

Dr. #9 BLACK HAWK

1083

BOOK 4

LEVEL BOOK

370

LEVELS

KEUFFEL & ESSER CO.

DRAWING MATERIALS

AND

SURVEYING INSTRUMENTS.

NEW YORK.

CHICAGO. ST. LOUIS. SAN FRANCISCO. MONTREAL.

Tables for Excavations and Embankments.

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

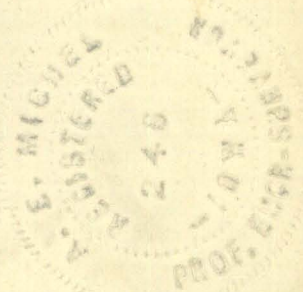
ROADWAY 18 FEET WIDE. SIDE SLOPES 1 TO 1.

FOR SINGLE TRACK EXCAVATION.

"Copyright, 1895, by Keuffel & Esser Co."

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	0
1	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	1
2	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	2
3	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	3
4	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	4
5	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	5
6	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	6
7	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	7
8	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	8
9	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	9
10	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	10
11	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	11
12	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	12
13	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	13
14	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	14
15	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	15
16	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	16
17	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	17
18	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	18
19	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	19
20	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	20
21	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	21
22	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	22
23	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	23
24	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	24
25	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	25
26	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	26
27	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	27
28	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	28
29	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	29
30	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	30
31	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	31
32	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	32
33	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	33
34	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	34
35	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	35
36	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	36

Calculated by Julien A. Hall, M. Am. Soc. C. E.



B.M.^s Listed

1.
Page
6-17

Checking Branches - Levels 18-67

Relocating Main-outlet to Sta 37+35

Levels 126-133

Alignment of Main

New outlet to Sta 37+35 150-153

Supplementary Survey Brs 3R 85

from new outlets, Pp. 76-86

Johnson Levels outlet #2 Dist #12

creek to R.R. 154-155

FILED
FEB 27 '23
J. W. Esther
COUNTY ENGINEER



Bench Marks. Dr. # 9.

Main.

New
Elev.

B.M. #1.	50.00	Top of W. end of S. end of concrete bridge
B.M. #2.	51.73	Spike in root of cottonwood tree near N.E. cor. - N.W. $\frac{1}{4}$ - SW $\frac{1}{4}$ Sec. 13.
B.M. #3.	57.60	Spikes in S. end of E. cap. of bridge between Secs. 14 & 23.
B.M. #4	✓	Top of boulder 84' S. of Sta. 72.
B.M. #5	65.30	Top of S. end of E. cap of bridge thru N $\frac{1}{2}$ of Sec. 23.
B.M. #6	66.45	Spikes in W. end of S. cap of bridge W. line Sec. 23.
B.M. #7	✓	Spikes in S. end of E. cap. bridge S. of Sec. 22. (Bridge destroyed)
B.M. #8	✓	Top of W. end cement culvert on N. & S. road W. line Sec. 27

B.M.A	51.26	Spike in E. end of N. cap of bridge on N. & S. Hwy.
B.M.B	57.90	Extreme W. willow in row at approx sta 37+00 (old survey.)
B.M.C	63.25	Black boulder at pasture fence (old survey) corner. Approx. Sta 70+00
B.M.D	71.09	Spike in corner post 200' E of Main on E & W. $\frac{1}{4}$ S. $\frac{1}{4}$ E.
B.M.E	70.37	Loth at N. & S. E. Approx 50' N. of Sta 1+00 Br 8 Left.
B.M.F	77.67	Spike at top of E. end of N. wing wall of Concrete bridge on Hawkeye Hwy.
B.M.G	79.57	Spike in Cor. post. SW cor NW $\frac{1}{4}$ NE $\frac{1}{4}$ Sec 27 Sta 163 Main. (Don't use)
B.M.H	92.39	NE Cor. of E. end of concrete culvert at end of Main

BM #1 Br. 7R. 76.52 ✓

BM #2 Br 7R 76.00

BM #3 Br 7R 80.55

BM #1 Br 6R 70.13 ✓

BM #2 Br 6R. 79.41 ✓

BM #3 Br 6R. 86.10 ✓

BM #1 Br 8R. 80.47

BM #2 Br 8R. 91.27

Large boulder approx. 200' N. of Sta 21
Br 7R and 200' W. of N. & S. Th.

Spike in root of S. of row willow
stumps approx 100' N. of Sta 34 Br 7R.

Spike in E. end of N cap of bridge
on Hwy. approx Sta 48+00 Br 7R.

Spike in N. end of E cap of bridge
N. of Sec 22 approx. Sta 19+50 Br 6R.

N.E. Cor. of E end of concrete Culvert
OR RR
S. side of Hwy. N. of Sec 22 Between Brs.

Spike in root of N. of row willows
running N.W. approx. Sta 7+ Br P.R.

Extreme N.E. Cor. E. end of concrete
culvert N. side of Hawkeye Hwy

S of Sec 22

N.E. Cor. of E. wing wall of concrete
culvert at N. side of Hawkeye Hwy.

N.W. Cor sec 27 & S.W. Cor. sec 22

BM ^{#1}	Br SR	63.13	✓
BM ^{#2}	Br SR	67.69	✓
BM ^{#3}	Br SR	73.69	✓
BM ^{#4}	Br SR	88.48	✓
BM ^{#5}	Br SR.	81.61	✓
BM ^{#6}	Br SR	81.46	✓
BM ^{#7}	Br 2R	73.83	✓
BM ^{#7}	Br SR	84.04	✓

Extreme N.E. Cor. of E. plank of Floor
W
of Bridge N. of Sec. 23 Sta 9 Br SR

Spike in root of lone willow
at property corner - Sta 37.50 Br SR

Spike in N. end of E. cap of
bridge N.E. cor SW $\frac{1}{4}$ NW $\frac{1}{4}$ Sec 14

N.E. Cor. of E. wall of concrete
Sta. 85. Br SR.
culvert between Secs. 10 & 11

N.E. Cor. N. wall conc. culvert
N. of Sec 15. Sta. 10 Br K. R.

N.E. Cor. N. wall conc. culvert
N. of Sec 15 - Sta 34 Br J. R.

Spike in root of S. of row
cottonwoods N. of Hwy
approx Sta 19 Br B. R.

Spike in E. of 2 cottonwoods
N. of Hwy - Sta 16 Br D. R.

B.M. [#] 1 Br 3R	73.09	Highest point on large rock in field approx 100' N.E. Sta 20 Br 3R
B.M. [#] 1 Br 2L	65.85	Spike in cor. post. S. end of Tr. 250' E. of Sta 29+26 Br 2 L
B.M. [#] 2 Br 2L	75.12	Top of white rock in field 200' W. of plank culvert on Hwy at Sta 45 Br 2L
	78.40	N.E. cor. of N. wall conc culvert on Hwy S. of Sec 13 - Sta 9+75 Br C. L.
B.M. [#] 3 Br 2L	89.11	N.E. cor. of N. wall conc. culvert on Hwy S. of Sec 13 - Sta 21+25 Br B. L.
B.M. [#] 1 Br 8L	76.94	N.E. cor of E wall conc culvert on Hwy E. of Sec 22 - 100' N. of Sta 10+50 Br 8L
B.M. [#] 2 Br 8L	85.26	Top of N. point of concrete base of steel corner post approx 50' W. of Sta 16 Br Q L.

B.M. #1 Br 34

88.90

B.M. #2 Br 34

77.67

B.M. #3 Br 34

87.79

Spike in root at N. side of large
cottonwood in S.W. cor. of grove

Approx. Sta. 19+25 Br. J L

N.E. cor. of small conc. culvert on

Hwy 5. of sec. 23 - Sta 54+50 Br 34

Spike in bottom of corner post

S.W. cor. sec. 29

18

Checking Br. 7R.

B.S. H.I. - S Elev.

B.M.D 1.29 72.38 71.09

Sta 17+43 Main 5.16 67.22

T.P. 5.70 73.60 4.48 67.90

5.01 5.17[?]

Sta 9 5.52 68.08

T.P. 6.02 76.45 3.17 70.43

5.77 76.44 2.93 70.67

Sta 18+77 6.11 77.90 4.66 71.79

T.P. 4.77 77.90 3.32 73.13

B.M.#1 Br. 7R. 1.38 76.52

T.P. 5.61 80.83 2.68 75.22

4.67 80.84 1.73 76.17

Sta 34+00 5.45 75.39

B.M.#2 Br. 7R 4.44 80.44 4.84 76.00

T.P. 4.86 80.44 5.26 75.58

Sta 34+00 5.05 75.39

Sta 35+00 4.70 75.74

70

48

118

May 25¹⁹ 20
Hoff
Whalen.

approx.
Large boulder approx. 200' N. of Sta 21+00
and 200' W. of N.B.S. #

Spike in root of S. of row of willow stumps
100' N. of Sta 34

B.S. Ht. In. - S Elev

Sta 40+00 6.15 82.82 3.77 76.67

5.14 82.82 2.76 77.68

B.M. #3 ^{B.T.R.} 5.18 85.73 2.27 80.55

Sta 41+78 4.39 78.43

B.T.R.
Sta 42+14 4.19 81.54B.M. #1 ^{B.T.R.} 1.64 78.16 76.52

Sta 22 5.96 72.20

Sta 23 5.73 72.43

Sta 21 6.33 71.83

Sta 19 6.74 71.42

Spike in E. end of N. Cap of Bridge

Sta 48+00

OK to Sta. 19. Sta 20 N.G. Sta 21 0.3' lower
 than orig. survey. Sta 22 0.59' lower &
 Sta 23 0.59' lower.

Adjust at Sta 21 - Reduce orig.
 elevations 1.60'.

Also Brs. S.R. - U.R. & T.R.

Checking Br. G.R.

B.S. H.I. - 5 Elev.

B.M. #5 4.79 70.09 65.30

T.P. 5.37 70.64 4.82 65.27

1.96 4.42 65.67

Sta. 10+75 6.30 64.34

T.P. 4.41 71.90 3.15 67.49

(71.89)

3.87 71.88 2.63 68.01

Sta 16 5.68 66.21

B.M. # Br. G.R. 4.13 74.26 1.76 70.13

T.P. 6.18 74.25 3.82 68.07

Spike in N. end of E. cap of bridge

N. of sec 22. Approx. Sta 19+50 Br. G.R.

Sta 19+62 6.07 68.18

old elev
68.15

Sta 2 Br. G.R. 5.06 69.19

Sta 1 Br. NR 1.35 72.90

Sta 27 Br. G.R. 2.04 72.21

Sta 28 Br. G.R. 0.85 73.40 73.53

Sta. 2 Br. NR

Sta 21+95 Br. OR. 3.47 70.78

T.P. 9.14 80.52 2.87 71.38

8.66 80.52 2.39 71.86

B.S.	H.I.	-S	Elev.
	80.52		
B.M. #2 B.G.R.		1.11	79.41
Sta 15 Br. Q.R.		2.35	78.17
T.P.	6.12	82.01	4.53 75.89
	5.33	82.00	3.85 76.67
Sta 12+39 Br. O.R.		5.84	76.16
Sta 9 17465		3.60	78.40
T.P.	5.62	84.15	3.47 78.53
	(84.14)		
	5.17	84.13	3.04 78.96
Sta 22		5.24	78.90
T.P.	7.12	88.04	3.22 80.92
	6.78	88.04	2.88 81.26
Sta. 27.		6.75	81.29
Sta 29		5.43	82.61
Sta 1 Br. M.R.		5.15	82.19
Sta 3 Br. P.R.		4.65	83.39 82.33
B.M. #3 B.G.R.		1.99	86.10
Sta 7 Br. P.R.		3.10	84.99 83.85

N.E. Cor. of E. wing Wall Concrete Culvert

S. side of Hwy N. of Sec. 22

Spike in root of N. of row willows

Running N.W. approx. Sta 7 Br. P.R.

Checking Brs. O.-P.B.W.R.

R.S. H.I. - S. Elev.
88.09

Sta 33 Br. O.R. 4.06 83.98 82.87 1.11

Sta 32 Br. O.R. 4.55 83.49 82.26 1.23

Last T.P. 4.51 85.43 80.92

4.16 85.43 81.26 old
Elevs

Sta 26 Br. O.R. 4.94 80.49 79.39 1.10

Sta 25 5.32 80.11 78.94 1.17 check to Sta 23. R. & Brs. Q.R. & N.R.

Sta 24 5.39 80.04 78.88 1.16 Adjust from Sta 23 Br. O.R.

Sta 23 6.08 79.35 79.35 and Brs. P.B.W.R. - Raise

Sta 22 6.57 78.86 79.00 original elevations 1.10'

Relevating B.M.F.

B.M.F. 5.48 75.85 70.37

T.P. 6.16 78.50 3.51 72.34

5.99 78.51 3.33 72.52

B.M.F. 5.60 83.26 0.85 77.66

T.P. 7.76 83.28 2.99 75.52

B.S. H. I. - S Elev.

Sta 7+19 Br. 9R. 83.27 5.57 77.70

Sta. 7 6.00 77.27

Sta. 612 6.16 77.11

#B. 8R.
B.M. 1 4.91 85.38 2.80 80.47

T.P. 4.15 85.37 2.05 81.22

Sta 0+41 Br. V.R. 4.66 81.72

T.P. 5.90 87.66 3.62 81.76

5.65 87.66 3.37 82.01

Sta 20+79 Br. 8R. 4.92 82.74

Sta 21+75 " " " 5.13 82.58 old elev

Sta 19+33 Br. 9R. 6.25 81.40 81.18

Sta. 20 6.02 81.64 81.43

Sta. 23 4.50 83.16 83.17

21 5.53 82.13 82.01

20 6.02 81.64 81.43

19+39 6.25 81.41

19 6.52 81.14 81.07

18 6.75 80.91 80.95

Extreme N.E. cor. of E. end of Concrete
culvert N. side of Hawkeye Hwy. Not
Sec. 27

B.S. H.I. -S Elev.

87.66

I.P. 9.74 92.33 5.07 82.59

9.35 92.34 4.67 82.99

B.M. ^{B-8R} 2.71 93.98 1.07 91.27

Sta 34+35 B-9R. 5.10 88.88

35+82 " " " 4.80 89.18

I.P. 4.66 94.46 4.18 89.80

4.23 94.47 3.74 90.24

Sta 38+79 B-8R. 3.71 90.75

Sta 36+82 " " " 5.19 89.32

B.M. #17 1.98 93.25 91.27

Sta 33 B-9R. 5.81 87.44 86.02

" 32 6.16 87.09 85.73

" 31 6.54 86.71 85.37

" 29 7.30 85.95 85.32

8.85 84.40

85.27
2.15

88.12

N.E. Cor. of E. wing wall concrete Culvert
at N. side Hawk Eye Hwy. N.W. Cor. Sec. 27

93.25

T. P 2.28 89.60 5.93 87.32

2.31 89.60 5.96 87.29

Sta 26 Br 9 R 5.67 83.93 82.90

Sta 25 5.85 83.75 82.98

Sta 24 5.95 83.62 83.38

" 23 6.38 83.22

Checks to sta 25.

Adjust from Sta 25 - Raise
original elevations 1.30'

	B.S.	H.I.	-S	Elev
B.M. G 167	64.92			63.25
Sta 4		4.57		60.38
Sta 5	7.02	66.32	5.62	59.30
T.P.	6.17	66.23	4.76	60.16
B.R.S.R				
B.M. #1	4.67	67.80	3.19	63.13
T.P.	6.26	67.81	4.77	61.55
T.P.	7.76	70.02	5.85	62.26
	7.13	70.02	4.92	62.89
Sta 15		8.35	61.67	60.84 .83
18		7.51	62.51	61.67 .84
B.M. #18	4.45	67.56		63.13
Sta 8+30		7.05	60.53	59.76 77
Sta 8+00		7.20	60.38	59.63 75
Sta 7.		7.55	60.03	59.91 76
B.M. #8	3.80	66.93		63.13
Sta 6		6.44	59.99	60.19 10
Sta 5		7.62	59.31	59.44

Extreme N.E. Cor. of E. plank of floor on
bridge 1880' E. of N.W. Cor. Sec. 23.

76 checks at Sta 6. Adj. just from Sta 6 -

Raise original elevations 0.80'

B.S. H.I. -S. Elev.

Last T.P. 6.20 68.46 62.26

5.55 ~~68.44~~ 62.89

Sta 21 5.54 62.92

T.P. 5.77 69.50 4.73 63.73

5.39 69.50 4.35 64.11

27+50 4.64 64.86

28 4.42 65.08

T.P. 6.42 71.49 4.93 65.07

5.96 71.51 3.95 65.55

Sta 31 5.49 66.01

T.P. 5.43 72.76 4.17 67.33

4.99 72.76 3.73 67.77

B.M. #2 Br. S.R. 5.07 67.69

Sta 36 5.05 67.71

Sta 37+95 4.52 68.24

Sta 40 6.41 75.28 3.89 68.87

T.P. 5.55 75.27 3.09 69.72

#2
Spike in root of lone willow

H.I.
75.28

Sta 45			4.01	71.27
Sta 47				
T.P.	7.46	78.28	4.49	70.79
		.24		
	6.39	78.23	3.44	71.84
BM #3 B&R			4.55	73.69
Sta 50 + 83			5.79	72.95
T.P.	9.11	82.42	4.93	73.31
	8.86	82.43	4.67	73.57
Sta 1 + 9 B&R			5.66	76.76
T.P.	5.16	82.87	4.71	77.71
	5.25	82.88	4.79	77.63
Sta 6 + 49			6.11	76.77
T.P.	5.88	85.96	2.80	80.08
		85.97		
	5.32	85.98	2.22	80.66
T.P.	6.80	88.03	4.74	81.23
		88.02		
	6.16	88.01	4.12	81.85
Sta 77			7.21	80.81
" 80			5.34	82.68

Spike in N. end of E. cap of bridge

NE. Cor. SW $\frac{1}{4}$ NW $\frac{1}{4}$ Sec. 14.

	B.S.	H.I.	-S	Elev.
		88.02		
T.P.	5.54	89.56	4.00	44.02
	5.14	89.56	3.60	84.42
Sta 83+89			5.82	88.74
Sta 84			5.81	83.75
B.M.#4 Br SR			1.08	88.48
Sta 1 Br SR			5.75	83.81
Sta 2 " " "			5.05	84.51
Sta 2 Br H.R.			4.28	85.08
Establishing B.M.#5 Br SR.				

	Br SR			
B.M.#3	5.83	79.52		73.69
T.P.	10.16	87.44	2.24	77.28
	9.79	87.44	1.87	77.65
T.P.	2.11	86.29	3.26	84.18
	1.69	86.29	2.84	84.60
B.M.#5 Br SR				
B.M.#52	3.73	85.34	4.68	81.61
T.P.	5.09	85.33	6.05	80.24

N.E. Cor. of E. wall Conc. Culvert

Bet. Secs. 10 & 11 - Sta 85 Br SR

Adjust Brs. G.R. & H.R. -

Raise original elevations 0.80'

N.E. Cor. of N. wall of concrete

culvert. N. of sec. 15, Sta 10 Br SR.

BS	H.I.	-S	Elev
	85.38		

Sta 9+17 Br. K.R.	7.02	78.31
-------------------	------	-------

Sta 33+59 Br. J.R.	6.42	78.91
--------------------	------	-------

B.M. #23	3.87	81.96
----------	------	-------

B.M. #20	6.54	80.22	73.69
----------	------	-------	-------

T.P.	10.02	88.03	78.01
		90.03	2.22

	9.82	88.02	78.20
		90.02	2.03

T.P.	4.81	89	84
		91.50	3.34

	4.57	89.50	84
		91.50	3.10

Sta 15 Br. J.R.	6.76	82.74	84.74
-----------------	------	-------	-------

		81.30
--	--	-------

Sta 12+85	8.20	83.61
-----------	------	-------

	5.89	85.61
--	------	-------

98	Sta 15	87.74
82.74	" 12+85	81.30
1.44		

Adjust Brs J.R. - K.R. - L.R. & M.R. -

Raise original elevations 0.80'

N.E. Cor. of N. Wall of Concrete

culvert N. of Sec 15 Sta 34 Br. J.R.

S. end of corrugated culvert

approx. Sta 15 Br. J.R.

5 backing B.R. 2R- R.R. D.R. - 1R&R

B.S. H.I. - S Elev.

B.M.#1 8.33 58.33 50.00

Sta 14+42 Br AR 4.69 53.64

T.P. 9.36 65.29 2.40 55.98

65.27

8.95 65.26 2.02 56.31

T.P. 12.73 76.55 1.45 63.82

12.33 76.54 1.06 64.21

T.P. 9.84 84.72 1.67 74.88

9.44 84.72 1.27 75.28

T.P. 1.35 79.27 6.80 77.92

0.89 79.28 6.33 78.39

Sta 18+39 Br BR 7.00 72.27

B.M.#2^{2R} 8.91 82.74 5.44 73.83

82.73

T.P. 9.45 82.72 6.00 72.27

T.P. 8.41 89.26 1.86 80.85

8.05 89.27 1.51 81.22

T.P. 5.69 87.13 7.83 81.44

5.40 87.13 7.54 81.73

9

Br A.R. OK.

Br B.R. OK.

Spike is root of S. of Row cottonwood
N. of Hwy. approx. Sta. 19+00 Br B.R.

	B.S.	H.I. 87.13	-5	Elev
Sta 21+59 Br. 2R.			7.69	79.44
T.P.	5.20	90.96	1.37	85.76
	4.83	90.97	0.99	86.14
B.M.#	4.60	88.38	7.19	83.78
Sta 15 Br. DR.			8.05	82.92
		88.40		
T.P.	4.27	88.41	6.83	84.14
B.M.# Br. 5R			4.36	84.04
T.P.	3.60	83.56	8.44	79.96
		83.55	9	
	3.27	83.54	8.13	80.27
T.P.	1.89	79.01	6.43	77.12
	1.59	79.01	6.13	77.42
Sta 23+19 Br. 3R			6.86	72.15
Sta 23			7.46	71.55
T.P.	3.66	76.75	5.92	73.09
	3.54	76.75	5.80	73.21
B.M.#			3.66	73.09

Br. 2R. OK.

Same corrugated Culvert.

Spike in E of 2 Cottonwoods. Sta 16

Br. D.R.

Sta 15 Br. DR = $82.92 - 1.44 = 80.48$. Elev. Sta. 12 + 95'Adjust Br. DR - Raise original elevations ^{0.80'}Highest point on large rock in field
approx. 100' N.E. of Sta 20+00 Br. 3R.

B.S. $\frac{H.I.}{76.75}$ - S Elev.

T.P. 2.19 71.44 8.50 68.25

2.78 71.44 8.09 68.66

T.P. 4.04 67.15 8.33 63.11

3.83 ~~67.16~~ 8.11 63.33

T.P. 1.58 58.21 10.52 56.63
58.22

1.21 58.23 10.13 57.02

T.P. 5.31 57.55 5.98 52.24
57.56

4.91 57.57 5.56 52.66

T.P. 4.03 58.77 2.82 54.74

3.58 58.77 2.37 55.19

B.M.B. 0.88 57.89

B.S. H.L. -5 Elev.

B.M. #2 3.63 55.36 51.73

T.P. 6.18 59.16 2.38 57.98

59.17

T.P. 5.71 59.18 1.89 53.47

T.P. 9.43 63.15 5.45 53.72

" 9.15 63.15 5.17 57.00

OK

T.P. 9.59 71.61 1.13 62.02

OK

9.95 71.62 1.48 61.67

T.P. 6.53 74.82 3.33 68.29

6.29 74.81 3.02 68.60

4.04 72.29 6.56 68.25

3.53 72.28 6.06 68.75

Sta 1 Br 2 L. 8.64 63.65

Sta 26 Br 2 L. 9.95 62.74

Sta 29126 ... 71.68 64.61

B.M. #18 Br 2 L. 6/7 72.02 6.44 65.85

T.P. 6.70 72.02 6.97 65.32

6.70

Spike in Cor. Post. S. end of Rd.

250' E. of Sta 29126 Br 2 L.

	B.S.	H.I. 72.02	-S.	Elev
T.P.	7.16	75.76	3.42	68.60
	6.93	75.76	3.19	68.83
T.P.	7.10	80.39 80.37	2.47	73.29
	6.64	80.36	2.04	73.72
Sta 44+13	Br 24		4.85	75.52
Sta 45+11			4.33	76.04
BM #2	Br 24		5.25	75.12
T.P.	10.16	87.91 87.92	2.62	77.75
	9.70	87.93	2.14	78.23
T.P.	2.55	87.94	2.53	85.39
	2.22	87.94	2.70	85.72
T.P.	2.91	82.67	8.18	79.76
	2.67	82.66	7.95	79.99
Br 24				
Br 24	5.45	83.85	4.26	78.40
Sta 9+69	Br. C.R.		6.83	75.83
T.P.	4.85	83.85	3.66	79.00

Top of white rock in field 200' W. of
plank culvert on Hwy Sta 45 Br 24.

N.E. cor. Conc. Culvert N. & S. Hwy

Sta. 9+75 Br. C.R. 4

B.S. H.I. - S. Elev.

T.P. 9.43 90.91 2.27 81.48

9.13 90.91 2.07 81.78

T.P. 2.96 88.47 5.40 85.51

2.64 88.48 5.07 85.84

B.M. #1 Br. Bluff 4.37 84.11

Sta 21+2 Br. B.L. 6.88 81.60

N.E. Cor. N. end of Conc. Culvert on

E. & W. Hwy. Sta 21+25 Br. B.L.

SL Checking Br 8¹ Left.
BS H.I -5 Elev.
B.M. E 8.85 79.22 70.37

T.P. 7.67 81.82 5.07 74.15
7.15 81.82 4.55 74.67

Sta 10+26 6.05 75.77

B.M. #1 Br 8 L 4.88 76.94

Sta 15 5.96 84.17 3.63 78.19

T.P. 5.77 84.16 3.43 78.39

Sta. 19+46 3.30 80.56

T.P. 7.57 89.39 2.34 81.82

7.27 89.40 2.03 82.13

6.92 91.91 4.41 84.99

6.60 91.90 4.10 85.30

Sta 15+44 Br Q L. 7.07 84.83

Sta 16 " " " 6.77 85.13

B.M. #2 Br 8 L 6.64 85.26

T.P. 7.57 95.63 3.84 88.06

7.24 95.63 3.51 88.39

N.E. Cor. of E. wall of concrete Culvert

approx 100' N. of Sta 10+50 Br 8 L

Top of N. point of Concrete base of steel

corner post approx 50' W. of Sta 16 Br Q L.

	B.S.	H.I.	- S.	Elev.
		95.63		
T.P.	3.36	92.99	6.00	89.68
		93.00		
	3.16	93.02	5.78	89.55
Sta 13+50 Br J 4			5.68	87.32
B.M. #1 Br 34			4.10	88.90
T.P.	3.05	90.12	5.93	87.07
	2.83	90.12	5.71	87.29
T.P.	3.03	85.27	7.88	82.24
	2.68	85.27	7.53	82.59
T.P.	4.02	82.32	6.97	78.30
	3.71	82.32	6.66	78.61
B.M. #2 Br 34			4.65	77.67
L. Hwy Sta 54+56 Br 34			4.86	77.46
	11.50	91.12	2.70	79.62
		91.11		
	10.95	91.10	2.17	80.15
B.M. #			3.32	87.79
Sta 22+33 Br 64			5.78	95.33

Spike in root at NE side of large cottonwood
Br. J. 4,
10 S.W. corner of grove. - Approx Sta 14+25

N.E. Cor. of N. wall of concrete Culvert.
Sta 54+50 Br 3 left.

Spike at bottom of Corner post S.W. Cor.
Sec. 24

B.S. H.I. - S Elev
91.11

2.31 87.80 5.92 85.19

1.76 87.49 5.38 85.73

Sta 10+82 Br. G.L. 11.20 76.29
76 55
26

B.M.⁺ 6.06 94.96 88.90

T.P. 2.20 95.87 1.34 93.62

1.82 95.87 0.96 94.00

T.P. 2.56 93.14 5.24 90.58

93.13
2.15 93.12 4.85 90.97

Sta 29+57 Br. G.L. 7.25 85.88

Br. G. left checks at Sta 10+82.

old elevations approx 1.00 low at Sta 22+33

Same spike in cottonwood

Br. G. left OK

B.S. H.I. -5 Elev.

B.P.⁴ 8.98 94.24 85.26

6.03 95.92 4.35 89.89

5.72 95.92 4.04 90.20

Sta 32+66 B.L. 6.78 89.14

T.P. 11.51 106.01 1.92 94.50

11.14 106.00 1.06 94.86

T.P. 4.03 106.92 3.11 102.89

3.57 106.92 2.65 103.35

T.P. 5.11 107.11 7.12 99.80

6.67 100.25

Sta. B.L.

8.23 108.03

108.04

7.80 108.05

old elev

Sta 13+23 B.L. 3.21 104.83 102.53

T.P. 2.48 105.56

2.25 105.79

100.25	99.80
7.80	8.23
108.05	108.103

99.25
7.60
107.05

823	7.12	63
780		
43	6.67	
	45	

Same corner post footing.

Not Sta. 13+23 as shown on plat.

loc corner at end of Br. O.L.

B.S. H.I. -S Elev.
108.04

T.P. 3.79 101.66 10.17 97.87

3.27 101.67 9.64 98.40

Sta 36+91 Br 9.4 3.97 97.70

Br 9.4. checks.

Same

T.P. Br 9.4 4.06 109.62 105.56

3.82 105.79

T.P. 3.61 105.49 7.74 101.88

3.44 105.48 7.58 102.04

Sta 11 Br 0.4 5.22 100.26

3.33 102.15

7.02 98.46

At #. should be end of Br 9.4.

Br 0.4 OK

Br 9.4

Sta 36+91 7.32 105.02 97.70

Br 9.4 OK.

T.P. 3.66 107.09 1.59 103.43

107.12

3.36 107.15 1.23 103.79

4.73 101.42 10.43 96.69

4.93 101.43 10.12 97.00

B.S. H.I. -S. Elev
101.93

T.P. 3.02 94.69 9.76 91.67

2.59 94.70 9.32 92.11

6.88 87.82 old
Elev

8.06 86.74 87.29

Ground level at end of Br. 11.4

In ditch at end of Br. 11.4

Box 11.4 OK.

Sta	B.S.	H.I.	-S	Elev.
B.M.#3	4.72	62.32	12.32	57.60
O=Sta 54 Main				
L 7 = "56 "			7.25	55.07
3.			7.60	54.72
4			7.70	54.62
5.			6.60	55.72
6			5.25	57.07
7.			4.40	57.92
8.			3.50	58.82
9.			4.00	58.32
T.P.	4.94	63.49	3.77	58.55
" " "	4.68	^{63.48} 63.47	3.53	58.79
10 Pond			6.30	57.18
L 10			5.50	57.98
12			5.30	58.18
13			5.50	57.98
14			5.65	57.83

Approximate location of Angle points.

L. Sta 1 = Sta 56 original Main.

L. " 6 = 130' N & 95' W. of SE. Meadow

Fence Corner.

Fence corner = 420' S. of S. Hay F. &
300' W. of Center of Bridge

Sta 55 Main

L. Sta 18 = 80' N. & 1040' W. of same F. Cor.

L. Sta 14 + 50 = 855' N & 220' S of " F. Cor.

Note Use Sta Number & Elev
on this page including Sta. 7

63.48

15

~~5.10 58.38~~

16+50

~~5.60 57.88~~

17

~~5.75 57.73~~

18

~~5.00 58.48~~

18

~~4.70 59.78~~

16+50

4.35 59.13

15+50

3.84 59.64

14+50

3.65 59.83

13+50

3.70 59.78

12+50

4.10 59.08

11+50

5.20 58.28

10+50

4.80 58.68

9+50

4.90 58.58

8+50

5.00 58.48

=54.6

5.45 58.03

T.P.

9.61

68.78

4.31

59.17

9.92

68.78

4.13

59.35

26.25
18
8.256.00
9.50
5.25
20.75

Note. Use cuts on this page
including ^{54.5} 8+50 & 16+50

28.78

17+50 9.25 59.53

18+50 9.00 59.78

19+50 8.95 59.83

20+50 8.75 60.03

21+50 8.70 60.58

S Hwy F. N. Hwy F.

22+36 23+22 —

22+50 —

E Hwy

22+79 7.58 61.23

23+50 7.40 60.38

24+50 8.35 60.43

24+75 = 9+80 orig. line 8.35 60.43

B.M. 1 4.28.

5.57 63.21 63.13

Use these stg numbers & Elevs

Sta	B.S.	H.I.	-S	Elev
-----	------	------	----	------

B.M. #3	4.90	62.50		57.60
---------	------	-------	--	-------

O = Sta 54+81 orig main.

1		7.00	55.50	
---	--	------	-------	--

2		6.40	56.10	
---	--	------	-------	--

3		5.30	57.20	
---	--	------	-------	--

4		4.85	57.65	
---	--	------	-------	--

5		4.10	58.40	
---	--	------	-------	--

6		4.20	.30	
---	--	------	-----	--

7		4.55		
---	--	------	--	--

8		5.30		
---	--	------	--	--

ditch				
-------	--	--	--	--

8+50		7.30		
------	--	------	--	--

9		4.45		
---	--	------	--	--

9+12		4.40		
------	--	------	--	--

Relocating Bar 34

Sta BS. H.I. -S Elev

BM 3 4.90 62.50 87.60

D = Sta 58 orig Main 8.15

1 8.00

2 8.70

3 6.10

4 6.45

5 5.50

6 5.00

7 4.50

7+75 4.40

Outlet = Sta 58 original main.

Relocating Br 5R

Sta	BS	HI.	-S	ELEV
BM#3	4.90	62.50		57.60

0

1

7.20

2

6.00

T

3

4.83

3 + SD = 516 - 154

4.97

Dist #9

Change to Open ditch

0 to sta. 37+35

BM #1 1.65 51.65 50.00

H²O 11.2 40.4

1 7.8 41.85

2 7.2 42.35

3 7.0 42.65

L 3+45

4 7.5 44.15

5 7.2 44.45

BM 2.43 52.43 50.00

L bridge 2.9 49.53

6 12.0 40.43

7 7.9 42.53

8 7.5 44.93

9 7.4 45.03

sta 0 = L Bridge N+5 Hwy.

100' W. outlet bridge on N+5 Hwy.

N. Fence line 5+86

S. F.L. 6+45

B-I-R 7+48

L 9+22

52.43

L. SW.

10 7.5 44.93

11 7.5 44.93

12 6.2 46.13

13 5.6 46.83

14 5.3 47.13

T.P. 5.01 52.35 5.09 47.34

4.17 52.33 4.27 48.16

15 52.34 6.1 46.24

16 5.0 47.34

17 5.8 46.54

18 5.2 47.14

18+10 BR. SE.

19 4.7 47.64

18+10 Flood water inlet

20 3.2 49.14

L 20+15

L. West.

21 3.6 48.74

22 2.9 49.44

23 2.3 50.04

23+00 E. E N+S. Hwy

23+07 52.34 3.1 49.24

E. ditch

23+27 1.60 50.74

E. HWY

23+49 5.3 47.04

W. ditch

24 2.8 49.54

23+56 W. P.L.

T.P. 4.96 55.70 1.60 50.74

4.48 55.70 1.12 51.22

BM #2 2.95 51.75

51.73

24+85 E. W. P.L.

25 7.5 48.20

26 7.4 48.30

27 7.0 48.70

28 7.3 48.40

29 6.6 49.10

30 7.0 48.70

31 6.3 49.40

32 5.7 49.80

33 5.7 50.00

34 5.6 50.10

34+31 L.

34+31 L. SW.

35 55.70 6.1 49.60

36 5.9 49.80

37 6.5 49.20

37+35 6.4 49.30

35+00 = BR. 2-R.

= 30 OF Original Main

#9

Outlet Change

Figure to use Ball Hwy.
bridges.

#1 Bridge on N + S
Hwy at new outlet is
427' N. of SE. COR NE of NW
Sec. 13.

#2 Bridge on E + W Hwy
is 317' W. of above Cor.

At Bridge #2

Bridge - P.I. #2	353' - 40'	315'	P.I. #2
" - P.I. #1	173' - 40'	280'	P.I. #1

At P.I. #1

Def'd Δ Bridge #1 - Bridge #2
61° - 30'

Briggs

Hoff

Whalen

Bridge Notes.

Bridge #1

26' x 5½' to H²O

26' x 7½' to bottom ditch

Footings approx 6' below W.L.

Bridge #2

17½' x 7' Waterway (1' water)

Footings 3' below W.L.

Alignment Main Cont.

Azim From Bridge #2 To

P.I. #2 $353^{\circ}-40'$ π At P.I. #2 = Sta. 9+22B.S. $353^{\circ}-40'$

#1

 $32^{\circ}-18'$

To P.I. #3

Def'l Δ $37^{\circ}-38'$ R
Def'l L used May 19-21 $37^{\circ}-40'$ R

Sta

 π At P.I. #3 = Sta. 20+15B.S. $32^{\circ}-18'$

#2.

 $58^{\circ}-40'$

To P.I. #4

New Def May 19 1921 Sta 16+30

Def'l L $26^{\circ}-20'$ R $\Delta = 34^{\circ}-34'$ R. π At P.I. #4B.S. $58^{\circ}-40'$

#3

 $31^{\circ}-52'$

To Sta 37+3

Def'l L $55^{\circ}-9'$ L

6/11/20

Johnson Levels
Outlet #2

CREEK to R.R.

W.L. 10.77 60.77

(50.00) (46.00)

G.L. 4.4

56.4 (52.4)

T.P. 4.29 61.28 3.78

51.99 (52.99)

G.L. 4.8

56.5 (52.5)

Bottom 6.2

55.1 (51.1)

Cattle Pass

O. J. Side R.R.

6.7 54.6 (50.6)

O. 10. Rept. to board
6/14/20Carl
Bedford
Hudson

4.6

.3
1.6

CREEK

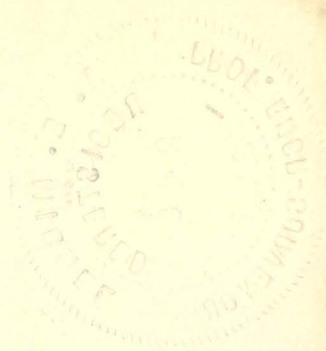
CREEK

G.L.

N. Side R.R.

160.

37+35 = 30 old
nom.



DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

ROADWAY 14 FEET WIDE. SIDE SLOPES $1\frac{1}{2}$ TO 1.

FOR SINGLE TRACK EMBANKMENT.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	7.0	7.2	7.3	7.5	7.6	7.8	7.9	8.1	8.2	8.4	0
1	8.5	8.7	8.8	9.0	9.1	9.3	9.4	9.6	9.7	9.9	1
2	10.0	10.2	10.3	10.5	10.6	10.8	10.9	11.1	11.2	11.4	2
3	11.5	11.7	11.8	12.0	12.1	12.3	12.4	12.6	12.7	12.9	3
4	13.0	13.2	13.3	13.5	13.6	13.8	13.9	14.1	14.2	14.4	4
5	14.5	14.7	14.8	15.0	15.1	15.3	15.4	15.6	15.7	15.9	5
6	16.0	16.2	16.3	16.5	16.6	16.8	16.9	17.1	17.2	17.4	6
7	17.5	17.7	17.8	18.0	18.1	18.3	18.4	18.6	18.7	18.9	7
8	19.0	19.2	19.3	19.5	19.6	19.8	19.9	20.1	20.2	20.4	8
9	20.5	20.7	20.8	21.0	21.1	21.3	21.4	21.6	21.7	21.9	9
10	22.0	22.2	22.3	22.5	22.6	22.8	22.9	23.1	23.2	23.4	10
11	23.5	23.7	23.8	24.0	24.1	24.3	24.4	24.6	24.7	24.9	11
12	25.0	25.2	25.3	25.5	25.6	25.8	25.9	26.1	26.2	26.4	12
13	26.5	26.7	26.8	27.0	27.1	27.3	27.4	27.6	27.7	27.9	13
14	28.0	28.2	28.3	28.5	28.6	28.8	28.9	29.1	29.2	29.4	14
15	29.5	29.7	29.8	30.0	30.1	30.3	30.4	30.6	30.7	30.9	15
16	31.0	31.2	31.3	31.5	31.6	31.8	31.9	32.1	32.2	32.4	16
17	32.5	32.7	32.8	33.0	33.1	33.3	33.4	33.6	33.7	33.9	17
18	34.0	34.2	34.3	34.5	34.6	34.8	34.9	35.1	35.2	35.4	18
19	35.5	35.7	35.8	36.0	36.1	36.3	36.4	36.6	36.7	36.9	19
20	37.0	37.2	37.3	37.5	37.6	37.8	37.9	38.1	38.2	38.4	20
21	38.5	38.7	38.8	39.0	39.1	39.3	39.4	39.6	39.7	39.9	21
22	40.0	40.2	40.3	40.5	40.6	40.8	40.9	41.1	41.2	41.4	22
23	41.5	41.7	41.8	42.0	42.1	42.3	42.4	42.6	42.7	42.9	23
24	43.0	43.2	43.3	43.5	43.6	43.8	43.9	44.1	44.2	44.4	24
25	44.5	44.7	44.8	45.0	45.1	45.3	45.4	45.6	45.7	45.9	25
26	46.0	46.2	46.3	46.5	46.6	46.8	46.9	47.1	47.2	47.4	26
27	47.5	47.7	47.8	48.0	48.1	48.3	48.4	48.6	48.7	48.9	27
28	49.0	49.2	49.3	49.5	49.6	49.8	49.9	50.1	50.2	50.4	28
29	50.5	50.7	50.8	51.0	51.1	51.3	51.4	51.6	51.7	51.9	29
30	52.0	52.2	52.3	52.5	52.6	52.8	52.9	53.1	53.2	53.4	30
31	53.5	53.7	53.8	54.0	54.1	54.3	54.4	54.6	54.7	54.9	31
32	55.0	55.2	55.3	55.5	55.6	55.8	55.9	56.1	56.2	56.4	32
33	56.5	56.7	56.8	57.0	57.1	57.3	57.4	57.6	57.7	57.9	33
34	58.0	58.2	58.3	58.5	58.6	58.8	58.9	59.1	59.2	59.4	34
35	59.5	59.7	59.8	60.0	60.1	60.3	60.4	60.6	60.7	60.9	35
36	61.0	61.2	61.3	61.5	61.6	61.8	61.9	62.1	62.2	62.4	36

Calculated by Julien A. Hall, M. Am. Soc. C. E.