30.49	27.05	3.44		
2		6.47	31.22	27.85	3.37		
3	End	5.24	32.45	28.65	3.80		

131P H-27-C

0	37.69	7.25	30.44	27.00	3.44	= 9425	H-27
1		6.63	31.06	27.90	3.36		
2	End	5.97	31.72	28.40	3.32		

130 J-5

0-3-4	6.03	36.80	30.77		
		36.76			
0-5-3	6.33	36.72	30.39		
0	on spoil Bank	6.62	30.14	25.50	4.64 = sta 12 Main J-Approx
0+20		7.70	29.06	26.00	3.06 $\frac{1.00}{90}$
1		6.52	30.24	26.50	3.74 $\frac{1.00}{90}$ = 0 J-5-A
1+80		5.63	31.13	26.90	4.23 = 0 J-5-B
2		5.82	30.94	27.00	3.94
2+52		5.84	30.92	27.26	3.66 $\frac{1.00}{90}$ = 0 J-5-C
3		5.66	31.10	27.50	3.60 $\frac{1.00}{90}$
3+31		5.58	31.18	27.65	3.63 = 0 J-5-D
3+50		5.58	31.18	27.75	3.43
4		5.29	31.47	28.00	3.47
4+14		5.16	31.60	28.03	3.57 $\frac{1.00}{90}$ = 0 J-5-E
5		5.33	31.43	28.15	3.28 $\frac{1.00}{90}$ = 0 J-5-F
5+85	NOTE	5.20	31.56	28.28	3.28

Br J - S - A

36.76

0	6.52	30.24	26.75 ₈₅	3.49	= sta 1 Br J-S
+50	6.02	30.74	27.13	3.61	$\frac{1.00}{1.00}$
1	5.80	30.96	27.50	3.46	$\frac{1.00}{1.00}$
2	5.32	31.44	28.25	3.19	
3 End	4.42	32.34	29.00	3.34	

Br J - S - 13

36.76

0	5.64	31.12	27.25	3.87	= sta 1+80 Br J-S
+50	5.27	31.49	27.75	3.74	$\frac{1.00}{1.00}$
1	5.07	31.69	28.25	3.44	$\frac{1.00}{1.00}$
2	4.95	31.81	28.75	3.06	$\frac{1.00}{1.00}$
2+60	4.22	32.54	29.20	3.34	$\frac{1.00}{1.00}$

BR J S C

(+20)

36.76

0	58.1	30.92	27.50	3.42	= 2 + 52/	2 - 8
+50	5.64	31.12	27.75	3.37	10	
1	5.41	31.35	28.00	3.35	5	
2	4.76	32.00	29.00	3.00		
2+20	4.22	32.54	29.70	3.34	1.00	

BR J S D

0	36.76	5.57	31.19	27.75	3.44	= 3 + 31	J S
+50		5.32	31.44	28.00	3.44	10	
1		5.15	31.61	28.25	3.36	7	
1+50		4.25	32.51	28.65	3.86		

BRJ-S-E

36.76

0

5.15 31.61 28.25

3.36

9.5 = 419 J-5

+50

5.22 31.57 28.38

3.16

2.7

1

4.85 31.91 28.50

3.41

1+20

4.28 32.48 28.90

3.58

2.8

BRJ-S-F

36.76

0

5.33 31.43 28.25

3.18

= 5 V-5

0+50

5.17 31.59 28.35

3.24

2.0

0+67

4.80 31.96 28.38

3.58

Tile Check

#9

BR. 6 Left.

B.M. 2.40 67.70 65.30
5.00
62.70

0.50 4.12 58.58 58.45

1 3.80 58.90 58.80

3.45

2.97

2.78

3 2.32

1.93

4 1.60 61.10 60.90

1.40

5 7.46 74.35 0.81 66.89
5.00
69.35 7.13

6 6.72 64.63 62.30

6.40

7 6.20

7+50

8

9

10

11

12

13

14

15

62.70 67.70
5.00 3.52
79.45 64.18
74.35
5.00
69.35

10" = 9+80

7.49

80.67
4.86
75.81

5.75

5.60

5.20

4.72

4.40

4.30

3.95

3.56

3.20

2.70

2.32

2.00

1.60

1.17

7.00

6.60

6.30

63.75

63.70

64.63

64.40

65.05

65.10

66.75

66.70

67.45

67.50

73.13

7 = 10

6/26/22
Brynn
Matthews

2

6 10 ft.

80.67
4.60

25

86.69
4.60
82.09

6.10 75.99 76.10

16

75.87

5.87 70.00 69.90

5.80

5.42

26

5.60 76.49 76.70

17

5.00 70.87 70.70

27

5.25

4.60

27

4.90 77.19 77.30

18

5.17 71.50

28

4.60

3.85

28

4.30 77.79 77.90

19

3.40 72.47 72.30

29

4.12

3.10

29

3.72 78.36 78.50

20

2.70 72.17 72.10

30

3.50

2.23

30

3.20 78.89 79.10

21

6"

2.10 78.77 78.70

31

2.75

1.85

31

2.65 79.44 79.70

22

1.70 7 74.20

1.90

7.15

86.69
4.60
82.09

1.12 79.54

3/ END.

23

6.96 75.11 74.90

OK To File

6.65

6/26/22

24

6.30 75.79 75.50

R.F.B.

80.56
455
7501

file check
5-R-

195
160
256

4.80

67.70

+

75

+

76

+ 25

+ 50

77

+

78

+

79

+

80

+

81

+

82

4.90
1.80
675

1.80
4.75
1

80.56

73.88

74.01

4.05

3.95

3.80

3.50

3.35

3.30

3.30

3.15

3.05

2.85

2.70

2.50

2.40

2.30

2.20

1.80

1.70

67.80 = .33
80-100 = .34%

69.86

69.94

70.31

70.27

70.71

70.60

70.96

70.93

71.31

71.26

71.61

71.59

71.01

71.93

72.31

72.27

5.60

77.28

675

77.53

5.48

73.68

67.05

67.53

67.73

67.63

68.02

67.96

68.32

68.39

68.78

68.72

69.03

69.05

75.84

69.21

69.28

69.66

(2) snails

67.30

67.63

67.96

68.32

68.39

68.78

68.72

69.03

69.05

69.21

69.28

69.66

69.81

67

+

68

+

69

+

70

+

71

+

72

+

T.P. 4.72

73

+

74

80.56

675

73.81

3.44

4.60

4.40

4.15

4

4.95
1.6
6.5577.03
6.18
83.21
6.55
76.63
21.83

T.P.

80.56 2.50 77.06

83.24
6.55

76.69 1.90

6.18 83.24
6.55

+

82

76.69 4.40 72.29 72.27 90 5.05 86.60 1.69 81.55 74.97
75.00

+

4.25 +

80.05 4.85

83

4.10 72.59 72.61 91 4.60 75.45 75.83

H0483

6.15 77.09 77.03 + 4.52

+

4.00 92 4.40 75.65 75.67

84

3.80 72.89 72.95 + 40 4.30

+

3.50 93 4.00 76.05 76.01

85

3.35 73.34 73.29 + 3.80

+

3.15 94 3.65 76.40 76.35

86

2.95 73.74 73.63 + 3.45

+

2.80 95 3.23 76.82 76.89

87

2.75 73.94 73.97 + 3.15

+

2.50 96 2.90 77.15 77.03

88

2.30 74.39 74.31 + 2.75

+

2.10 97 2.50 77.55 77.37

89

2.00 74.69 74.65 + 2.40

5

$$\begin{array}{r} 4.95 \\ 1.5 \\ \hline 6.45 \end{array}$$

$$\begin{array}{r} 86.60 \\ \hline 605 \end{array}$$

98

20 15

2.42

77.72

77.71

98+50

H0599

VSE.

3.10

(83.50)

83.52

CHIK

G-R

8/25/22

8

87.75

6.00

81.75 81.80

99

5.72

89.22

83.50

5.70

O+no

82.07

4.87

78.20

77.80

9

5.40

82.25 82.30

1

4.00

78.27

78.30

10

4.90

82.85 82.80

4.50

4.60

2

83.27

4.40

78.87

78.80

11

4.40

83.35 83.30

4.25

5"

87.95

4.40

3

4.00

79.27

79.30

12

4.20

83.75 83.80

3.62

3.90

4

3.55

79.72

79.80

13

3.75

84.20 84.40

3.25

3.40

5

3.00

80.27

80.30

14

6.95

91.81

3.07

84.86

85.00

2.70

6.60

6

2.50

80.77

80.80

15

6.40

85.41

85.60

2.20

6.00

7

6.45

87.75

1.97

81.30

81.30

16

5.80

86.01

86.20

6.20

5.40

8

8

89.77 2.20 86.57 86.45

2.05

99

6.85

90.35

83.50

9

2.85 86.92 86.85

0

84.80

6.00

78.80

78.60

2.60

0+5

10

2.45 87.22 87.25

1

11

89.97 1.90 88.07 88.25

12

9.33 98.47 0.82 89.14 89.25

2

13

8.25 90.22 90.25

3

14

7.20 91.27 91.25

4

15

6.30 92.17 92.25

5

16

5.25 93.22 93.25

4

16+50

4.75

7

17

4.40 94.07 94.25

7+65 End

18

3.50 94.97 95.25

19

1.50

20

1.50

21 End

0.51

78.60

6

CHIC

495
555

H-R.

8/25/22

99
 6.85
 90.35
 555
 84.80
 6.00
 78.80
 78.60
 5.65
 79.15
 78.90
 5.45
 79.25
 79.20
 5.30
 4.85
 79.95
 79.80
 4.30
 80.50
 80.40
 3.55
 81.25
 81.00
 3.10
 81.70
 81.60
 2.45
 82.35
 82.20
 2.05
 82.75
 82.80
 1.40
 83.40
 82.19

CH

CHK

8/25

R.P.B.

9

Tile Chk Main Line

R.P.	7.06	85.64 6.30 79.34	78.56	Book 9 Pg. 27
110+50 (Hwy)		8.12	77.51	
tile 110		7.24		
110+50		7.10		
111		6.90	72.44 72.45	
+		6.70		
112		6.45	72.89 72.90	
+		6.25		
113		5.90	72.40 72.35	
+		5.78		
114 $\frac{1}{2}$ mile		5.56		
+		5.45		
115		79.50 5.25	74.09 74.25	
+		5.00		
116		4.85	74.69 74.70	
+		4.50		

25 22 45 77.52
22 69
12
61

7.9 tile Rod
85.64
79.54 4.23

7/18/22

117	+	4.23		
118		3.98	75.52	75.60
T.P.	6.83	88.97 6.10 82.87	2.50	82.14
118		7.30	75.57	75.60
+		7.10		
117		6.85	76.02	76.05
+		6.62		
120		6.50	76.27	76.50
+		6.23		
121		6.02	76.85	76.95
+		5.85		
122		5.50	77.27	77.40
+		5.35		
123		5.05	77.82	77.85
+		4.92		
124		4.70	78.17	78.30

Ok to fill

7/19/22
R.P.

10

Main Check

88.77

5.95

82.82

4.60

124+50

125

4.40

78.62

78.75

Hwy 126

5.54

90.30

5.95

84.35

84.76

+

4.05

+

4.75

79.95

126

2.80

79.22

79.95

.127

4.45

79.90

79.95

+

2.40

+

4.15

127

3.13

79.89

79.95

128

3.80

80.55

80.55

Hwy 127

2.80

(85.15) use

+

3.50

129

3.15

81.20

81.15

+

2.90

130

2.65

81.70

81.75

+

2.25

131

2.00

82.35

82.35

+

1.75

132

1.46

82.89

82.95

+

1.13

133

5.26

94.15

0.81

89.49

83.54

83.55

+

5.95

88.80

5.00

MAIN CLK

8.18	86.79
7.74	
.44	

11

134

94.75

4.65

8/10/22 P.M.

134

86.80

84.15

84.15

+

4.25

125

4.05

84.75

84.75

+

3.70

126

3.40

85.40

85.25

+

3.15

127

2.94

85.86

85.75

+

2.65

128

2.25

86.55

86.55

138+40

2.05

86.75

86.79

1311

2.12

(92.62)

Center West Wing Core Culv.

OK.
A-1 Excellent
Work

12

12 left CLK

4.88
5.75

.7%

7/18/22

88.97
5.75

83.22 4.88 78.24 78.40

+50

4.60

1

4.20 79.02 79.10

+

2.80

2

2.60 79.62 79.80

+

2.20

3

6.95 87.27 2.88 80.24 80.50

+

6.60

4

6.20 81.09 81.20

+

5.80

5

5.45 81.84 81.90

+

5.16

6

4.80 82.49 82.60

+

4.45

7

4.10 83.19 83.30

+

3.70

8 END

3.33 83.96 84.00

OK To file
7/18/22
RRB

13

11 left,

58.00
55
27tile No 1 4.95
10" 1.55 = 10
.5 = End.

85.64

Tile chkr

8

79.69 2.95 76.74 7/18/22

85.64

+

2.65

5.95

79.69 7.35 72.34 72.40

9

2.30 77.39 77.35

+ 50

7.02

+

2.10

1

6.80 72.89 72.95

10

1.92 77.77 77.75

+

6.53

T.P.

2.80 (87.84) USE.

2

6.23 73.46 73.50

+

5.93

3

5.70 73.99 74.05

+

5.34

4

5.10 74.59 74.60

+

4.85

5

4.55 75.14 75.15

+

4.20

6

3.95 75.74 75.70

+

3.70

7

3.45 76.24 76.25

+

3.17

14

CHIC
5-R

78.05

$$\begin{array}{r} 78.05 \\ 35 \\ 72.29 \\ 2 \\ \hline 51 \end{array}$$

111

92.61

3.27

89.34

89.37

99+55 6.30 90.31 84.01

112

101 6.15 90.26 84.11

113

2.60

90.01

89.89

98+50 90.28 OK

114

99 5.95
84.33 OK

115

78.05

OK to file
8/25/22
P.P.B.

2.10

90.51

90.37

1.70

90.91

90.89

1.10

91.51

91.39

99+50 6.23 78.10 78.22 C.L.

2.90

100+50 5.65 78.68 78.56

101 84.52 5.25 79.28 79.37

4.95

101+50 4.58

$$\begin{array}{r} 1.10 \\ 5.05 \\ 8 \\ \hline 5.85 \\ 2.90 \\ \hline 95 \end{array}$$

102 4.12 80.35 80.39

103 3.05 81.48 81.39

104 2.20 82.32 82.39

105 9.10 92.61 1.02 83.51 83.39

106 9.10 83.51 8.10 84.51 84.39

107 7.30 85.31 85.39

108 6.15 86.46 86.39

109 5.15 87.46 87.39

110 4.25 88.36 88.39

15

BR 6-R

8/29/2

540
495
1035
497
538

8.97
495
1392

1.490
14

13.92
258
5.34

BIM

Cont See 70.14

pg-101 Book 9. Spike at End E. Cap.

Top 10" 13.92 62.92 50.00

21
3250
2137
11.13
4900
6013 = 0

21+37			8.58	55.34	49.00	6.34	
22			8.36	55.56	49.63	5.93	
23			7.90	56.02	50.63	5.39	
24			6.94	56.98	51.63	5.35	
25			5.97	57.95	52.63	5.32	
26			4.87	59.05	53.63	5.42	
27			4.14	59.78	54.63	5.15	1.00%
28	7.10	67.71	3.31	60.61	55.63	4.98	
29			6.13	61.58	56.63	4.95	
30			5.03	62.68	57.63	5.05	
31			4.27	63.44	58.63	4.81	
32			3.25	64.46	59.63	4.83	
32+50 End			2.33	65.38	60.63	5.25	

- 6 BR IV.

Cuts 8 1/2 4 1/22
RMS

16

BRV.-R.

0

62.92 4.14 59.78 54.80 4.98 = 27 6-R

0+50

2.93 59.99 55.50 4.49 do

1

2.12 60.80 56.20 4.60 d

2

1.98 61.94 57.60 4.34

2+45 End

1.21 62.61 58.23 4.38 cuts 8/29/22

RRB

44	5	54.63	62.00	64.50
2			1.1	17
	45			
	14			
	180			
	45			
	630			

17

BR R-Right.

$$\begin{array}{r} 56.72 \\ 4 \\ \hline 52.72 \end{array}$$

$$\begin{array}{r} 15 \\ 7 \\ \hline 12 \end{array}$$

B.H 8" corr. 10.41 60.41 50.00

0

6.72	53.69	50.00	50.00	3.69	10
------	-------	-------	-------	------	----

1

4.67	55.74	51.00	51.50	4.24	1.5
------	-------	-------	-------	------	-----

1+70

3.69	56.72	54.70	52.05	4.67	
------	-------	-------	-------	------	--

18

Tile chkr

K. Rt.

18

90.43

5.03

79.65

79.78

B.M.

4.23

85.84

81.61

Block 8

19

84.88

4.25

80.63

80.41

7

79.89

6.95

72.94

72.80

20

3.90

80.93

81.00

8

6.34

73.55

73.45

21

3.40

81.48

81.67

8+50

6.15

21+8' End

2.30

82.50

9

80.09

5.90

74.19

74.08

+

5.70

BR.

L

10

5.45

74.64

74.71

0

90.42

4.60

80.20

80.16

+

5.20

1

4.20

11

4.65

75.40

75.34

2

3.90

+

4.50

3

2.55

OK. Feb 7/28/22
R.P.B.

12

4.30

75.79

75.97

4

3.00

81.88

81.76

+

3.85

5

1.50

82.38

82.46

13

3.55

76.54

76.60

6

0.00

84.88

84.86

14

3.00

77.09

77.23

6-1

15

2.45

7 End

16

1.70

17

5.68

90.43

1.09

84.75

90.43
555
24.8885.84
575
80.094.95
575
5754.95
575
575

10" 8+50

4.75
19J-R. 941
Tide Chick

7/28/22

29 4.45
50 12 6154.45
14 60524.81
6.25
70.56
6.45
71.56B. 1990
1797 NEWS80.81
6.15
78.66

BPM	3.25	84.81	81.46	Book 8 Pg-118	37			78.80	74.86	74.77
29		6.15	6.90	71.56	71.30	+		2.50		
+50		78.66	6.60					3.40	75.26	75.17
30			6.20	72.46	71.80	+		3.27		
			6.10			39		3.20	75.46	75.57
31			6.00	72.66	72.67	+		2.90		
31+50			5.80			40	6.90	29.17 5.95	2.54	82.27 76.12 75.97
32			5.50	72.16	72.00	+		83.22	6.75	
+			5.40			41		6.50	76.72	76.67
33			5.15	73.51	72.33	42		5.80	77.42	77.37
+			5.05			43		5.10	78.12	78.07
34			4.95	72.71	73.66	44		4.40	78.82	78.77
+			4.80			45		3.75	79.48	79.47
35+15			4.65	74.01	73.99	46		2.00	80.22	80.17
35+50			4.48			47		2.25	80.97	80.92
36			4.30	74.36	74.37	48		1.43	81.77	81.77
+			4.00			49	6.50	95.17	88.67 87.72	87.57

20

50

51

52

53

54

54+47END.

95.17 6.00

575

89.42

5.20 84.12 84.17

4.50 84.92 84.97

3.60 85.22 85.77

2.80 86.62 86.57

2.35 87.07 86.95

OK To File

7/28/22

4.75
2
57510" - 50
8" -

21

7-R

Tile Chik

R.P.	6.38	77.75 6.75	71.37	31+40	4.68	68.99	68.85				
18		71.00	5.95	65.05	64.95	32+40	4.35	69.32	69.15		
+			5.87	33	4.10	69.57	69.45				
19			5.80	65.20	65.25	34	3.90	69.77	69.75		
+			5.60	35	3.65	70.02	70.05				
20			5.35	65.65	65.55	36	3.25	70.42	70.35		
+		✓	5.32	37	3.12	70.54	70.65				
21			5.20	65.80	65.85	38	2.70	70.97	70.95		
22			4.90	66.10	66.15	39	2.50	71.17	71.25		
23			4.50	66.50	66.45	40	5.21	83.31	78.10	71.55	
24			4.20	66.80	66.75	41	76.76.	76.96	4.70	71.86	71.65
25			3.90	67.10	67.05	42	16"	4.71	72.18	72.15	
26			3.60	67.40	67.35	43	14"	4.50	72.46	72.45	
27			3.45	67.55	67.65	44	4.20	72.76	72.75		
28			3.00	68.00	67.95	45	3.75	73.01	73.05		
29	5.17	80.22	2.10	68.30 75.05	68.25	46	3.64	73.32	73.35		
		655				47	3.32	73.64	73.65		
		73.67									

22

83.21

76.96

7-R 3.72

90.64

H0547

4.15 79.16 79.13

47+50 4.16

2.10 72.86 72.80

48

3.00 72.96 73.95

49+35

74.25

49+60

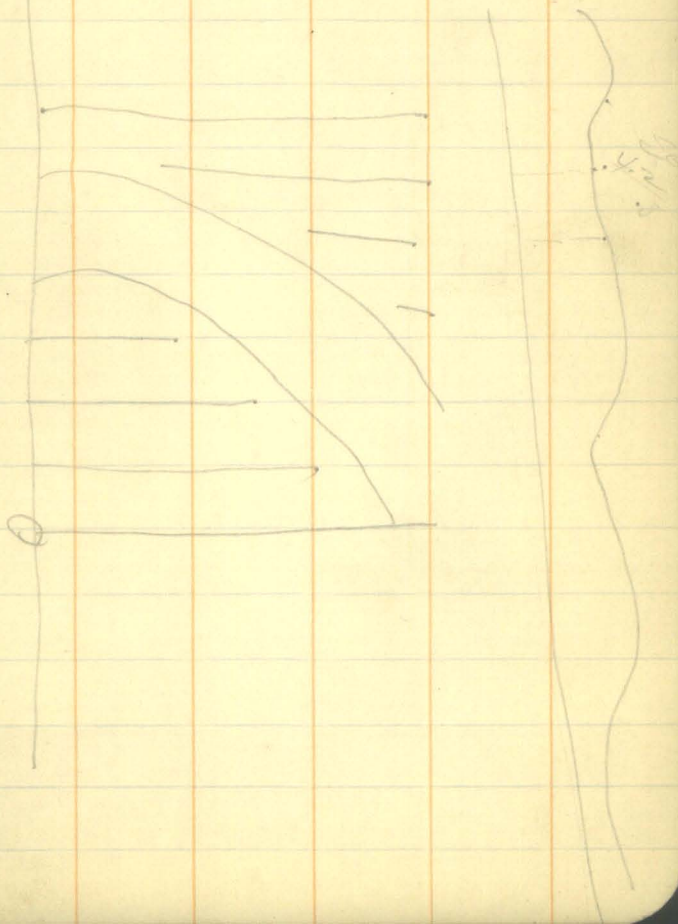
2.50 74.46 74.43

50

2.55 74.41 74.55

H0550

3.23 79.98 79.91



23

chic T-R

$$\begin{array}{r} 4.95 \\ 8 \\ \hline 515 \end{array}$$

$$\begin{array}{r} 91.20 \\ 5.75 \\ \hline 86.05 \end{array}$$

$$\begin{array}{r} 4.95 \\ 12 \\ \hline 615 \end{array}$$

$$\begin{array}{r} 4.95 \\ 5.40 \\ \hline 5.30 \end{array}$$

$$\begin{array}{r} 86.90 \\ 5.95 \\ \hline 80.99 \end{array}$$

57+50

$$\begin{array}{r} 86.94 \\ 80.99 \end{array}$$

2.50

50

7.04

86.95

79.91

74.55

58

2.05

78.94

78.95

51

6.32

86.94

80.62

+

1.60

file 50

6.15

80.79

6.20

59

6.17

$$\begin{array}{r} 91.86 \\ 85.91 \end{array}$$

1.25

85.69

79.74

79.75

50+50

6.10

+

5.65

51

6.05

74.74

74.85

60

5.40

80.57

80.55

+

5.80

+

5.15

52

5.72

75.07

75.15

61

86.05

4.75

81.30

81.35

+

5.55

+

4.30

53

5.40

75.29

75.45

62

3.90

82.15

82.15

+

5.30

+

2.60

54

86.94

5.00

75.77

75.75

63

OK. Full
8/25/22
RMB

2.15

82.90

82.95

+

80.99

4.80

+

2.65

55

4.40

76.59

76.55

64

2.30

83.75

83.75

+

4.10

+

1.85

56

3.70

77.29

77.35

65

1.54

84.51

84.55

+

3.20

65+63

1.00

85.05

85.05

57

2.80

78.19

78.15

34

chic
U - Right

75.20

495
8
575

51	8.00	88.62	80.62
		5.75	
		<u>82.87</u>	

0+10	7.57	75.20	75.20
------	------	-------	-------

0+50	7.15		
------	------	--	--

1	6.75	76.12	76.10
---	------	-------	-------

2	5.90	76.97	77.00
---	------	-------	-------

3	5.00	77.87	77.90
---	------	-------	-------

4	4.05	78.82	78.80
---	------	-------	-------

5	3.10	79.77	79.70
---	------	-------	-------

6	2.15	80.72	80.60
---	------	-------	-------

T.P.	5.07	86.61	<u>1.23</u> 81.54
------	------	-------	-------------------

7	4.75	81.86	81.50
---	------	-------	-------

8	4.20	82.41	82.40
---	------	-------	-------

9	3.25	83.36	83.30
---	------	-------	-------

10	2.50	84.11	84.20
----	------	-------	-------

10+ End	1.10	84.51	84.71
---------	------	-------	-------

Tid

8/2 5/22

RRB

56	85.26 61.5 79.11	CHIC	4.95 1.75 67.5	95.26 1	74.40	4.16	4.95	4.95	82.06	76.11	76.00
		T- Right	8/25/22	8			85.26 5.95	3.20			
50	5.25	85.26 5.95	79.71			7.02	79.21 89.08				
0		79.31	4.95	74.26	74.40	8+50	82.13 82.93	6.70			
0+50		79.11	4.65			9		6.30	76.83	76.85	
1			4.55	74.76 74.56	74.60	+		5.90			
+			4.05			10	83.13	5.68	77.45	77.70	
2			4.35	74.96 74.76	74.80	10+50		5.40			
+			4.26			11		4.80	78.33	78.55	
3			4.15	75.16 74.96	75.0	+		4.50			
+			4.05			12		3.90	79.23	79.40	
4			4.00	75.21 75.11	75.20	+		3.30			
+			3.90			13		3.10	80.03	80.25	
5			3.75	75.56 75.36	75.40						
+			3.68								
6			3.60	75.71 75.51	75.60						
4			3.45								
7			3.35	75.96 75.76	75.80						
+			3.25								

24

file check
O-R

8/17/22

Spice Mill

$$\begin{array}{r} 74.30 \\ 83.89 \quad 4.5 \\ \hline 77.74 \end{array}$$

$$\begin{array}{r} 4.5 \\ 1.2 \\ \hline 6.5 \end{array}$$

$$\begin{array}{r} 83.89 \\ 6.5 \\ \hline 77.74 \end{array}$$

27

P-R chik

89.32

5.95

83.37

4.20

79.17

79.30

19

98.15

92.40

5.30

87.10

87.10

6

20

4.75

87.65

87.70

+

2.90

21 laid 21450

4.20

88.20

88.30

7

2.60

77.77

79.90

22 Hly

4.80

92.31

+

3.20

8

2.20

80.57

80.50

Hly 8

6.97

92.63

5.95

86.68

3.66

85.66

85.63

6.20

80.48

80.50

9

5.60

81.08

81.10

10

5.05

81.63

81.70

11

4.50

82.16

82.30

12

3.95

82.72

82.90

13

3.45

83.23

83.50

14

2.80

83.88

84.10

15

2.10

84.58

84.70

16 8"

86.88

1.70

85.18

85.30

17

6.50

98.15

5.75

92.40

0.98

85.90

85.90

18

5.90

86.50

86.50

478
85
51592.63
575
8688

30

#1

Cont Book 8-195

Q - Right

~~8 8.76 77.16 68.40~~
~~9 8.05 77.05 69.00~~

8 8.76 81.57 72.87

9 8.05 81.51 73.46

10 7.08 81.48 74.40

10 8.52 7.08 74.44 69.60

11 5.99 75.53 70.20

12 5.71 75.81 71.60

12+90 9.20 86.98 2.84 77.68 72.86

13 8.89 78.09 73.00

14 7.45 79.53 74.40

15 6.15 80.83 75.80

16 5.50 81.48 77.20

17 4.69 82.29 77.60

18 4.67 82.21 78.00

19 4.51 82.47 78.40

20 4.30 82.68 78.80

20+6. End 3.15 83.83 79.00

$$\begin{array}{r} 69.60 \\ 14.0 \\ \hline 83.60 \\ 16.0 \\ \hline 99.60 \\ 12.0 \\ \hline 111.60 \\ 12.0 \\ \hline 123.60 \\ 12.0 \\ \hline 135.60 \end{array}$$

$$\begin{array}{r} 16 \\ 460 \\ \hline 1380 \\ 7720 \\ \hline 7858 \end{array}$$

4.84

5.33

4.21

4.82

5.09

5.13

5.03

4.28

4.69

4.31

4.07

3.88

4.79

31

CHIC 3L

9/8/22 60x50

$$\begin{array}{r} 4.95 \\ 1.0 \\ \hline 6.35 \\ 75.42 \\ \hline 81.77 \end{array}$$

$$\begin{array}{r} 81.77 \\ 6.35 \\ \hline 75.42 \end{array}$$

.4 = 73

Briggs
mathews

BM.	4.22	81.77 6.35 75.42	77.55	61			75.42	5.05	4.90	70.82	70.80
53			7.52	67.90	68.10			4.70			
+			7.20			62		4.40	71.02	71.20	
54			7.20	68.22	68.40	T.F.	5.17	82.34 6.35 76.99	3.60	78.17	
			7.00			62		6.00	70.99	71.20	
55			6.80	68.62	68.70			5.70			
			6.60			63		5.70	71.29	71.60	
56			6.52	68.90	69.00			5.45			
			6.82			64		5.30	71.69	72.00	
57			6.15	69.27	69.30			5.10			
			6.00			65		4.95	72.04	72.40	
58			5.70	69.52	69.60	+		4.70			
			5.65			66		4.40	72.59	72.80	
59			5.45	69.97	70.00			4.10			
			5.40			67		3.80	73.19	73.20	
60			5.30	70.12	70.40	+		3.75			

32

32

$$\begin{array}{r} 81.78 \\ 6.75 \\ \hline 88.53 \end{array}$$

$$\begin{array}{r} 4.85 \\ 1.25 \\ \hline 6.10 \end{array}$$

$$\begin{array}{r} 83.34 \\ 6.15 \\ \hline 89.49 \end{array}$$

68 $\begin{array}{r} 83.34 \\ 6.35 \\ \hline 76.99 \end{array}$ 3.50 63.49 73.60

+ 3.30

69 3.10 73.89 74.00

+ 3.00

70 $\begin{array}{r} 83.34 \\ 77.19 \end{array}$ 3.00 74.19 74.40

+ 4.35 $\begin{array}{r} 84.84 \\ 6.15 \\ \hline 78.69 \end{array}$ 2.85 80.49

71 78.69 4.20 74.40 74.80 4.05 78

+ 3.95

4.05 5.00 79.84 80

72 3.70 74.99 75.20 79

+ 3.60

73 3.40 75.29 75.60

4.05 73 3.76 81.08 79

+ 3.05

74 2.65 76.04 76.20 80

+ 2.40

75 2.10 76.59 76.90 82

+

6.06

76

+

77

+

4.05 78

78

80

79

78

+

79

80

81

82

$$\begin{array}{r} 80.84 \\ 6.15 \\ \hline 78.69 \end{array}$$

$$\begin{array}{r} 89.57 \\ 6.15 \\ \hline 83.42 \end{array}$$

83.42

5.90

5.60

5.10

6.56

6.56

4.64

5.64

89.78

4.80

4.00

3.90

$$\begin{array}{r} 89.78 \\ 83.83 \end{array}$$

3.60

3.00

2.15

1.73

1.73

6.05

5.90

5.60

5.10

6.56

83.25

85.13

84.13

4.73

4.80

4.00

3.90

3.60

3.00

2.15

2.15

82.11

77.37

78.25

77.82

78.01

83.01

83.25

85.13

84.13

78.90

79.49

79.49

80.23

80.23

80.94

81.74

81.74

3.1

82

89.78

83.83

1.35

88.42

81.74

82.54

82.48

6.20

95.23

5.95

89.28

6.10

83.18

83.34

84

8.5

5.20

84.14

86

4.45

87

88

4/8/22

2.80

89

2.00

87.28

87.34

89+35

1.70

9

4.95

4.95

5.75

0

1

2

3

4

5

6

7

8

9

10

11

12

12+10

13 End

0-Left

95.23

5.75

89.48

2.25

87.23

87.10

2.10

87.38

87.50

1.55

87.90

1.30

88.18

88.20

8.40

96.94

0.94

88.54

88.70

8.00

89.10

7.30

89.64

89.50

6.30

90.50

5.40

91.50

91.50

4.20

3.40

2.20

1.30

0.9

CHIC

4.95
8
5.75

L-L aft.

89.78
575

0.405

84.03

6.34

82.44

84.79

0.110

4.80

79.78

79.20

1

4.50

2

4.25

3

4.00

80.03

80.10

4

3.20

5

2.45

6

1.70

82.33

82.50

6+90 End

1.00

OK

9/8/22

M-Loft.

file chr

485
55
495
6
515

96.56
575
90 81

4.00
1.95
2.65

12 5.22 96.54 91.32 86.60

11 6.05 96.59 90.54

96.56
555

13 + 92nd 91.01 2.85 88.16 87.85

12 3.85 87.25

12 4.20 86.81 86.60

11 90.81 4.85 85.96 85.95

10 5.50 85.31 85.30

9 6.30 84.65

8 7.00 83.81 84.00

7 1.35 84.66 7.50 83.31 83.3

6 2.15 82.51 82.7

5 2.70

4 3.30

3 3.90

2 4.80

1 5.30 79.36 79.45

0 5.90

OK
9/9/22
RFB

J. Left.

4.25
80
575

July 0	6.83	86.67	79.84
0		<u>575</u>	
		80.92	6.75 74.17 74.50
1		5.85	75.07 75.15
2		5.30	75.62 75.80
3		4.60	76.32 76.42
4		3.90	77.02 77.12
5		3.40	77.72
6		2.70	78.22 78.42
7	OK	2.10	78.82 79.02
8		1.65	79.27 79.72
9		0.90	79.82
10		0.20	79.92

7+30=0

1

✓

3

6"

8/12 1.85 79.27 79.24

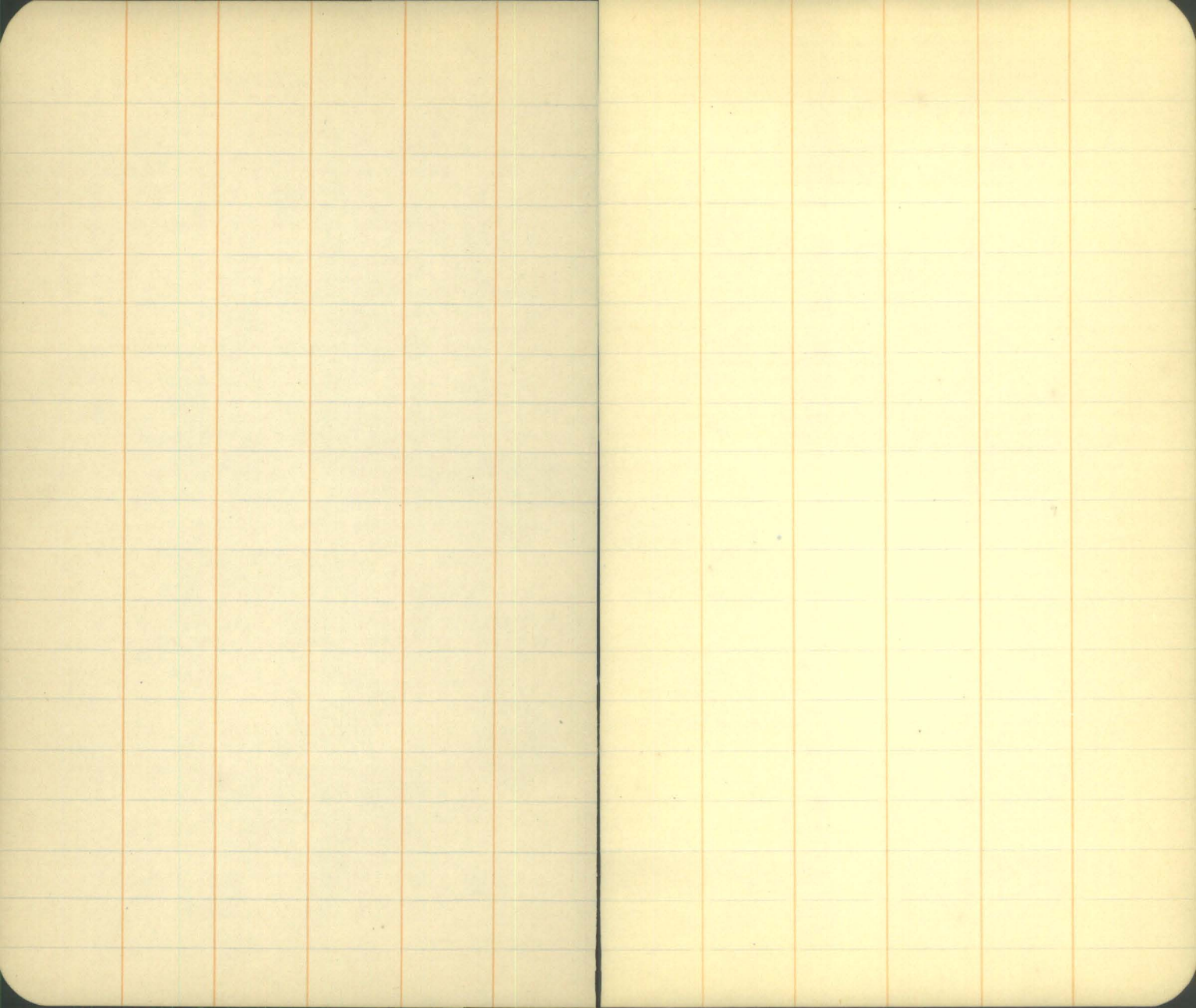
1.50

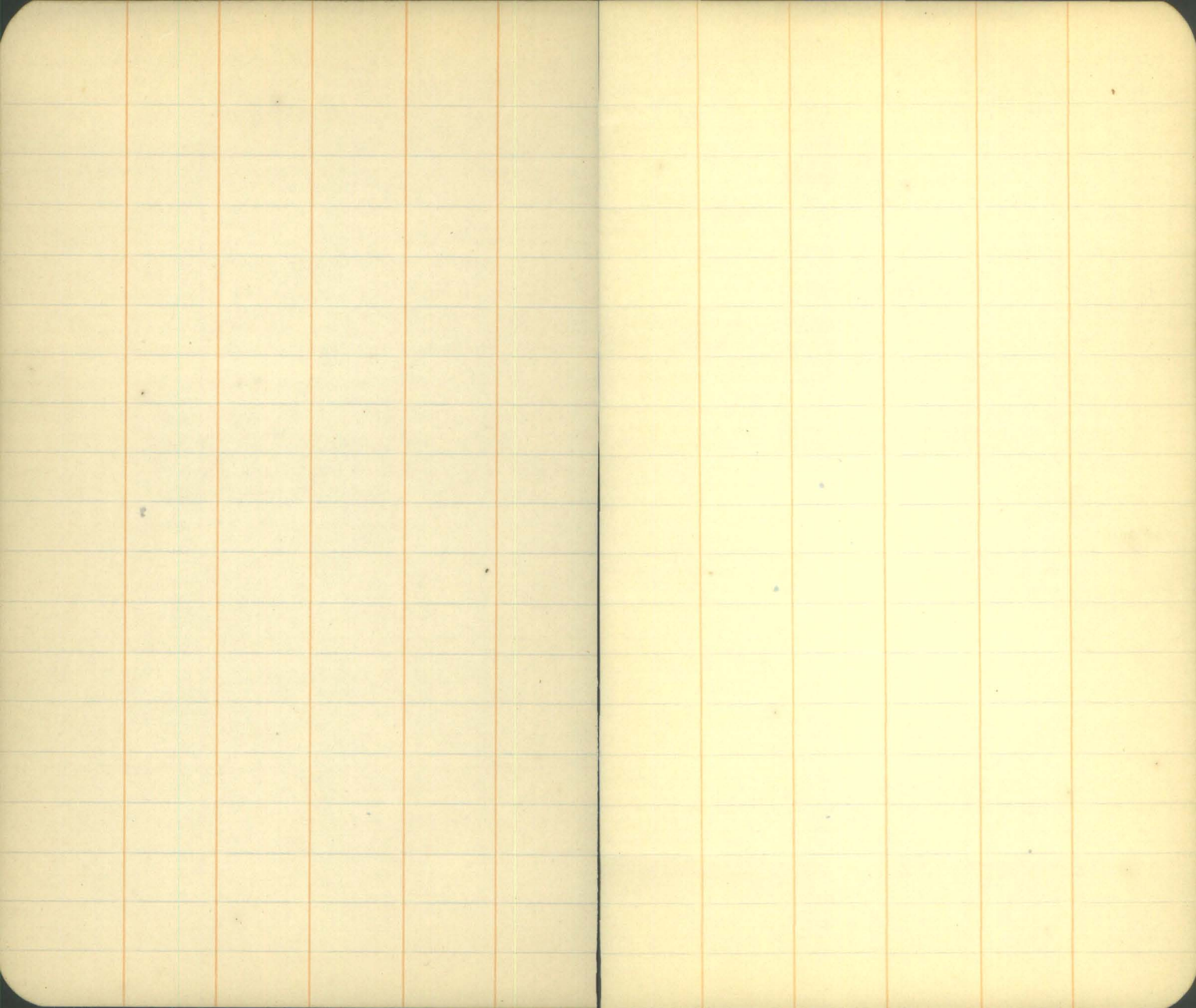
0.50

OK

9/9/22 0.00

8/12





60.04
5.85
54.19

Flan 9997 CHIC
10/9/22
BRA.

1	5.85	60.06	54.21	
1+50	5.24	60.03	54.71	
2	4.94	60.02	55.09	
		60.04		
		<u>59.44</u>		
0		10.10	49.34	49.40
+		9.80		
1		9.55		
+		9.27		
2		9.10	50.24	50.20
+		8.95		
3		8.70		
+		8.50		
4		8.20		
+		8.15		
Hub 4+50		5.49	54.55	
5		8.05	51.39	51.40

	60.04	7.80	Briggs math 1003	
6	59.44			
8.40	60.84	7.60	52.44	
	<u>60.24</u>	8.20		
+		7.93	52.31	52.20
+		7.80		
8		7.50		
+		7.35		
9		7.15		
+		6.70		
10		6.80	53.40	53.40
+		6.65		
11		6.45	53.79	53.60
+				

oil.
R.F.B.

CHK A-1 Flanagan

4+50 A	6.07	60.62	54.55	10
0		$\frac{60.62}{60.12}$		9
+		8.77	51.25	8
1		8.60		7
+		8.45	51.67	6
+		8.30		5
+		8.15	51.80	4+50
+		8.05		4
3		7.85	52.27	3+50
+		7.75		3
4		7.60		(2+50
+		7.25		1
5		7.20	52.92	6+50
6		6.40		1
7		5.65	54.47	0+50
8		4.90	55.22	0
9		4.10	55.10	
		3.80		

CHK A-2

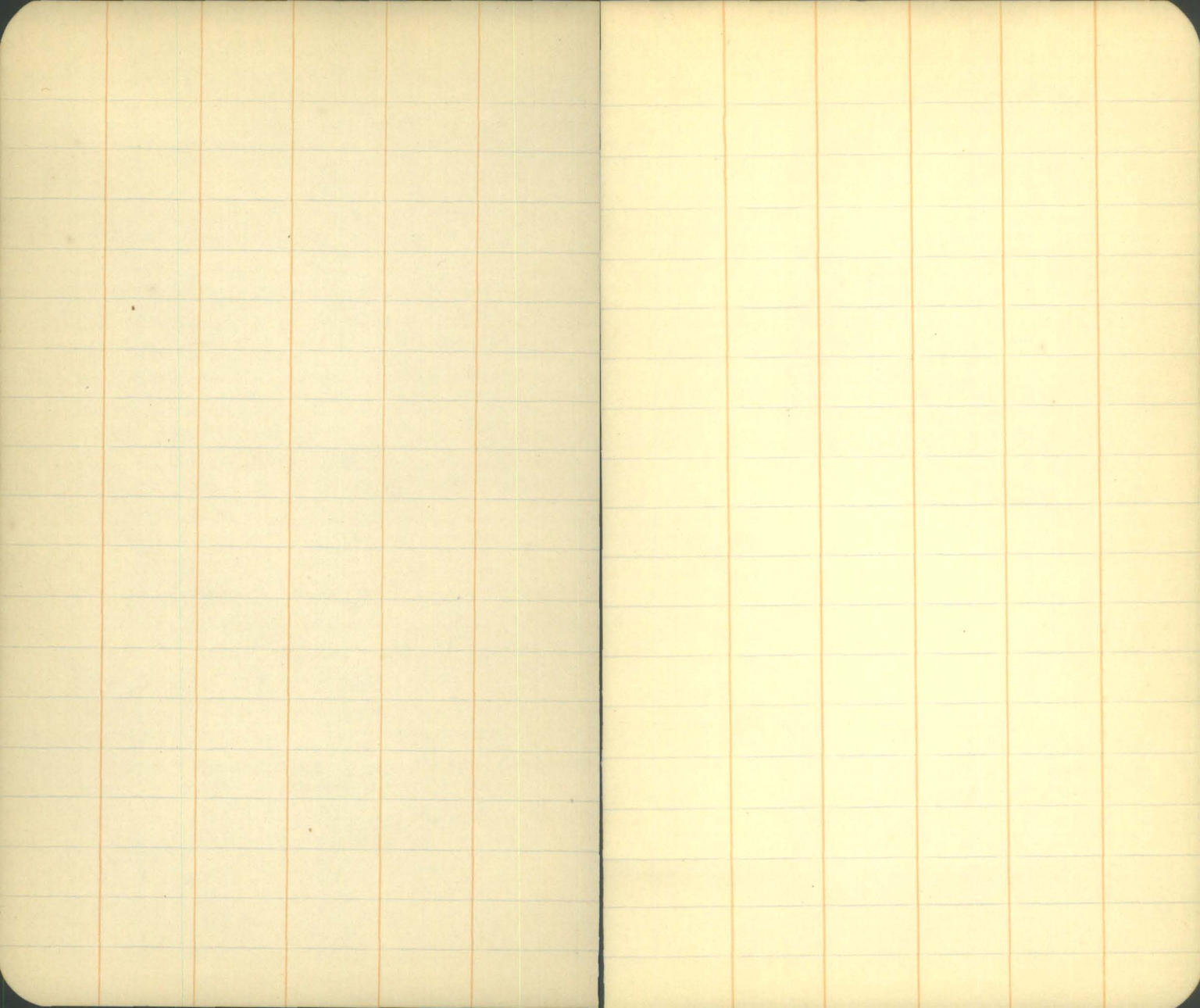
60.12	4.15	55.97	55.90
	4.75		
	5.45		
	6.20		
	6.85		
	7.50		
	7.55		
	7.68		
	7.90		
	8.00		
	8.10		
	8.16		
	8.25		
	8.31		
	8.50		
	8.60	51.52	

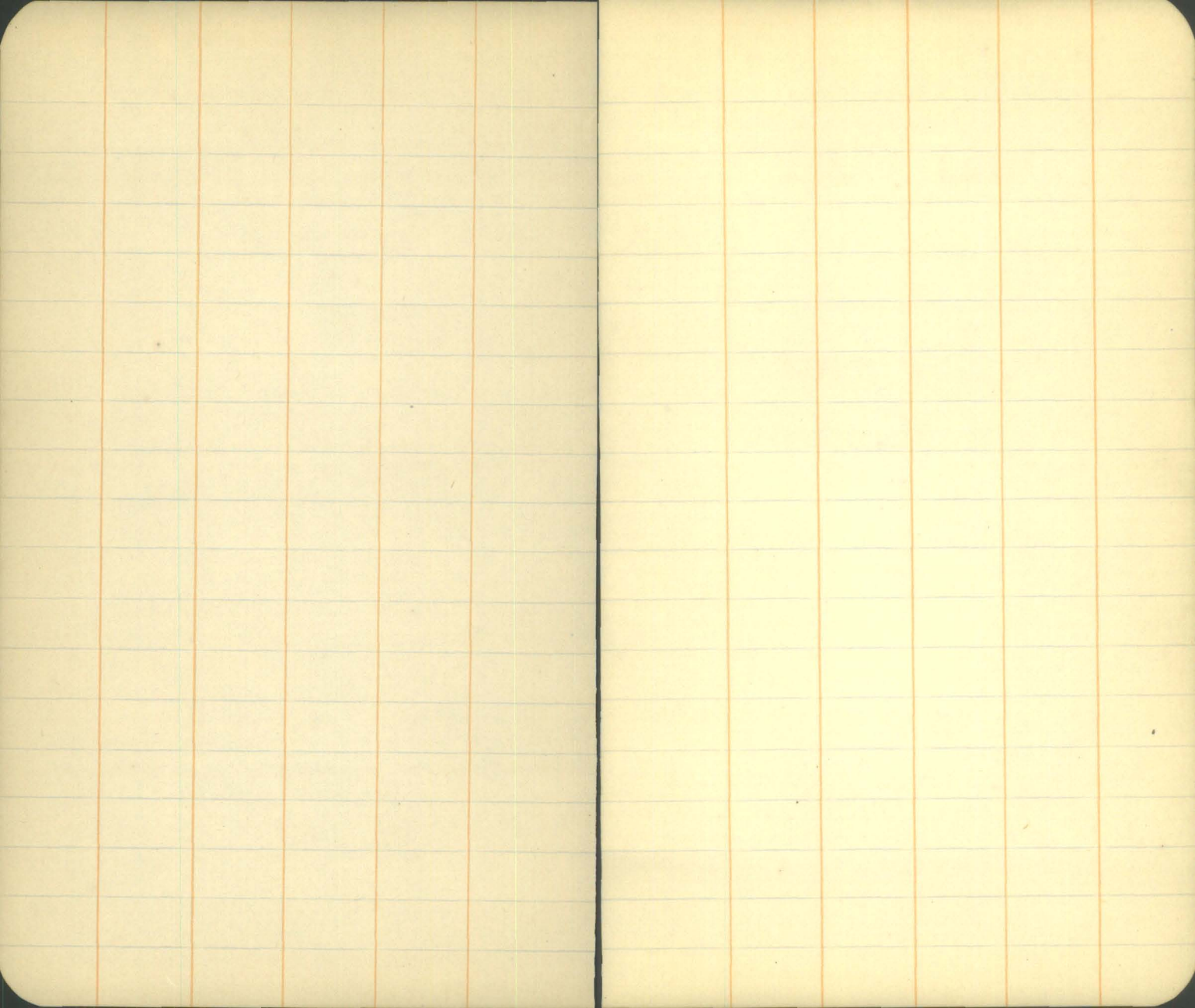
chk
BA B.

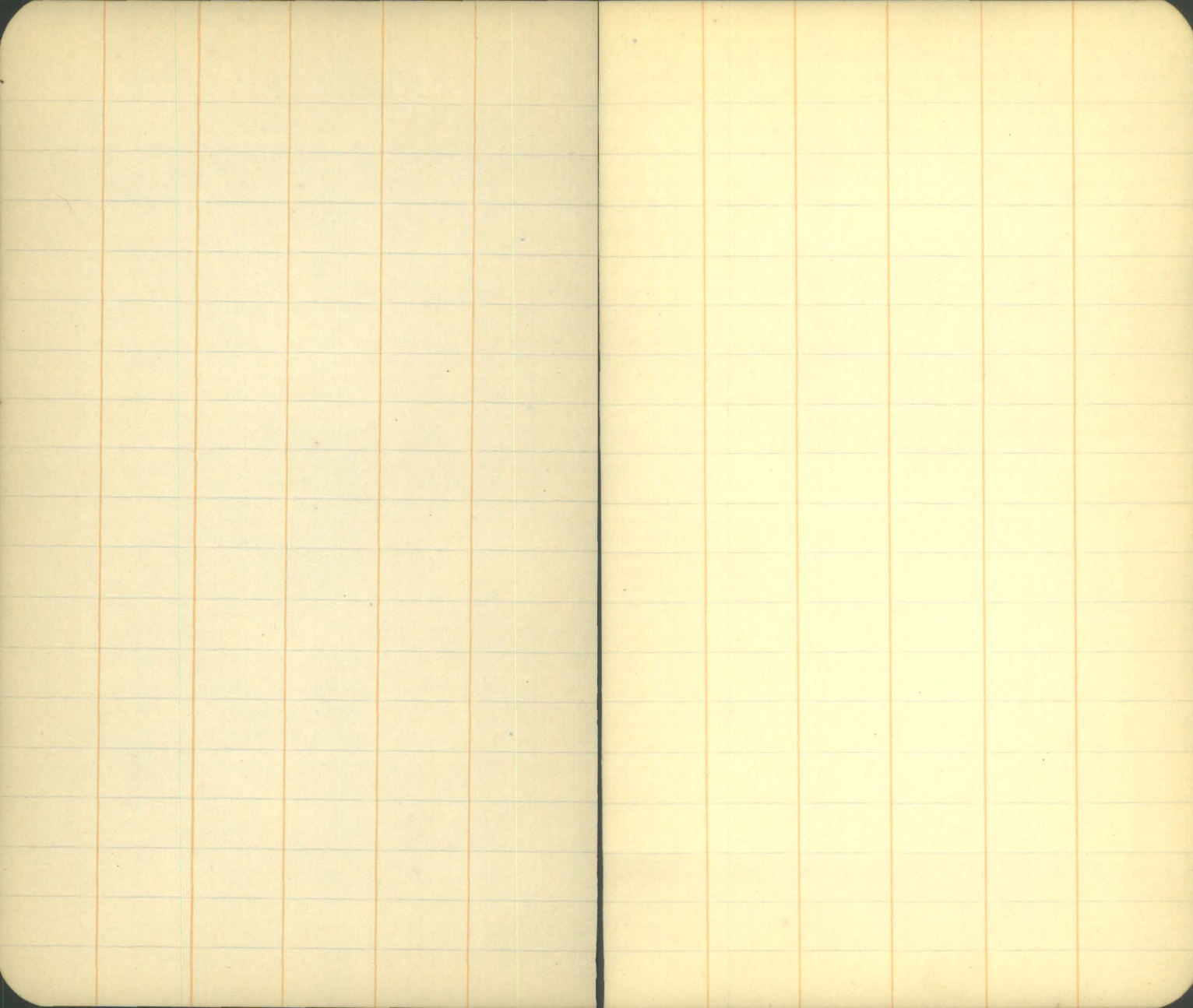
1 BRT	4.95	59.14	54.19	
0		<u>4.60</u> 54.54	5.10 49.44 49.40	
+		4.95		
1		4.65	49.89 49.80	
+		4.45		
2		4.25		
+		4.15		
3		<u>OK</u> 4.00	50.24 50.60	
+		3.80		
4		3.60	50.74 51.00	
5		3.40		
5		1.90	52.64 52.60	
		0.30		

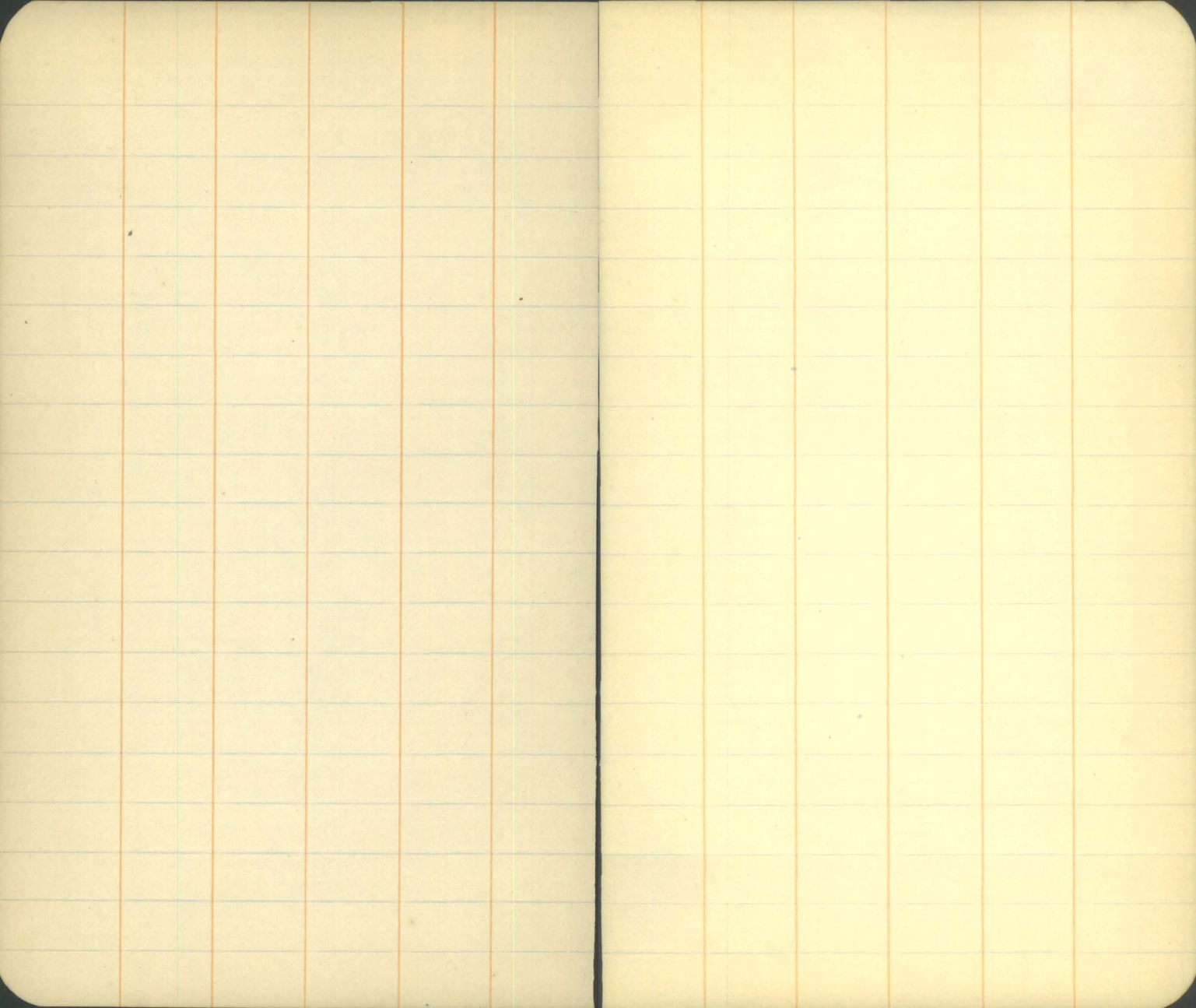
4.60
chk G.

0		54.54	4.35	50.19	50.20
1			3.35		
2			2.35		
3			1.40		
4			0.50		
5			- .50		
		F.			
0		54.54	3.50	51.04	50.97
1			2.40		
2			1.30	53.24	53.37
2+50	5.40	59.25	0.69	53.85	
3			4.90	54.35	54.57
3+50			4.25		
4			3.50		
5			2.50		









4.5 + 50 5.12 60.38

54.76

1

5.14 55.24

1 + 50

4.81 55.57

8.66 51.72

55.24
51.72

3.52

5.00
3.75

.25

500
352

148

51.72
55.57
51.32

3.75

BKF
F/679997

A-1

8.64
5.13
3.51

60.40 11.00 49.40 49.50

0

0 + 50

10.65

1

10.30

1 + 50

9.90

2

9.60

3

8.85 51.62 51.60

4

8.05

5

7.30

6

6.70 53.78 53.70

7

10.71 65.00 6.19 54.80 54.40

8

9.90

9

9.30

10

8.60 56.40 56.50

11

7.75

12

7.05

13

6.45 58.55 50.60

14

5.60

4

4.38 60.31 55.93

5

3.87 60.44 56.57

3

4.21 59.84 55.63

2

5

3.87 60.49 56.62

4

4.38 60.44 56.06

3

4.21 60.38 56.17

2

4.62 60.32 55.71

1

5.12 60.29 55.17

60.30 5.12 55.18

1

5.13 55.13 50.00

~~78~~

Tim Meachy

Private

8/16/22 PM

BRA West

6.83
 4.95
 11.88
 1

77.20 16

99 (SR)	8.54	92.00	83.50	
Top 10"		12.88	(79.16)	
0 Hvy		7.62	84.42	79.40 5.02 $\frac{80}{16}$
1		7.92	84.11	81.00 3.11 $\frac{1}{1}$
2		7.65	84.39	81.30 3.09
3		5.66	86.38	81.60 4.78
4		4.84	87.20	81.90 5.30 $\frac{80}{16}$
5		4.54	87.50	82.20 5.30 $\frac{7}{1}$
6		4.72	87.21	82.50 4.81
7		5.71	86.23	82.80 3.53
8		5.40	86.64	83.10 3.54
9		4.60	87.44	83.70 3.74 $\frac{10}{16}$
10		3.78	88.26	84.30 3.96 $\frac{10}{16}$
11 End		2.70	89.34	84.90 4.44

Tim 1/1/1974

BR 13

583
495
1048
1

OERA 6.00 90.42 84.42

file 13.4 10" 11.48 78.94

O BR 13 6.00 84.42

0 + 90 6.02 84.40

0 BR 13-1

1 6.20 84.22

2 5.48 84.96

2 + 19 5.40 85.02

0 BR 13-2

3 4.92 85.49

3 + 49 4.58 85.84

0 BR. 13-3

4 4.55 85.87

4 + 79 4.08 86.34

0 BR. 13-4

5 4.00 86.42

5 + 96 3.76 86.66

0 BR. 13-5

6 3.74 86.68

7 3.30 87.12

7 + 50 END. 2.50 87.92

T.10 Chick Flamingo
BR D

63.46

5440
10
1500

1 BA.	5.96	60.15	54.19	8	8.30		
0		<u>59.65</u>	10.05 49.60 49.50	+	7.90		
+		9.60		9	7.50	55.96	55.80
1		9.40		+	7.20		
+		9.10		10	6.90		
2		8.80		+	6.50		
+		8.40		11	6.25		
3		8.00	51.65 51.60	+	5.90		
+		7.65		12	5.50	57.96	57.90
4		7.35		+	4.85		
+		7.00		13	4.50	58.96	58.60
5		6.60					
+		6.25					
6	7.86	63.46	6.07 53.58 53.70				
+		9.45					
7		9.10	54.36 54.40				
+		8.15					

Chk BXC Flora 997

2

60.48

9.65

~~52.81~~

50.83

13

63.46

58.50

1+50

10.10

5.00 58.46

1

10.40

12

5.70

0+50

10.75

11

6.40

0

10.90 49.58 49.40

10

7.05

9

7.70

8

8.40 55.06 55.00

7

9.20

6+50

9.50

6

9.75

5+50

7.19

60.48 10.17 52.29

5

7.50

4+50

7.85

4

8.26

3+50

8.63

3

9.05

2+50

9.20

Flam 995

BR. G -

59.91

$$\begin{array}{r} 51.97 \\ 24 \\ \hline 54.37 \end{array}$$

$$\begin{array}{r} 94 \\ 276 \end{array}$$

$$\begin{array}{r} 50.60 \\ 37 \\ \hline 50.97 \end{array}$$

$$\begin{array}{r} 12 \\ 72 \\ \hline 108 \end{array}$$

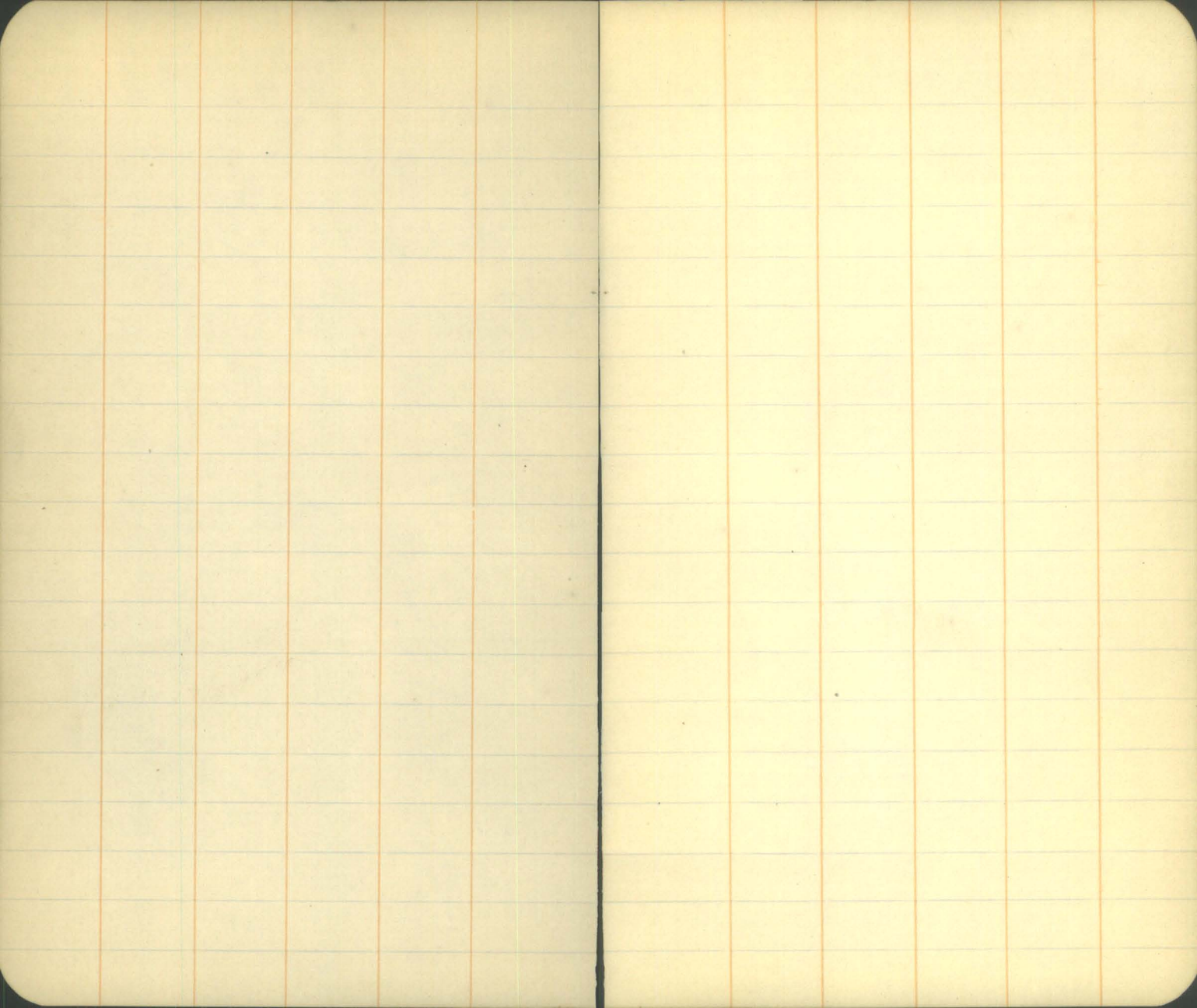
0		3.95	54.96	50.20	3.76
1		5.08	54.82	51.20	3.63
2		4.04	55.87	52.20	3.67 $\frac{10}{10}$
3		3.10	56.81	53.20	3.61 $\frac{10}{10}$
4		2.55	57.36	54.20	3.16
5		1.33	58.58	55.20	3.38

= 2 BR B

BR. F

0		59.91	4.96	54.95	50.97	3.98	
1			3.85	56.06	52.17	3.89	
2			2.79	57.12	53.37	3.75	
2+60	7.27	64.90	2.38	57.53	54.09	3.44	10
2+90			7.22	57.68	54.45	3.23	10
3			7.06	57.84	54.57	3.27	
3+50			6.35	58.55	55.17	3.38	
4			5.41	59.49	55.77	3.72	
5			4.21	60.89	56.97	3.72	

= 3+94 BRB.



54

Br. W. Right 7/26/22

26	6.70	88.80	82.10	
27	6.54	88.69	82.15	
28	6.03	88.65	82.62	
0		88.69	7.03	81.66 75.50 6.16
1			7.00	81.69 76.20 5.49
2			7.22	81.47 76.90 4.57
3			6.15	82.34 77.60 4.94
4			4.90	83.79 78.30 5.49
5			4.57	84.12 79.00 5.12
6			4.22	84.47 79.70 4.77
7			3.97	84.72 80.40 4.32
8	7.64	73.12	3.20	85.49 81.10 4.39
9			6.92	86.20 81.80 4.40
10			6.18	86.95 82.50 4.45
11			5.34	87.79 83.20 4.59
12			4.45	88.68 83.90 4.78
13			3.45	89.68 84.60 5.05

13+85 END

5.60
25.95
195.30
5.60
1.65
1.33
1.55
64.20

26.82.62

75.15

12

75.31

13
1.33
1.55
64.20

.55=36

.5=45

.7=END.

=26+20

8

8

7

7

Cuto 7/26/22 RRP.

Tile chik B

1 6.28 59.92 52.54

0 6.74 59.90 53.16

0. tile. 59.30 9.40 49.40 49.40

0+30 9.90

0+50 9.60

1 9.45 49.85 49.80

4 9.30

2 9.10 50.20 50.20

1 8.90

2 8.60 50.70 50.60

Flanagan

36 50.00
122 49.20 49.40 49.20 49.20
49.40 49.20 49.40 49.20
57.52

Top 8" 9.51 59.51 50.00 49.20

A"

0	59.51	6.28	53.12	49.40	3.73
+ 3)		6.21	53.30	49.52	3.78
+ 50		6.16	53.35	49.60	3.75
1		5.30	54.21	49.80	4.41
+		4.80	54.71	50.00	4.71
2		4.42	55.09	50.20	4.89
+		2.87	55.54	50.40	5.24
3		3.83	55.68	50.60	5.08
+		4.15	55.36	50.80	4.56
4		4.51	55.00	51.00	4.00
+		5.00	54.51	51.20	3.31
5		5.10	54.41	51.40	3.01
+		4.75	54.76	51.60	3.16
6		4.27	55.14	51.80	3.34

56.97

$\frac{25}{22}$ $\frac{20}{25}$ $\frac{25}{100}$
 $\frac{55}{125}$

39.44
 56.97
 96.41

6+50	5.55	59.51	3.85	55.66	52.00	3.66
7		61.21	5.23	55.98	52.20	3.78
+			5.02	56.18	52.40	3.78
8			5.08	56.13	52.60	3.58
+			4.84	56.37	52.80	3.57
9			4.75	56.46	53.00	3.46
+			4.57	56.64	53.20	3.44
10			4.17	57.04	53.40	3.64
+			4.04	57.17	53.60	3.57
11			4.01	57.20	53.80	3.40
+			3.60	57.61	54.00	3.61
12	—	—	—		54.20	

25) 96.41 (3.86
 75
 214
 200
 141

39.44 Ave 3.86

Flanigan
BR. B.

49.40
1.60
51.00

250
1.50
250
50.00

Top 8"	9.29	59.29	50.00	49.20	
0		6.13	53.16	49.40	3.76
0 + 20		6.07	53.23	49.52	3.70
0 + 50		6.01	53.28	49.60	3.68
1		5.75	53.54	49.80	3.74
+		5.57	53.72	50.00	3.72
2		5.25	53.94	50.20	3.74
+		5.08	54.21	50.40	3.81
3		4.82	54.47	50.60	3.87
+		4.47	54.82	50.80	4.02
4		4.18	55.11	51.00	4.11
+		3.76	55.53	51.80	3.73
5		3.18	56.11	52.60	3.51
+		2.30	56.99	53.40	3.59
6		1.55	57.74	54.20	3.54
6 + 50		0.70	58.59	55.00	3.59

20" W. of F. and 8"

Co 5

15/56.11 (3.74)
45
111
105
61

386
374

21760
2.80

56.11 Ave. 3.74

Flanigan

BR-A-1

29
27

4	6.11	61.11	55.00		
5	6.74	61.15	54.41		
3+50	5.78	61.14	55.26		
0 (4+34) _A	61.13	6.47	54.66	51.70	3.46
0+22		6.66	54.47	51.30	3.17
1		6.23	54.90	51.50	3.40
2		5.90	55.23	51.80	3.43 ⁸⁰
3		5.50	55.63	52.10	3.53 ⁷⁸
4		5.20	55.93	52.40	3.52
4+29		5.13	56.00	52.49	3.51
5		4.56	56.57	52.70	3.87
6		4.32	56.81	52.80	3.81
7		3.54	57.59	54.30	3.29 ⁸⁰
8		2.77	58.34	55.10	3.24 ⁸
9		1.78	59.35	55.90	3.45
10 END.		0.60	60.53	56.70	3.83

13/45.02 (3.50)
29
60

45.02 AVE 3.50

Fla., 1927

8/15/22

4 PM.

BR A-2

0 (4+37) A.	61.12	6.89	54.24	51.40
0+33		6.40	54.73	51.47
1		5.96	55.17	51.60
2		5.42	55.71	51.80
3		4.96	56.17	52.00
4		5.07	56.06	52.20
4+54		4.58	56.55	52.32
5		4.51	56.62	52.40
6		4.02	57.10	53.10
7		3.42	57.71	53.80
8		2.73	58.40	54.50
9		2.25	58.68	55.20
10 End		1.54	59.59	55.90

7.63	7.63
53	5
812	8.13
430	4.30
3.82	3.83

26	2 =
8.50	
4.12	
3.88	

7.60
7.45
7.00
7.20

7.84

2.26

2.57

3.91

4.17

3.86

4.23

4.22

4.00

3.91

3.90

3.68

3.69

49 24

AVE 3.80

13/49.24	3.80
39	
102	

= 5 = 0 A-3

KRS, checked.

BR A-3

0	61.13	4.51	56.62	52.40	4.22
1		2.94	57.19	53.10	4.09
2		3.45	57.68	58.80	3.88 $\frac{1}{10}$
3		2.90	58.23	54.50	3.72 $\frac{1}{10}$
4		2.39	58.74	55.20	3.54
5 End.		1.76	59.27	55.90	3.47

2293

C1/K

1	60.12	6.20	53.30	52.10
2		6.10		
3	<u>01L</u>	5.40		
4		4.80		
5		4.00		

6/22.93 (3.80)
 $\frac{15}{49}$

AVE. 3.80
 3.80
 3.50
 $\frac{3}{11.10}$ (2.70)
 $\frac{9}{21}$

7.84
 $\frac{53}{8.30}$
 $\frac{4.80}{35.3}$ = 5/10 5+00 A-2

-7.60
 -7.80
 -7.80
 8.00

Flanagan

BR E

1 (12)	7.94	61.48	53.54	
2 (12)	7.53	61.47	53.94	
O = (0+30) 3.		8.23	53.24	49.50 3.74
0+50		8.01	53.46	49.85 2.61
0+90		7.80	53.67	50.13 2.54
1		7.70	53.77	50.20 2.57
2		7.04	54.42	50.90 2.52
3		6.11	55.36	51.60 2.76
4		5.07	56.40	52.30 4.10
5		4.21	57.26	53.00 4.26
6		3.85	57.62	53.70 3.92
7		3.55	57.92	54.40 3.52
8		3.07	58.40	55.10 2.80
9		2.30	59.17	55.80 2.37
10	65.54	1.61	59.86	56.50 2.26
11		4.92	60.62	57.20 3.42
12		4.15	61.39	57.90 3.49
13		3.18	62.36	58.60 3.76
14		2.36	63.18	59.30 3.88

A-2

rod readings

0	8.50
0+50	8.40
0+75	8.20
1	8.16
1+25	8.18
1+50	8.13
1+75	8.00
2	7.95
2+50	8.00
3	7.80

- 7% all

3.6

BR. C.

0=0	61.47	8.11	53.36	49.40	3.96
1		7.60	53.87	50.10	3.77
2		7.13	54.34	50.80	3.54
3		6.28	55.09	51.50	3.59
4		5.56	55.91	52.20	3.71
5		4.98	56.49	52.90	3.59
6		4.48	56.99	53.60	3.39
7		3.82	57.64	54.30	3.24
8		2.95	58.52	55.00	3.52
9		2.11	59.36	55.70	3.66
10	5.47	65.54	11.40	60.07	56.40
11		4.70	60.84	57.10	3.74
12		3.85	61.69	57.80	3.89
13 End.		3.02	62.52	58.50	4.02

= 46' up Bet 10th County

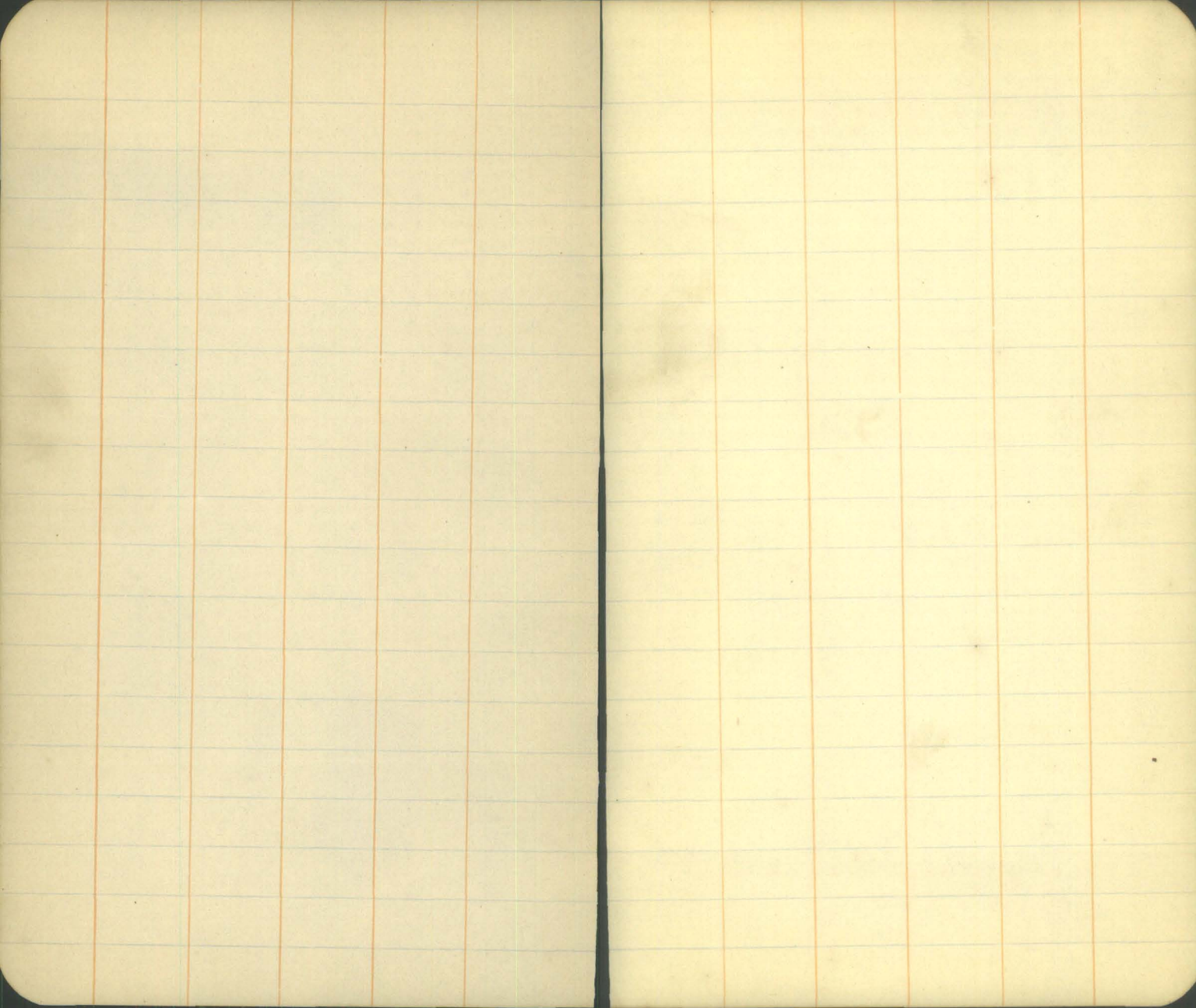
7.0

3.6

BR. D.

0 = 0 + 30 A.	61.47	8.10	52.37	49.50	3.87
0 + 60		7.38	54.09	49.92	4.17
1		7.18	54.29	50.20	4.09
2		6.70	54.77	50.90	3.87
3		6.15	55.32	51.60	3.72
4		5.60	55.87	52.30	3.57
5		5.12	56.35	52.00	3.35
6		4.39	57.08	53.70	3.28
7		3.83	57.64	54.40	3.24
8		2.77	58.70	55.10	3.60
9		1.95	59.52	55.80	3.72
10	65.54	0.74	60.53	56.50	4.03
11		4.51	61.03	57.20	3.82
12		3.48	61.86	57.90	3.96
13 End		2.75	62.59	58.60	3.99

3.7



SEC. 1

25-12" intakes

2-15"

40 trees

SEC. 2

10-12" intakes

4-15"

12 trees

SEC. 3

11-12" intakes

2-15"

SEC. 4

11-12" intakes

6-15" "

SEC. 5

15-12" intakes

3-15" "

6/26/22

SEC. 4.

Check T&W system

Stake out 17. small lines -

SEC. 6

2-40' 10" Cor. Pipe

4-20' 12"

120'-10" S.P.

#12

Repair Man #12

Telephone Bk 2825

Nels.

Constr. Levels Drain #9

BR 3-Left

Mch-15-22

Hoff

H. Gole

st+20 Tile	10.63	20.00	9.37 - 1.4 = 7.97
st+Hub	6.10	13.90	7.89
55	5.83	14.17	8.29
5.6	5.19	14.81	8.69
57	4.18	15.82	9.09
+50	3.84	16.16	9.29
58	3.82	16.18	9.49
B.M.	2.91	17.09	

= Cor. El ^{st+20} Top of 14" tile sta st+20

$\frac{5.4}{.4}$
13.8

6.01

5.88

6.12

6.73

6.87

6.69

N. Hwy E

N.E. Cor. N. Head wall

Conc. Hwy Culv W. of Sta 57+15

Drove 1 1/2" Oak
hubs and gage
tile grade at Sta
st+20 as laid
from old Grades
assumed Elev of
7.97

Whalers - Schuler

Ed. Smith Dewar Smith

Bros store -

Pomer Twp.

Sewer Pipe + Corr. Culv

Conn. Y-T Johnsons

1 12" x 20' Corr. Pipe
3 10" x 20' Corr. Pipe
14 18" x 2' Sewer pipe.
27 12" x 22' Sewer pipe.
29 10" x 2' Sewer pipe.
9' - Tile.

1 12' x 6" 1 - 18 x 10

1 8' x 6 1 - 10 x 6

1 10 x 8 1 - 18 x 12

1 18 x 6

2 18 x 8

TABLE IX.—CALCULATION OF EARTHWORK.

Width	HEIGHT														
	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15
1	.02	.04	.06	.07	.09	.11	.13	.15	.17	.18	.20	.22	.24	.26	.28
2	.04	.07	.11	.15	.18	.22	.26	.30	.33	.37	.41	.44	.48	.52	.56
3	.06	.11	.17	.22	.28	.33	.39	.44	.50	.56	.61	.67	.72	.78	.83
4	.07	.15	.22	.30	.37	.44	.52	.59	.67	.74	.81	.89	.96	1.04	1.11
5	.09	.19	.28	.37	.46	.56	.65	.74	.83	.93	1.02	1.11	1.20	1.30	1.39
6	.11	.22	.33	.44	.56	.67	.78	.89	1.00	1.11	1.22	1.33	1.44	1.55	1.67
7	.13	.26	.39	.52	.65	.78	.91	1.04	1.16	1.30	1.42	1.55	1.68	1.81	1.94
8	.15	.30	.44	.59	.74	.89	1.04	1.19	1.33	1.48	1.63	1.78	1.92	2.08	2.22
9	.17	.33	.50	.67	.83	1.00	1.17	1.33	1.50	1.67	1.83	2.00	2.17	2.33	2.50
10	.18	.37	.56	.74	.93	1.11	1.30	1.48	1.67	1.85	2.04	2.22	2.41	2.59	2.78
11	.20	.41	.61	.82	1.02	1.22	1.43	1.63	1.83	2.04	2.24	2.44	2.65	2.85	3.06
12	.22	.44	.67	.89	1.11	1.33	1.56	1.78	2.00	2.22	2.44	2.67	2.89	3.11	3.33
13	.24	.48	.72	.96	1.20	1.44	1.68	1.92	2.16	2.41	2.65	2.89	3.13	3.37	3.61
14	.26	.52	.78	1.04	1.30	1.55	1.81	2.08	2.33	2.59	2.85	3.11	3.37	3.63	3.89
15	.28	.56	.83	1.11	1.39	1.67	1.94	2.22	2.50	2.78	3.06	3.33	3.61	3.89	4.17
16	.30	.59	.89	1.18	1.48	1.78	2.07	2.37	2.67	2.96	3.26	3.56	3.85	4.15	4.44
17	.31	.63	.94	1.26	1.57	1.89	2.20	2.52	2.83	3.15	3.46	3.78	4.09	4.41	4.72
18	.33	.67	1.00	1.33	1.67	2.00	2.33	2.67	3.00	3.33	3.67	4.00	4.33	4.67	5.00
19	.35	.70	1.06	1.41	1.76	2.11	2.46	2.82	3.17	3.52	3.87	4.22	4.57	4.92	5.28
20	.37	.74	1.11	1.48	1.85	2.22	2.59	2.96	3.33	3.70	4.07	4.44	4.81	5.18	5.56
21	.39	.78	1.17	1.55	1.94	2.33	2.72	3.11	3.50	3.89	4.28	4.67	5.06	5.44	5.83
22	.41	.81	1.22	1.63	2.04	2.44	2.85	3.26	3.67	4.07	4.48	4.89	5.30	5.70	6.11
23	.43	.85	1.28	1.70	2.13	2.56	2.98	3.41	3.83	4.26	4.68	5.11	5.54	5.96	6.39
24	.44	.89	1.33	1.78	2.22	2.67	3.11	3.56	4.00	4.44	4.89	5.33	5.78	6.22	6.67
25	.46	.92	1.39	1.85	2.31	2.78	3.24	3.70	4.17	4.63	5.09	5.56	6.02	6.48	6.94
26	.48	.96	1.44	1.92	2.41	2.89	3.37	3.85	4.33	4.82	5.30	5.78	6.26	6.74	7.24
27	.50	1.00	1.50	2.00	2.50	3.00	3.50	4.00	4.50	5.00	5.50	6.00	6.50	7.00	7.50
28	.52	1.04	1.55	2.07	2.59	3.11	3.63	4.15	4.67	5.18	5.70	6.22	6.74	7.26	7.78
29	.54	1.07	1.61	2.15	2.68	3.22	3.76	4.30	4.83	5.37	5.91	6.44	6.98	7.52	8.06
30	.56	1.11	1.67	2.22	2.78	3.33	3.89	4.44	5.00	5.55	6.11	6.67	7.22	7.78	8.33
31	.57	1.15	1.72	2.30	2.87	3.44	4.02	4.59	5.17	5.74	6.32	6.89	7.46	8.04	8.61
32	.59	1.18	1.78	2.37	2.96	3.56	4.15	4.74	5.33	5.92	6.52	7.11	7.70	8.30	8.89
33	.61	1.22	1.83	2.43	3.05	3.67	4.28	4.89	5.50	6.11	6.72	7.33	7.94	8.55	9.17
34	.63	1.26	1.89	2.52	3.15	3.78	4.40	5.04	5.67	6.29	6.93	7.56	8.18	8.81	9.44
35	.65	1.30	1.94	2.59	3.24	3.89	4.53	5.18	5.83	6.48	7.13	7.78	8.42	9.08	9.72
36	.67	1.33	2.00	2.67	3.33	4.00	4.66	5.33	6.00	6.67	7.33	8.00	8.67	9.33	10.00
37	.68	1.37	2.06	2.74	3.42	4.11	4.79	5.48	6.17	6.85	7.54	8.22	8.91	9.59	10.28
38	.70	1.41	2.11	2.82	3.52	4.22	4.92	5.63	6.33	7.03	7.74	8.44	9.15	9.85	10.56
39	.72	1.44	2.17	2.89	3.61	4.33	5.05	5.78	6.50	7.22	7.95	8.67	9.39	10.11	10.83
40	.74	1.48	2.22	2.96	3.70	4.44	5.18	5.92	6.67	7.41	8.15	8.89	9.63	10.37	11.11

Table gives cu. yds. in 1 ft. of a triangle of given width and height. Corrections for tenths of width are one tenth the values found under each height considering the widths from 1 to 9 as tenths and similarly the corrections for tenths of height are one tenth the figures opposite width considering the heights from 1 to 9 as tenths. Thus if $w = 16.2$ and $h = 5.3$, cu. yds. $= 1.48 + .028 + .089 = 1.597$ cu. yds. or practically 160 cu. yds. per 100 ft. If w exceeds 40 ft., use one half and multiply result by 2, if both w and h are large use one half of each and multiply result by 4. Any cross-section may be divided into figures following the following rule. To the triangle of the sum of the outside cuts (or fills) $= h$, and $\frac{1}{2}$ the roadbed $= w$, add the triangles formed by taking the distance out to each break in turn ($= w$'s) by the difference between the cuts (or fills) on each side of it ($= h$'s) always subtracting the outer from the inner.

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

Roadway 16 feet wide.

Side Slopes 1 on 1½

For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.2	8.3	8.5	8.6	8.8	8.9	9.1	9.2	9.4	0
1	9.5	9.7	9.8	10.0	10.1	10.3	10.4	10.6	10.7	10.9	1
2	11.0	11.2	11.3	11.5	11.6	11.8	11.9	12.1	12.2	12.4	2
3	12.5	12.7	12.8	13.0	13.1	13.3	13.4	13.6	13.7	13.9	3
4	14.0	14.2	14.3	14.5	14.6	14.8	14.9	15.1	15.2	15.4	4
5	15.5	15.7	15.8	16.0	16.1	16.3	16.4	16.6	16.7	16.9	5
6	17.0	17.2	17.3	17.5	17.6	17.8	17.9	18.1	18.2	18.4	6
7	18.5	18.7	18.8	19.0	19.1	19.3	19.4	19.6	19.7	19.9	7
8	20.0	20.2	20.3	20.5	20.6	20.8	20.9	21.1	21.2	21.4	8
9	21.5	21.7	21.8	22.0	22.1	22.3	22.4	22.6	22.7	22.9	9
10	23.0	23.2	23.3	23.5	23.6	23.8	23.9	24.1	24.2	24.4	10
11	24.5	24.7	24.8	25.0	25.1	25.3	25.4	25.6	25.7	25.9	11
12	26.0	26.2	26.3	26.5	26.6	26.8	26.9	27.1	27.2	27.4	12
13	27.5	27.7	27.8	28.0	28.1	28.3	28.4	28.6	28.7	28.9	13
14	29.0	29.2	29.3	29.5	29.6	29.8	29.9	30.1	30.2	30.4	14
15	30.5	30.7	30.8	31.0	31.1	31.3	31.4	31.6	31.7	31.9	15
16	32.0	32.2	32.3	32.5	32.6	32.8	32.9	33.1	33.2	33.4	16
17	33.5	33.7	33.8	34.0	34.1	34.3	34.4	34.6	34.7	34.9	17
18	35.0	35.2	35.3	35.5	35.6	35.8	35.9	36.1	36.2	36.4	18
19	36.5	36.7	36.8	37.0	37.1	37.3	37.4	37.6	37.7	37.9	19
20	38.0	38.2	38.3	38.5	38.6	38.8	38.9	39.1	39.2	39.4	20
21	39.5	39.7	39.8	40.0	40.1	40.3	40.4	40.6	40.7	40.9	21
22	41.0	41.2	41.3	41.5	41.6	41.8	41.9	42.1	42.2	42.4	22
23	42.5	42.7	42.8	43.0	43.1	43.3	43.4	43.6	43.7	43.9	23
24	44.0	44.2	44.3	44.5	44.6	44.8	44.9	45.1	45.2	45.4	24
25	45.5	45.7	45.8	46.0	46.1	46.3	46.4	46.6	46.7	46.9	25
26	47.0	47.2	47.3	47.5	47.6	47.8	47.9	48.1	48.2	48.4	26
27	48.5	48.7	48.8	49.0	49.1	49.3	49.4	49.6	49.7	49.9	27
28	50.0	50.2	50.3	50.5	50.6	50.8	50.9	51.1	51.2	51.4	28
29	51.5	51.7	51.8	52.0	52.1	52.3	52.4	52.6	52.7	52.9	29
30	53.0	53.2	53.3	53.5	53.6	53.8	53.9	54.1	54.2	54.4	30
31	54.5	54.7	54.8	55.0	55.1	55.3	55.4	55.6	55.7	55.9	31
32	56.0	56.2	56.3	56.5	56.6	56.8	56.9	57.1	57.2	57.4	32
33	57.5	57.7	57.8	58.0	58.1	58.3	58.4	58.6	58.7	58.9	33
34	59.0	59.2	59.3	59.5	59.6	59.8	59.9	60.1	60.2	60.4	34
35	60.5	60.7	60.8	61.0	61.1	61.3	61.4	61.6	61.7	61.9	35
36	62.0	62.2	62.3	62.5	62.6	62.8	62.9	63.1	63.2	63.4	36
37	63.5	63.7	63.8	64.0	64.1	64.3	64.4	64.6	64.7	64.9	37
38	65.0	65.2	65.3	65.5	65.6	65.8	65.9	66.1	66.2	66.4	38
39	66.5	66.7	66.8	67.0	67.1	67.3	67.4	67.6	67.7	67.9	39
40	68.0	68.2	68.3	68.5	68.6	68.8	68.9	69.1	69.2	69.4	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 41.9. For same slopes but other widths of roadbed correct above figures by one-half difference in width of roadbed; thus in example above for 20 ft. roadbed distance will be $41.9 + (20 - 16) \div 2$ or 2 ft. added to 41.9 = 43.9. For slopes of 1 on 1 see inside of front cover.