

U. S. No. 508

UNITED STATES DEPARTMENT OF AGRICULTURE

Field Book

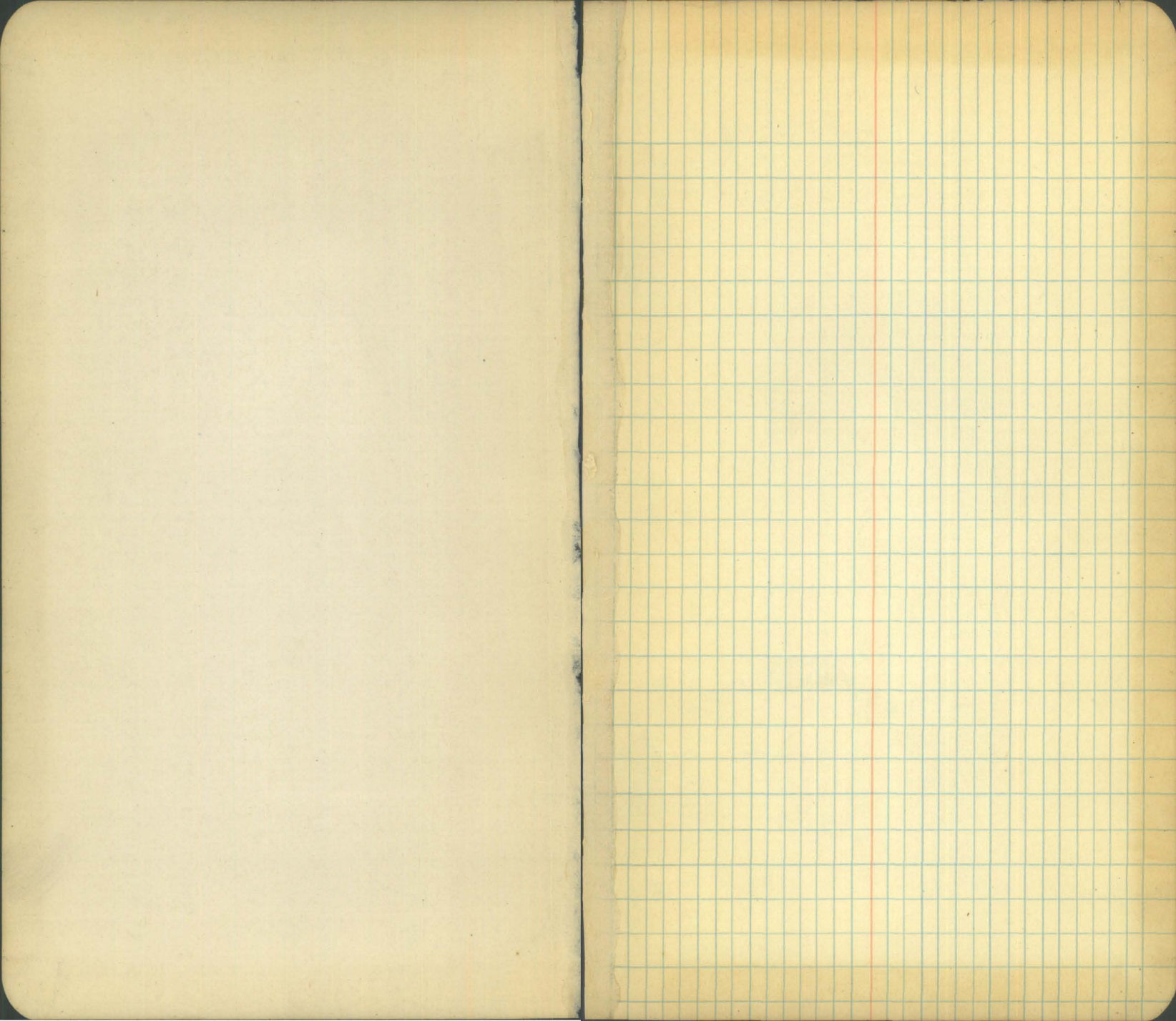
FOR THE RECORD OF FIELD WORK

80

Property of
Black Hawk County
Care of
County Engr.



406



1928

Index to Contents.

Pages

Cedar Falls-Dunkerton Co. Rd.

Final X-Sections

1-18 ✓

Permanent Reference Ties

20 ✓

1930

Levels on each side of Road

by CULV. on Anthony's Land

N. 85. side Road

Between Sec 16 Cedar & 21 Big Creek 21

Spring Creek Twp. Between Sec's 17-18

87-11

Levels for Tile on W. side of Road

Levels on outlet Tile East

22-24 ✓

Permanent Reference Ties

26-27 ✓

Tile levels on Hudson-Hicks Co. Rd

28-29

Tile levels in Spring Creek Twp

30-31 ✓

Hudson-Hicks Co. Rd check on 6" Tile

32 ✓

Tile Profile between Sec's 6 & 7-9 & 11

Lester Twp.

34-35 ✓

1931

Cor. Stone Ties. Big Creek Twp.

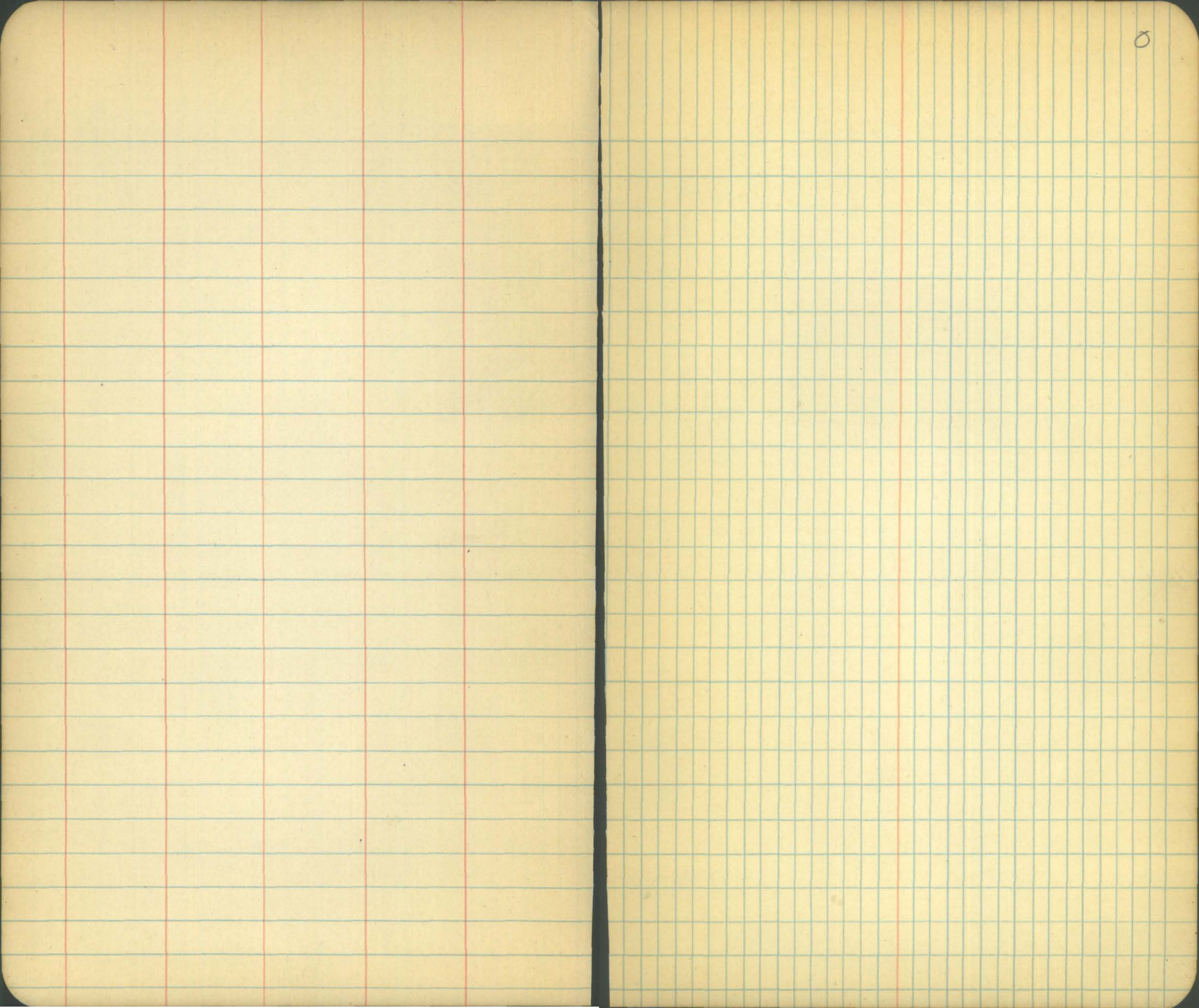
Between Sec's. 33 & 34-87-12

38 ✓

" " 34 & 35-87-12

37 ✓

Stadia & level notes Electric Park Intersection 42-50



9/10/28 AM. D.S.B. Clear - Warm.
F.R.K.
P.G.H.

Sta. B.S. H.I. F.S. Elev.
B.M. 9.16 944.52 ✓ 935.36
① 10.31 953.83 ✓ 100 943.52 ✓

109+00

110+00

111+00

112+00

① 5.60 959.69 ✓ 1.74 952.09 ✓

112+50

113+00

114+00

115+00

115+42

115+47 = Conc. Culv. = pitch ends. H.I. = Lt.

115+52

B.M. 8.61 960.88 ✓ 5.43 952.26 ✓ 952.27

Cedar Falls - Dunkerton Co. Rd.
Final X-Sections.

Na. in Teh Pole S.W. Cor. Intersections Sta 116+62

H9.5 H1.8 H1.2 H1.6 H3.6 H3.8 H4.0 H4.9 H3.8 H3.6 H3.6
10.3 12.0 11.6 11.2 10.0 10.0 9.8 11.1 11.8 11.2 7.2
31 29 23 16 17 0 13 16 20 23 30 ✓

H4.9 H3.6 H3.7 H3.9 H1.2 H1.6 H1.2 H1.2 H3.8 H3.6 H3.9
6.9 8.4 8.1 7.9 6.4 6.2 6.1 7.4 8.0 8.2 3.9
31 29 23 17 13 0 19 17 21 25 31 ✓

H4.9 H3.1 H3.5 H3.7 50.1 50.5 50.4 H4.9 H3.6 H3.8 51.6
4.5 5.7 5.3 5.1 3.7 3.3 3.4 5.1 5.3 5.5 1.8
31 29 23 17 13 0 13 17 22 26 31 ✓

51.9 H4.7 H4.8 50.4 50.1 50.5 51.6 50.2 H4.8 H4.6 53.8
2.1 2.1 2.0 2.9 2.4 2.0 2.2 3.6 4.0 4.2 0.0
31 29 23 16 13 0 13 17 22 27 31 ✓

50.1 H4.8 50.1 50.5 50.2 50.2 50.1 50.6 50.0 H4.9 51.2
5.6 7.9 7.6 7.1 5.7 5.5 5.6 7.2 7.7 7.8 3.5
31 27 24 16 13 0 13 17 22 26 31 ✓

51.5 H4.9 50.1 50.5 50.2 50.2 50.1 50.6 50.1 H4.8 53.0
5.9 7.8 7.6 7.2 5.5 5.3 5.6 7.2 7.6 7.9 4.2
31 28 24 17 13 0 13 16 24 26 31 ✓

H4.7 H3.8 H4.9 H4.6 52.2 52.4 52.1 H4.8 H4.4 H4.4 51.9
8.0 8.9 8.8 8.2 5.5 5.3 5.3 7.9 8.3 8.5 6.0
31 30 23 17 13 0 14 18 24 28 31 ✓

H3.1 H4.6 H4.4 H4.0 52.6 52.9 52.1 H4.6 H4.2 H3.8 H4.9
2.0 10.1 8.8 8.7 5.2 5.0 5.0 8.1 8.7 8.9 2.8
31 30 26 19 17 0 13 17 25 30 31 ✓

H3.1 H4.8 H4.0 H4.7 52.6 52.8 52.1 H4.9 H4.2 H4.1 H4.5
2.0 9.9 9.7 9.0 5.1 4.9 4.8 5.4 8.4 8.5 8.2
31 30 27 16 12 0 14 18 26 30 31 ✓

H3.2 H3.1 52.6 52.8 52.6 52.9 H3.2
9.5 5.7 5.7 4.9 4.7 5.4 2.5
12 13 11 0 15 16 16 ✓

H3.1 H3.0 H3.2 H3.7 52.6 52.8 52.8 H4.6 H4.2 H4.2 H4.4
2.6 2.7 2.5 2.0 5.1 4.9 4.9 8.2 8.5 8.5 8.3
31 30 24 17 11 0 14 14 21 30 31 ✓

Sta. B.S. H.I. F.S. Elev.

960.88

116+00

116+50

+75=Ditch begins Rt. & Lt.

117+00

118+00

119+00

① 11.18 971.01 ✓ 1.05 959.83 ✓

120+00

121+00

122+00

② 10.10 980.45 ✓ 0.66 970.35 ✓

123+00

124+00

125+00

18.6 14.6 5.1 50.1 85.7 82.6 80.3 49.9
123 11.3 7.8 7.8 8.2 8.3 10.6 11.2
26 18 13 8 11 12 16 21

50.2 53.4 59.4 53.4 50.8 50.2
10.7 10.5 7.3 7.5 10.1 10.7
20 13 8 13 19 23

51.2 50.1 50.8 51.6 54.4 52.5 54.4 51.8 51.0 50.9 51.5
9.7 10.8 10.1 9.3 6.5 6.7 6.5 9.1 9.9 10.0 9.7
31 30 24 18 13 8 13 17 24 30 31

54.4 53.8 59.8 54.2 51.1 59.3 57.0 54.2 53.9 54.4 53.0
6.0 7.1 7.1 6.7 3.8 3.6 3.9 6.7 2.0 6.5 5.5
31 30 25 17 13 8 14 18 26 30 31

59.1 57.5 67.4 57.8 60.6 60.6 60.1 57.9 57.9 58.0 59.1
1.8 3.4 3.5 3.1 0.4 0.4 0.8 3.0 3.0 2.9 6.8
31 29 24 18 13 8 14 17 26 30 31

64.1 60.7 60.9 61.7 63.6 63.7 63.3 60.0 61.2 60.9 64.0
6.4 10.3 10.1 9.3 7.3 7.3 7.5 7.0 9.8 10.3 7.0
32 28 23 17 13 8 13 16 22 27 31

65.9 61.8 64.9 65.2 66.7 62.0 67.1 65.9 64.8 64.8 65.3
2.7 6.7 6.7 5.8 4.3 4.0 3.9 5.3 6.2 6.2 2.7
32 27 25 18 13 8 12 15 24 27 32

71.0 67.1 67.6 65.5 70.1 70.8 70.0 68.5 67.9 67.4 70.7
0.0 3.6 3.4 2.5 0.9 1.0 1.0 2.5 3.1 3.6 0.3
32 28 25 17 14 8 12 16 22 28 32

72.9 69.9 70.0 70.9 70.7 70.7 70.6 71.0 70.9 70.1 72.4
7.6 10.6 10.5 9.6 7.8 7.8 8.0 9.5 10.2 10.2 8.1
32 28 24 16 13 8 13 17 24 26 32

74.2 71.7 71.6 72.4 74.4 74.4 74.1 72.9 71.6 71.6 73.1
6.3 8.8 8.4 7.4 6.1 6.1 6.4 8.1 8.8 8.0 7.1
32 24 24 17 13 8 13 18 25 30 32

75.8 72.6 72.9 72.7 75.7 75.7 75.4 74.0 72.9 72.7 74.9
4.7 7.7 7.6 6.8 4.8 4.8 5.1 6.5 7.6 7.8 5.8
32 28 25 18 13 8 13 17 24 30 32

Sta. B.S. H.I. F.S. Elev.

98045

126+00

127+00

○ 7.45 986.66 1.24 979.21

128+00

129+00

129+50

130+00

131+00

132+00

133+00

○ 5.15 987.34 4.47 982.19

134+00

135+00

77.4 77.2 76.4 76.3 76.1 77.1 77.1 75.9 74.4 74.1 76.1
31 6.3 6.1 5.2 3.6 3.7 3.7 5.2 6.1 6.4 7.5
32 28 29 18 13 0 13 17 26 30 32

78.6 76.1 76.1 76.6 78.2 78.3 78.0 76.5 75.9 75.5 77.5
19 5.1 4.8 4.0 2.3 2.2 2.5 4.0 4.6 5.0 3.0
32 28 25 18 13 0 13 16 22 29 32

79.6 76.6 77.2 77.6 77.3 77.4 77.2 77.5 76.9 76.1 78.3
7.1 9.9 9.5 8.9 7.7 7.3 7.5 9.1 9.8 10.0 8.2
32 30 24 17 13 0 13 16 23 27 32

80.5 78.6 78.1 78.8 80.4 80.4 80.1 78.5 78.1 77.7 77.8
6.2 8.5 8.6 7.9 6.6 6.3 6.6 8.1 8.6 9.0 6.9
32 30 25 16 13 0 13 16 23 30 32

80.4 78.6 78.6 77.5 80.6 80.4 80.4 79.9 78.4 78.3 80.1
5.8 8.2 8.1 7.2 6.2 5.8 6.3 7.8 8.3 8.4 6.6
32 29 24 15 13 0 13 16 25 30 32

81.3 78.7 78.8 77.5 80.9 81.2 81.0 77.2 78.4 78.6 80.9
5.4 8.0 7.9 7.2 5.8 5.5 5.7 7.5 8.3 8.1 6.0
32 28 25 17 13 0 13 17 25 29 31

81.7 79.0 79.0 80.0 81.5 81.7 81.7 80.0 78.8 78.7 80.8
4.8 7.7 7.5 6.7 5.4 5.0 5.0 6.7 7.9 8.0 5.9
31 26 24 16 14 0 13 16 25 29 31

81.7 79.3 79.5 80.1 81.6 81.7 81.5 79.9 78.9 78.9 80.8
5.0 7.2 7.4 6.6 5.1 5.0 5.4 6.8 7.8 7.8 5.9
31 26 23 17 14 0 13 15 24 29 31

81.2 79.1 79.3 80.6 81.6 82.0 81.9 80.4 79.2 79.2 81.3
5.5 7.6 7.4 6.1 5.1 4.7 4.8 6.3 7.5 7.5 5.9
31 24 25 17 13 0 13 17 25 29 31

80.5 79.1 79.0 80.5 82.2 82.0 82.0 80.5 79.1 79.1 81.6
6.5 8.2 8.3 7.0 5.1 5.3 5.3 7.3 8.2 8.2 5.8
31 29 26 16 13 0 14 17 23 28 31

81.0 79.0 79.3 80.8 82.1 82.3 81.9 80.1 79.6 79.8 81.6
6.3 8.3 8.0 7.2 6.2 5.0 5.4 7.2 7.7 8.0 5.8
32 29 24 17 13 0 13 16 23 28 31

Sta. B.S. H.I. F.S. Elev.

987.39

136+00

137+00

138+00

139+00

○ 470 988.23 ✓ 3.81 983.53 ✓

140+00

+74 = 16' x 20' x 1.5 = 176 yd Add to Fill 15' x 20' Corr. Pipe on Lt.

141+00

142+00

143+00

144+00

145+00 = Ditch ends on Lt.

B.M. 479 990.20 ✓ 2.80 985.43 ✓ 985.41

145+15

6.1 7.9 7.7 6.8 5.0 4.9 5.2 6.5 7.2 8.2 5.7
32 29 25 17 13 0 17 17 25 28 31

5.9 7.6 7.6 6.8 7.8 7.7 5.0 7.0 7.8 8.0 5.6
32 29 25 17 13 0 13 17 24 28 31

5.5 7.4 7.3 6.7 7.4 7.2 7.5 6.5 7.5 7.5 5.5
31 28 26 18 13 0 13 17 25 29 31

5.1 6.6 6.6 6.0 3.7 3.5 7.0 6.0 6.9 6.9 4.9
31 29 23 17 13 0 17 17 25 29 31

5.1 6.2 6.5 5.2 3.8 3.9 7.1 6.7 7.0 7.1 5.2
31 29 25 17 13 0 13 17 25 29 31

4.0 5.7 5.6 4.8 3.6 3.5 3.4 5.4 6.1 5.9 4.9
28 24 21 16 13 0 17 18 26 29 31

3.3 5.0 5.0 4.4 3.3 3.0 3.3 4.3 5.0 5.0 3.3
29 26 23 16 13 0 17 17 24 29 31

3.9 5.2 5.1 4.6 3.6 2.5 2.6 4.1 4.6 4.5 3.5
31 29 24 17 13 0 17 17 25 29 31

4.9 5.9 5.8 5.1 2.6 2.5 2.5 4.5 4.9 4.6 3.6
32 30 25 18 13 0 13 17 24 29 31

5.9 6.6 6.6 6.0 3.1 2.8 3.2 5.8 5.9 5.7 3.8
31 30 24 18 13 0 17 18 25 29 32

on S. Hawk Conc. Curb. Sta. 145+20.5

8.2 5.1 4.9 5.2 7.8 8.2 8.0 5.9
16 13 8 14 18 24 29 32

Sta. B.S. H.I. F.S. Elev.

990.20

145+20.5 = E. Conc. Culv.

145+26

+95 = Ditch begins on Lt.

146+00 = Borrow begins on Rt.

147+00

148+00

15" x 20" corr. Pipe

+82 = 18' x 19' x 2.0' = 25 C.Y. Add to Fill on Lt.

149+00

150+00

+30 = Borrow ends on Rt.

150+50

① 8.61 997.11 1.70 998.50

151+00

152+00

153+00

$$\begin{array}{r} 81.4 \quad 85.4 \quad 85.5 \quad 85.5 \quad 85.4 \quad 85.4 \quad 85.4 \quad 81.6 \\ 8.8 \quad 4.8 \quad 4.7 \quad 4.7 \quad 5.0 \quad 4.8 \quad 4.8 \quad 8.6 \\ 14 \quad 19 \quad 13 \quad 0 \quad 16 \quad 16 \quad 17 \quad 17 \end{array}$$

$$\begin{array}{r} 81.4 \quad 85.4 \quad 85.5 \quad 85.5 \quad 82.1 \quad 82.1 \quad 82.0 \quad 83.9 \\ 8.3 \quad 5.1 \quad 4.9 \quad 5.2 \quad 7.5 \quad 8.2 \quad 8.2 \quad 6.3 \\ 18 \quad 13 \quad 0 \quad 16 \quad 17 \quad 24 \quad 29 \quad 32 \end{array}$$

$$\begin{array}{r} 81.8 \quad 80.8 \quad 86.7 \quad 82.0 \quad 85.2 \quad 85.3 \quad 84.6 \quad 82.0 \quad 81.0 \quad 85.3 \quad 88.8 \quad 83.6 \quad 83.8 \quad 84.0 \quad 85.2 \\ 8.7 \quad 9.3 \quad 9.5 \quad 8.2 \quad 5.0 \quad 4.9 \quad 5.4 \quad 7.4 \quad 7.9 \quad 6.9 \quad 6.4 \quad 6.6 \quad 6.9 \quad 6.2 \quad 6.0 \\ 32 \quad 30 \quad 25 \quad 18 \quad 13 \quad 0 \quad 15 \quad 19 \quad 29 \quad 36 \quad 45 \quad 53 \quad 59 \quad 62 \quad 64 \end{array}$$

$$\begin{array}{r} 81.6 \quad 81.6 \quad 81.6 \quad 81.6 \quad 81.6 \quad 81.6 \quad 81.6 \quad 81.6 \quad 81.6 \quad 81.6 \quad 81.6 \quad 81.6 \quad 81.6 \quad 81.6 \quad 81.6 \\ 7.7 \quad 8.6 \quad 8.7 \quad 8.4 \quad 5.0 \quad 5.0 \quad 5.0 \quad 7.8 \quad 7.8 \quad 7.1 \quad 6.9 \quad 7.0 \quad 6.7 \quad 5.5 \\ 32 \quad 30 \quad 26 \quad 20 \quad 13 \quad 0 \quad 13 \quad 19 \quad 31 \quad 38 \quad 50 \quad 58 \quad 59 \quad 64 \end{array}$$

$$\begin{array}{r} 83.6 \quad 83.6 \quad 83.6 \quad 83.6 \quad 83.6 \quad 83.6 \quad 83.6 \quad 83.6 \quad 83.6 \quad 83.6 \quad 83.6 \quad 83.6 \quad 83.6 \quad 83.6 \quad 83.6 \\ 6.6 \quad 7.2 \quad 7.2 \quad 7.0 \quad 4.0 \quad 4.1 \quad 4.5 \quad 7.0 \quad 6.8 \quad 5.9 \quad 5.8 \quad 4.4 \\ 31 \quad 30 \quad 26 \quad 18 \quad 13 \quad 0 \quad 14 \quad 18 \quad 31 \quad 50 \quad 58 \quad 65 \end{array}$$

$$\begin{array}{r} 84.8 \quad 84.8 \quad 84.8 \quad 84.8 \quad 84.8 \quad 84.8 \quad 84.8 \quad 84.8 \quad 84.8 \quad 84.8 \quad 84.8 \quad 84.8 \quad 84.8 \quad 84.8 \quad 84.8 \\ 9.8 \quad 5.9 \quad 5.8 \quad 5.7 \quad 3.5 \quad 3.1 \quad 3.3 \quad 6.0 \quad 6.0 \quad 5.2 \quad 4.9 \quad 4.6 \quad 4.8 \\ 31 \quad 30 \quad 25 \quad 17 \quad 13 \quad 0 \quad 13 \quad 18 \quad 28 \quad 40 \quad 50 \quad 59 \quad 65 \end{array}$$

$$\begin{array}{r} 86.6 \quad 86.6 \quad 86.6 \quad 86.6 \quad 86.6 \quad 86.6 \quad 86.6 \quad 86.6 \quad 86.6 \quad 86.6 \quad 86.6 \quad 86.6 \quad 86.6 \quad 86.6 \quad 86.6 \\ 3.6 \quad 4.7 \quad 4.7 \quad 4.2 \quad 2.4 \quad 2.1 \quad 2.1 \quad 4.6 \quad 4.4 \quad 3.5 \quad 3.2 \quad 3.2 \quad 2.7 \quad 2.2 \quad 1.7 \\ 31 \quad 50 \quad 25 \quad 17 \quad 13 \quad 0 \quad 13 \quad 18 \quad 28 \quad 38 \quad 50 \quad 54 \quad 62 \quad 63 \quad 65 \end{array}$$

$$\begin{array}{r} 86.9 \quad 86.9 \quad 86.9 \quad 86.9 \quad 86.9 \quad 86.9 \quad 86.9 \quad 86.9 \quad 86.9 \quad 86.9 \quad 86.9 \quad 86.9 \quad 86.9 \quad 86.9 \quad 86.9 \\ 3.3 \quad 4.3 \quad 4.2 \quad 3.7 \quad 4.5 \quad 4.5 \quad 4.5 \quad 3.3 \quad 3.2 \quad 2.3 \\ 31 \quad 29 \quad 24 \quad 16 \quad 13 \quad 0 \quad 13 \quad 18 \quad 26 \quad 32 \end{array}$$

$$\begin{array}{r} 86.9 \quad 86.9 \quad 86.9 \quad 86.9 \quad 86.9 \quad 86.9 \quad 86.9 \quad 86.9 \quad 86.9 \quad 86.9 \quad 86.9 \quad 86.9 \quad 86.9 \quad 86.9 \quad 86.9 \\ 2.6 \quad 4.8 \quad 4.6 \quad 4.0 \quad 2.8 \quad 7.7 \quad 7.5 \quad 9.7 \quad 10.3 \quad 10.3 \quad 8.1 \\ 31 \quad 29 \quad 24 \quad 17 \quad 12 \quad 0 \quad 17 \quad 16 \quad 26 \quad 29 \quad 32 \end{array}$$

$$\begin{array}{r} 87.1 \quad 87.1 \quad 87.1 \quad 87.1 \quad 87.1 \quad 87.1 \quad 87.1 \quad 87.1 \quad 87.1 \quad 87.1 \quad 87.1 \quad 87.1 \quad 87.1 \quad 87.1 \quad 87.1 \\ 7.7 \quad 9.5 \quad 9.2 \quad 8.7 \quad 6.9 \quad 6.7 \quad 6.8 \quad 8.7 \quad 9.2 \quad 9.2 \quad 7.3 \\ 31 \quad 29 \quad 25 \quad 16 \quad 13 \quad 0 \quad 14 \quad 18 \quad 24 \quad 29 \quad 31 \end{array}$$

$$\begin{array}{r} 87.1 \quad 87.1 \quad 87.1 \quad 87.1 \quad 87.1 \quad 87.1 \quad 87.1 \quad 87.1 \quad 87.1 \quad 87.1 \quad 87.1 \quad 87.1 \quad 87.1 \quad 87.1 \quad 87.1 \\ 6.0 \quad 7.8 \quad 7.9 \quad 7.2 \quad 5.5 \quad 5.5 \quad 5.7 \quad 7.5 \quad 8.6 \quad 8.9 \quad 5.6 \\ 31 \quad 29 \quad 24 \quad 17 \quad 13 \quad 0 \quad 14 \quad 19 \quad 24 \quad 28 \quad 31 \end{array}$$

Sta. B.S. H.L. F.S. Elev.

997.11

154+00

155+00

156+00

⊙ 7.51 1002.73 2.19 994.92 ✓

157+00

158+00

158+50

⊙ 6.48 1006.26 2.65 999.78 ✓

159+00

159+50

+55 = pitches and Rt. & Lt.

159+75+

160+00 = Ditches begin Rt. & Lt.

B.M.

8.19 998.07 998.16 ✓

filled in Walnut S. Side Rd. Sta. 160+30

91.4 89.8 90.0 90.8 92.7 92.9 92.9 91.1 90.6 90.4 92.8
5.7 23 21 6.3 4.7 4.2 4.2 6.0 6.6 6.7 4.8
32 30 24 17 13 0 13 18 23 28 31 ✓

90.7 89.7 89.6 90.6 91.0 91.1 91.4 90.7 90.4 90.9 91.9
6.4 7.4 7.5 6.5 3.1 2.7 2.8 6.4 6.7 6.8 4.8
31 30 26 19 13 0 13 19 24 29 31 ✓

91.2 91.5 91.6 90.0 91.0 91.7 91.4 91.1 90.1 90.6 91.2
6.4 7.6 7.6 7.1 2.1 1.4 2.0 5.9 6.4 6.3 4.9
31 30 27 22 13 0 13 20 27 30 31 ✓

92.1 91.1 91.0 91.7 91.6 91.6 91.4 92.9 92.7 92.9 91.1
10.3 11.3 11.4 10.7 5.9 5.8 6.0 9.5 9.7 9.5 8.0
30 27 26 21 13 0 12 20 25 30 32 ✓

90.7 91.6 91.8 91.7 91.1 91.8 91.6 91.6 91.6 91.6 91.6
6.7 7.9 7.6 6.7 4.3 4.2 4.1 5.8 6.6 6.8 3.9
30 28 24 18 14 0 14 19 25 28 32 ✓

91.5 91.3 91.2 91.0 91.8 91.6 91.1 91.5 91.2 1.7
3.9 6.1 6.2 5.4 3.6 3.4 3.3 4.9 5.2 0.7
30 27 23 18 14 0 15 20 25 32 ✓

91.3 91.6 91.8 91.8 91.9 91.2 91.1 91.5 91.1 91.2
7.0 8.5 8.5 8.0 6.4 6.1 5.9 7.2 7.5 7.6 1.1
31 25 22 18 14 0 16 19 22 26 34 ✓

91.6 91.7 91.6 91.7 91.6 91.6 91.6 91.6 91.6 91.6
1.8 2.6 5.8 5.6 5.8 6.2 6.2 6.2 6.2 6.2
31 24 16 0 32 38 42 45 48 51 ✓

0.0 0.1 0.1 0.0
1.3 6.2 6.2 6.0
33 0 19 33

91.9 91.7 91.7 91.6 91.6 91.7 91.7 91.6 91.6 91.6
6.4 8.6 8.6 8.8 7.8 7.6 7.6 8.2 8.2 8.8 5.4
31 27 24 18 15 0 15 18 24 28 31 ✓

7/10/28 P.M.

Twp. Borrow South

Sta. B.S. H.I. F.S. Elev.
B.M. 8.98 1007.14 ✓ 998.16 ✓
0+00 = 2 Twp. Rd. at S. Rwy. line Sta. 159+75.4

0+40 = Twp. Rd. S.

1+00 = Twp. Rd. S.

2+00 = Twp. Rd. S.

2+50 = End Twp. Borrow S.

Twp. Borrow North

0+00 = 2 Twp. Rd. at N. Rwy. Line Sta. 159+75.4

0+20 = Twp. Rd. N.

1+00 = End Twp. Borrow N.

Cedar Falls - Dunkerton Co. Rd.
Final X-Sections Twp. Rd. N. & S.
Opp. Sta. 159+75.4

Spike in Walk-out S. Side Rd. Sta. 160+30

1.9 98.5 98.5 99.1 0.1 6.4 99.8 1.8 0.0 1.8 5.9
6.2 8.6 8.4 7.7 7.0 6.7 7.3 5.3 5.1 5.8 1.4
24 21 17 15 0 32 36 43 50 67 81

1.3 98.9 98.8 0.5 0.6 1.0 0.1 0.1 2.0 2.0 3.9
5.8 8.2 8.3 6.2 6.5 6.1 7.0 7.0 5.1 5.1 1.2
23 19 17 14 0 13 17 19 21 29 35

1.1 99.2 99.0 0.6 0.6 1.0 99.8 99.8 6.9
6.0 7.9 7.9 6.5 6.6 6.1 7.3 7.3 1.8
22 18 16 13 0 11 15 17 24

98.9 91.5 97.4 98.2 98.9 99.0 98.2 98.2 3.3
8.2 9.6 9.7 8.4 8.2 7.8 8.9 8.9 2.9
20 18 16 12 0 13 17 19 22

97.5 96.0 96.0 97.4 97.4 96.9 95.9 95.9 97.7
9.6 11.1 11.1 9.5 9.5 10.2 11.2 11.4 9.8
18 16 14 10 0 15 17 19 21

1.1 99.8 99.6 0.0 99.8 99.8 98.5 98.7 0.2
3.0 7.3 7.5 7.1 7.3 7.3 8.3 8.4 6.9
28 23 20 18 0 13 17 19 22

0.9 98.6 98.4 99.2 99.5 99.5 98.4 98.5 0.4
4.2 8.5 8.7 7.9 7.6 7.9 8.7 8.6 6.7
27 22 20 18 0 14 17 19 21

06.3 95.5 95.4 96.1 96.2 96.1 95.1 95.1 96.0
10.8 11.6 11.7 11.0 10.9 11.0 12.0 12.0 11.1
21 20 19 17 0 9 12 14 15

9/10/28 P.M.

Cedar Falls - Dunkerton Co. Rd.
Final X-sections

8

Sta.	B.S.	H.I.	F.S.	Elev.
13.M.	0.69	998.85		998.16
161+00				
+65 = 17' X 22' X 1.8 = 24 C.Y. Add to Fill on Lt. 15" X 20" Corr. Pipe				
①	0.46	990.39	8.92	989.93

162+00

163+00

13.M.			10.78	979.61
8/13/28				
B.M.	2.11	981.72		979.61

164+00

165+00

166+00 = Barrow begins on Rt.

167+00

①	1.42	971.68	11.46	970.26
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168+00

+86 = 18' X 18' X 2.3 = 27 C.Y. Add to Fill on Lt.

169+00

169+50

Spike in Walnut S. Side Rd. Sta. 160+30

91.7	90.8	90.9	91.6	90.8	91.0	90.8	91.2	91.6
2.2	8.0	8.0	7.3	5.0	7.8	4.6	7.4	8.0
31	29	24	18	12	8	12	19	24

91.4	90.2	90.4	91.1	90.3	91.1	90.9	91.6	91.8
7.0	5.2	5.0	4.0	1.3	1.1	1.3	4.7	4.9
31	29	25	18	14	8	13	24	29

91.7	90.6	90.7	90.9	91.2	90.3	91.4	91.6	91.5
8.7	8.8	9.7	7.5	6.2	6.1	6.0	8.8	8.9
31	30	26	19	13	8	13	17	24

Nail in Cor. Post on Lt. Sta. 163+

91.1	90.9	91.1	91.5	90.5	91.0	90.8	91.8	91.0
3.6	4.8	4.6	3.9	1.2	1.1	1.3	3.9	3.9
31	24	20	17	13	8	13	17	24

91.0	91.4	91.5	91.1	91.9	91.9	91.3	91.7	91.5
6.1	7.3	7.2	4.6	4.4	4.4	4.9	6.0	6.2
31	30	25	18	13	8	13	17	25

91.2	91.7	91.5	91.4	91.1	91.5	91.1	91.9	91.2
7.5	9.0	8.9	8.3	6.6	6.5	6.1	7.6	6.8
31	29	24	18	13	8	13	17	24

91.6	91.0	91.2	91.6	91.9	91.8	91.5	91.4	91.3
10.1	11.7	14.7	14.9	8.8	8.8	8.8	10.2	13.5
31	29	24	17	13	8	13	16	22

91.6	91.1	91.3	91.0	91.2	91.4	91.6	91.4	91.5
3.1	4.6	4.4	4.1	1.5	1.3	1.3	3.3	3.4
31	29	25	18	13	8	12	16	24

91.5	91.4	91.5	91.4	91.2	91.1	91.3	91.1	91.2
6.2	7.3	7.7	7.1	3.4	3.3	3.4	6.0	6.1
31	30	26	23	14	8	13	19	26

91.8	91.4	91.5	91.7	91.6	91.1	91.4	91.5	91.4
2.5	8.3	8.4	8.0	4.2	4.0	4.1	6.9	2.1
31	30	27	21	13	8	13	18	26

Sta. B.S. H.I. F.S. Elev.

946.94

179+00

179+50

179+60

179+81 = $\frac{1}{2}$ Conc. Culv.

B.M.

6.01

940.95

941.35

Note: Sta. 180+00 to 189+00 Final X-sections

taken in Book #79 Page 28.

B.M. 5.25

943.96

938.21

189+88

189+95 = $\frac{1}{2}$ Conc. Culv.

190+00

+80 = Ditch begins on L.F.

191+00

192+00

+14 = 17' X 16' X 2.0' = 20.0 yd. Add to Fill on Rt. No corr. Pipe.

+25 Ditch begins on Rt.

193+00

10.37 952.69 1.17 942.32

91.8
22 5.2 5.1 5.1 8.6
21 13 8 13 19

97.1
9.9 5.7 5.2 5.6 8.5
20 12 8 12 17

96.5
10.5 5.6 5.3 5.6 10.6
23 14 8 14 25

94.9
12.1 5.6 5.5 5.3 5.4 6.0 94.5
16 16 14 8 14 16

on S. Hdwl. Conc. Culv. Sta. 179+81

on N. Hdwl. Conc. Culv. Sta. 189+95

91.8
2.8 5.2 5.1 5.4 8.3
19 13 8 12 17

94.1
9.4 5.3 5.3 5.1 5.4 5.6 9.3
14 14 13 8 13 17 14

95.1
8.4 5.4 5.2 5.4 8.3
17 13 8 13 16

96.1
2.7 7.6 8.0 2.7 5.5 5.3 5.7 8.7
31 28 23 17 13 8 13 18

96.5
2.9 2.2 2.1 2.0 4.4 4.3 4.5 2.6
31 29 24 17 12 8 13 19

91.0
2.5 2.3 4.2 3.9 4.9 2.0 2.3 4.5 4.8 5.1 3.6
31 26 22 17 12 8 13 18 24 28 31

Sta. B.S. H.I. F.S. Elev.

952.69

194+00

195+00

T.B.M. 1.45 951.24 ✓

8/19/28

D.S. Butterfield.
F.R. Krulish.
P.G. Hill.

T.B.M. 6.06 957.30 ✓ 951.24 ✓

195+50

196+00

196+50

+65' 16' x 16' x 3.0' = 28 C.Y. Add to Fill on Lt.

197+00

197+50

198+00

199+00

200+00

1.67 950.24 ✓ 8.73 948.57 ✓

H6.1 H2.9 H9.1 H3.2 H4.8 H5.1 H4.4 H3.1 H2.1 H3.4 H5.6
6.4 9.8 9.6 9.5 7.9 7.6 7.9 9.6 9.6 9.3 7.1
30 26 22 17 13 8 17 17 27 28 31

H2.3 H7.1 H7.1 H2.5 H5.4 H1.1 H8.9 H2.0 H7.2 H7.1 H9.9
9.4 5.6 5.6 5.4 3.8 3.6 3.8 4.7 5.5 5.6 2.8
30 23 20 15 12 6 13 16 22 26 31

Splice in fence post on Rt. Sta. 195+30

H4.4 H5.4 H6.6 H5.0 H5.0 H5.5 H4.3 H4.0 H4.7 H5.6
2.7 8.9 8.7 8.3 6.7 6.7 6.8 8.0 8.3 8.6 5.7
30 21 18 14 12 6 13 16 21 26 31

H5.8 H0.2 H4.8 H0.6 H1.7 H1.5 H1.8 H0.6 H0.3 H4.7 H2.9
1.5 7.1 7.5 7.3 5.6 5.5 5.5 6.7 7.2 7.4 4.5
30 21 18 16 11 8 12 13 21 26 31

H1.5 H0.9 H0.8 H1.1 H2.3 H2.4 H2.3 H1.1 H0.8 H0.5 H3.2
0.8 6.4 6.5 6.2 5.0 4.9 5.0 6.2 6.5 6.8 4.1
30 22 18 15 12 8 13 16 22 27 31

H5.9 H0.7 H0.5 H0.9 H2.4 H2.9 H0.3 H0.9 H0.4 H0.5 H0.8
1.4 6.6 6.8 6.4 4.9 5.0 5.0 6.4 6.9 6.8 4.5
30 23 21 17 12 8 12 16 22 26 31

H4.9 H0.2 H0.1 H0.6 H1.1 H1.4 H1.8 H0.4 H0.0 H0.0 H1.7
2.4 7.1 7.2 6.7 5.3 5.4 5.5 6.9 7.3 7.3 5.4
30 22 19 16 12 8 13 16 22 27 31

H3.4 H9.7 H9.4 H0.0 H0.8 H1.0 H1.8 H4.4 H4.1 H4.1 H0.8
3.4 7.4 7.9 7.3 6.5 6.3 6.5 7.9 8.2 8.2 6.5
30 23 18 14 12 8 12 15 23 28 31

H1.3 H7.3 H7.5 H1.5 H5.3 H8.4 H5.6 H6.9 H7.1 H6.8 H9.3
6.0 10.0 10.0 9.8 8.8 8.5 8.8 10.8 10.3 10.5 9.0
30 24 20 15 13 8 13 16 23 28 31

H4.1 H5.0 H3.0 H5.0 H6.4 H4.1 H4.0 H4.9 H4.1 H6.4
1.1 5.3 5.2 5.2 4.2 3.8 4.2 5.6 5.5 5.6 3.8
31 25 20 16 13 8 13 17 24 29 31

Sta. B.S. H.I. F.S. Elev.

950.24

201+00

202+00

1.08 939.18 12.14 938.10

203+00

204+00

205+00

206+00

2.09 931.92 9.35 929.83

207+00

208+00

209+00

210+00

2.21 927.01 7.12 924.80

211+00

114.9	111.3	111.5	111.5	113.0	113.3	113.3	111.4	111.4	111.2	113.3
5.3	8.9	8.7	8.7	7.2	6.9	6.9	8.8	8.8	7.0	6.9
31	25	21	17	13	8	13	16	23	28	31
10.2	98.0	98.1	98.2	100.2	10.2	100.2	97.6	97.9	97.1	97.1
100	12.2	12.1	12.0	10.0	10.0	10.0	12.6	12.5	12.8	11.1
31	28	24	17	13	0	13	18	24	28	31

85.6	84.7	84.3	84.3	87.4	87.6	87.1	85.0	84.6	83.9	84.8
5.7	7.5	7.9	7.9	1.8	1.6	2.1	4.2	5.2	5.3	4.4
31	29	25	19	13	0	19	19	25	30	31

83.3	82.9	81.2	82.5	84.6	84.8	84.6	82.2	81.7	81.7	82.4
5.9	6.4	7.0	6.7	4.6	4.4	4.7	7.0	2.5	2.5	6.8
32	31	24	17	13	0	17	17	23	24	31

81.4	81.0	80.4	80.7	82.7	82.9	82.1	80.2	79.6	80.1	80.4
7.3	8.2	8.8	8.5	6.5	6.3	6.6	7.0	9.4	9.1	8.5
29	28	21	15	13	0	13	19	28	29	31

80.4	81.3	80.7	80.8	80.9	81.0	81.0	80.9	80.4	80.7	80.6
8.8	8.9	10.5	10.4	8.3	8.2	8.2	10.3	10.6	10.6	8.6
30	29	23	17	13	0	13	16	22	26	30

28.2	27.0	26.9	27.2	29.0	29.3	29.3	26.8	26.9	27.0	28.3
3.7	4.9	5.0	4.7	2.9	2.6	2.6	5.1	5.2	4.9	3.6
30	28	21	16	13	0	13	16	24	26	31

26.1	25.2	25.0	25.1	27.8	27.9	27.6	25.2	24.9	25.1	26.2
5.8	6.7	6.4	6.8	4.1	4.2	4.3	6.7	7.0	6.8	5.7
31	30	25	18	13	0	13	16	24	29	31

24.4	23.7	23.9	23.9	26.0	26.0	26.2	23.7	23.4	22.9	23.6
7.5	8.2	8.2	8.0	5.9	5.7	5.7	8.2	8.5	8.2	7.3
31	30	25	18	13	0	13	16	24	29	31

23.6	22.9	22.7	22.4	25.2	25.2	25.2	23.1	22.9	22.2	23.4
8.4	9.0	9.2	9.0	6.7	6.7	6.6	8.8	10.0	9.7	8.5
31	30	25	19	13	0	13	16	25	30	31

23.2	22.2	22.1	22.0	24.8	24.7	24.4	22.0	21.6	21.4	22.4
3.9	4.8	4.9	5.0	2.2	2.3	2.4	5.0	5.2	5.6	4.6
31	30	25	18	13	0	13	16	24	29	31

Sta. B.S. H.I. F.S. Elev.

927.01

212+00

B.M. 3.69 927.00 ✓ 3.69 923.32 ✓ 923.31

+42 = Ditches end Rt. & Lt.

212+68.7 = E. Top. Rd. N. & S.

18" X 24' = Corr. Pipe on Lt.

+95 = Borrow begins on Lt.

213+00 = Ditches begin Rt. & Lt.

214+00

215+00

① 3.93 922.59 ✓ 8.34 918.66 ✓

216+00

217+00

218+00

219+00

+65 = Borrow ends on Lt.

220+00

+30 = Ditch ends on Lt.

B.M. 2.43 921.84 ✓ 3.18 919.41 ✓ 919.42

+50 = Ditch ends on Rt.

220+50

23.0 22.0 21.9 21.8 22.8 23.6 23.7 21.5 20.9 21.2 22.5
4.0 5.0 5.1 5.2 3.2 3.4 3.3 5.5 4.1 5.8 4.5
3.1 2.9 2.9 1.0 1.2 0 1.3 1.7 2.4 2.9 3.1

8 Conc. base Flag-pole School Yard N. Side Rd. 574.212+33

23.4 23.4 23.2 23.2 22.5 22.1 22.0

3.4 3.4 3.7 3.8 4.5 4.9 5.0

3.3 2.5 1.2 0 1.0 2.6 3.3

23.6 23.6 22.5 22.3 21.5 20.9 21.2 22.4 22.6 22.4 21.6 21.4 20.6 21.7
3.4 4.5 4.7 4.5 5.6 1.5 5.8 4.6 4.4 4.6 3.5 3.6 6.5 5.3
8.5 8.4 6.7 5.0 3.2 2.3 1.5 1.3 0 1.3 1.6 2.1 2.8 3.0

23.6 23.6 22.5 22.3 21.5 20.9 21.2 22.4 22.6 22.4 21.6 21.4 20.6 21.7
4.5 5.8 5.6 6.0 7.0 7.8 7.4 5.8 5.7 6.0 2.8 2.9 2.9 5.2
8.6 8.6 6.4 5.0 3.7 2.3 1.6 1.3 0 1.3 1.6 2.2 2.8 3.1

21.6 21.6 21.6 19.1 18.9 8.1 15.6 19.4 20.0 19.9 16.0 19.0 16.1 21.2
5.4 6.6 6.4 7.3 8.1 9.0 8.5 7.1 7.0 7.1 9.0 9.0 8.9 5.8
8.4 8.3 7.3 5.0 3.9 2.7 1.6 1.3 0 1.3 1.7 2.0 2.7 3.1

19.4 19.4 18.2 18.1 18.1 11.1 10.9 14.1 15.2 15.9 11.9 16.1 16.1 18.4
3.2 4.2 4.4 4.5 4.8 5.5 5.7 3.7 3.7 3.7 5.7 6.0 6.0 3.7
8.4 8.3 7.2 5.0 4.2 2.8 1.7 1.3 0 1.3 1.7 2.2 2.8 3.1

16.2 16.2 14.7 14.6 14.4 14.1 18.1 16.1 18.0 14.3 13.8 13.6 14.4
7.4 8.1 7.9 8.0 8.2 8.2 4.5 4.9 4.6 8.3 8.8 9.0 9.5
6.4 6.2 5.0 4.2 2.8 1.8 1.3 0 1.3 2.0 2.2 2.6 2.7

14.4 13.4 13.4 13.4 13.6 13.4 17.4 17.6 17.0 13.2 13.1 12.6 13.7
8.0 8.7 8.7 8.7 8.0 9.2 5.2 5.0 5.0 9.4 9.5 9.8 8.9
6.2 6.0 5.0 4.2 3.2 2.0 1.2 0 1.3 1.9 2.2 2.6 2.8

14.2 13.2 13.2 13.2 13.3 12.4 14.3 14.3 12.1 12.8 12.6 12.6 13.6
8.4 9.1 9.2 9.1 9.3 10.2 5.1 5.4 5.5 9.8 10.0 9.8 9.0
6.1 5.9 5.0 4.0 3.1 2.1 1.2 0 1.3 2.1 2.3 2.5 2.7

13.1 12.2 11.6 13.1 13.3 16.9 16.8 16.3 13.6 13.3 12.1 12.0 13.9
8.9 10.4 11.0 9.5 9.3 5.7 5.8 5.8 9.0 9.3 10.5 10.4 8.7
3.5 2.8 2.3 2.2 1.9 1.3 0 1.3 1.9 2.3 2.6 2.9 3.1

② on N. Conc. Hdr'l. 574.220+70

16.1 16.1 16.1
5.1 5.1 5.1
1.3 0 1.3

Sta.	B.S.	I.I.	F.S.	Elev.
1	1.25		1.25	100.00
2	1.50		1.50	100.50
3	1.75		1.75	101.00
4	2.00		2.00	101.50
5	2.25		2.25	102.00
6	2.50		2.50	102.50
7	2.75		2.75	103.00
8	3.00		3.00	103.50
9	3.25		3.25	104.00
10	3.50		3.50	104.50
11	3.75		3.75	105.00
12	4.00		4.00	105.50
13	4.25		4.25	106.00
14	4.50		4.50	106.50
15	4.75		4.75	107.00
16	5.00		5.00	107.50
17	5.25		5.25	108.00
18	5.50		5.50	108.50
19	5.75		5.75	109.00
20	6.00		6.00	109.50
21	6.25		6.25	110.00
22	6.50		6.50	110.50
23	6.75		6.75	111.00
24	7.00		7.00	111.50
25	7.25		7.25	112.00
26	7.50		7.50	112.50
27	7.75		7.75	113.00
28	8.00		8.00	113.50
29	8.25		8.25	114.00
30	8.50		8.50	114.50
31	8.75		8.75	115.00
32	9.00		9.00	115.50
33	9.25		9.25	116.00
34	9.50		9.50	116.50
35	9.75		9.75	117.00
36	10.00		10.00	117.50
37	10.25		10.25	118.00
38	10.50		10.50	118.50
39	10.75		10.75	119.00
40	11.00		11.00	119.50
41	11.25		11.25	120.00
42	11.50		11.50	120.50
43	11.75		11.75	121.00
44	12.00		12.00	121.50
45	12.25		12.25	122.00
46	12.50		12.50	122.50
47	12.75		12.75	123.00
48	13.00		13.00	123.50
49	13.25		13.25	124.00
50	13.50		13.50	124.50
51	13.75		13.75	125.00
52	14.00		14.00	125.50
53	14.25		14.25	126.00
54	14.50		14.50	126.50
55	14.75		14.75	127.00
56	15.00		15.00	127.50
57	15.25		15.25	128.00
58	15.50		15.50	128.50
59	15.75		15.75	129.00
60	16.00		16.00	129.50
61	16.25		16.25	130.00
62	16.50		16.50	130.50
63	16.75		16.75	131.00
64	17.00		17.00	131.50
65	17.25		17.25	132.00
66	17.50		17.50	132.50
67	17.75		17.75	133.00
68	18.00		18.00	133.50
69	18.25		18.25	134.00
70	18.50		18.50	134.50
71	18.75		18.75	135.00
72	19.00		19.00	135.50
73	19.25		19.25	136.00
74	19.50		19.50	136.50
75	19.75		19.75	137.00
76	20.00		20.00	137.50
77				

921.84

220783.

221+00 = Ditch begins on Lt.

+75 =	11	12	11	Pf.
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222+00

223400

224+00

225700

①	6.04	923.57	4.31	917.53
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226400

227+00

228400

229+00

230 + 00

①	7.56	926.56	4.57	919.00
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12.9	12.1	12.0	13.2	16.9	16.6	16.7	11.1
8.9	9.7	8.8	8.6	4.9	5.0	5.1	10.7
33	32	26	21	13	0	13	25
16.1	14.1	11.1	10.0	16.1	16.1	16.1	19.0
5.4	7.7	8.0	6.8	5.3	5.1	5.3	8.6
33	30	24	16	13	0	14	20
11.1	15.1	14.1	11.1	11.1	16.1	16.1	19.1
4.7	6.7	6.9	6.3	4.6	4.9	4.9	7.2
31	28	23	16	13	0	14	19
16.6	15.0	15.0	16.6	11.1	11.1	16.1	16.1
5.0	6.8	6.8	6.2	4.1	4.2	8.6	6.1
31	28	24	17	13	0	13	18
11.1	15.1	15.1	16.0	11.1	15.1	16.1	16.1
4.7	6.3	6.5	5.8	4.2	3.7	4.0	5.9
31	28	24	18	13	0	13	17
11.1	15.1	15.1	16.1	11.1	15.1	16.1	16.1
6.1	8.1	7.9	7.5	5.9	5.7	5.5	7.5
30	28	24	17	13	0	14	18
11.1	16.1	15.1	16.1	16.1	16.1	16.1	16.1
6.1	7.5	7.8	7.4	5.1	5.1	5.2	7.5
30	28	23	16	12	0	13	17
16.1	15.1	15.1	16.1	16.1	16.1	16.1	16.1
6.1	7.7	8.0	7.5	5.4	4.9	5.4	7.6
31	29	25	19	14	0	13	19
16.6	16.0	15.1	16.1	16.1	16.1	16.1	16.1
7.0	7.4	7.9	7.5	5.1	4.7	5.9	7.3
30	29	25	19	14	0	14	17
16.6	16.1	16.1	16.1	16.1	16.1	16.1	16.1
6.8	7.3	7.5	7.2	4.9	4.5	4.9	7.6
30	29	24	17	13	0	14	18

Sta. B.S. H.I. F.S. E/ev.

944.07

241+00

242+00

243+00

○ 11.56 955.10 0.53 943.54 ✓

244+00

245+00

246+00

246+50

○ 7.70 960.29 2.51 952.59 ✓

247+00

+70 = ditch ends on Rt.

248+00

249+00

250+00

12.2 13.6 13.6 13.3 10.9 10.7 10.8 12.7 13.7 14.2 12.2
31 28 27 17 13 0 13 17 23 28 30

8.1 10.0 10.0 9.7 7.5 7.0 7.3 7.3 9.5 9.6 7.9
30 28 27 16 12 0 14 18 24 28 31

3.9 5.6 5.7 5.4 3.7 3.4 3.3 3.9 4.9 5.0 2.9
30 27 22 15 12 0 13 15 21 26 30

9.3 13.2 12.8 12.3 11.1 10.7 11.1 12.4 12.6 12.8 9.5
30 26 21 15 12 0 12 16 22 26 30

3.8 7.3 7.2 8.8 7.3 7.7 7.6 7.1 9.6 9.7 5.7
30 23 20 15 12 0 13 14 21 25 30

6.2 5.8 5.7 5.5 4.3 4.0 4.5 5.8 5.9 6.2 3.1
30 23 20 15 12 0 13 16 22 25 30

+ 0.7 9.8 4.4 4.1 3.0 2.7 3.5 4.6 4.8 4.6 2.3
30 23 18 14 13 0 13 16 24 27 30

7.3 8.9 8.8 8.4 7.0 7.0 7.5 8.7 9.1 9.3 7.8
30 24 21 15 12 0 14 17 22 27 30

5.1 8.0 7.6 6.8 5.7 5.7 6.1 8.5
30 26 22 17 14 0 14 19

5.1 7.7 7.3 7.0 5.1 5.0 5.2 8.9
30 26 23 17 14 0 13 17

5.1 6.6 7.0 6.9 2.7 4.4 4.7 8.3
30 28 23 17 13 0 13 19

Sta B.S. H.I. F.S. Elev.

960.29

251+00 = Ditch begins on Rt.

251+50

252+00

○ 7.52 966.55 1.26 959.03

253+00

254+00

254+50

255+00

15" X 20' Corr. Pipe

+88 = 15' X 18' X 1.7' = 17 C.Y. Add to Fill on Rt.

256+00

15" X 20' Corr. Pipe

+21 = 16' X 17' X 2.7' = 27 C.Y. Add to Fill on Lt.

257+00

○ 1.57 956.87 11.25 955.30

258+00

+70 = Ditch ends on Rt.

259+00

15" X 20' Corr. Pipe

+39 = 15' X 17' X 2.7' = 25 C.Y. Add to Fill on Rt.

4.6 6.4 6.4 6.3 4.1 3.6 3.7 7.8 8.3 8.0 8.2
30 27 24 18 13 0 14 20 25 29 30

4.3 5.6 5.9 6.1 3.3 2.9 3.0 6.7 7.2 6.9 5.9
30 29 25 19 14 0 14 20 24 28 30

2.7 4.2 4.4 4.9 2.2 1.8 1.8 4.9 5.0 4.8 3.4
30 28 23 17 12 0 13 18 24 29 30

5.7 8.7 8.4 8.2 6.8 6.5 7.0 8.3 8.6 8.7 6.9
30 26 22 16 13 0 13 17 22 27 30

3.6 6.8 6.6 6.4 5.0 4.9 5.3 6.8 7.1 7.3 5.1
30 24 20 15 12 0 13 16 23 26 30

3.0 6.5 6.4 6.1 4.0 4.5 4.9 6.5 6.9 7.0 4.9
30 25 21 15 12 0 13 17 21 26 30

3.1 7.1 6.8 6.6 5.1 4.7 5.4 6.6 7.2 7.3 5.1
30 24 20 15 12 0 13 17 22 26 30

4.9 8.8 8.8 8.4 7.0 7.0 7.7 8.8 9.3 9.3 6.9
30 24 20 15 12 0 13 17 23 26 30

7.2 11.8 11.1 9.7 9.6 10.1 11.3 11.8 11.8 9.0
30 23 15 12 0 14 16 20 24 30

0.1 4.0 4.3 3.9 2.8 2.6 3.2 4.2 4.5 4.7 2.0
30 25 22 13 12 0 13 16 21 25 30

5.2 7.4 7.5 7.0 5.0 4.8 4.9 7.8 7.8 7.8 7.8
30 26 23 16 13 0 13 18

Sta. B.S. H.I. F.S. Elev.

956.87

259+50 = Ditch ends on Lt.

260+00

260+06 = $\frac{1}{2}$ Conc. Calc.

260+12

+70 = Ditch begins on Lt.

261+00 = Ditch begins on Rt.

262+00

262+50

263+00

O 11.53 963.21 519 951.68 ✓

264+00

265+00

+58 = Ditches end Rt. & Lt. ✓

B.M.

3.87

959.34 959.45

$$\begin{array}{r} 49.9 \quad 49.5 \quad 49.0 \quad 48.5 \quad 48.0 \quad 47.5 \quad 47.0 \quad 46.5 \\ 8.0 \quad 8.6 \quad 8.9 \quad 8.6 \quad 5.7 \quad 5.4 \quad 5.6 \quad 8.8 \\ 30 \quad 29 \quad 25 \quad 19 \quad 13 \quad 8 \quad 13 \quad 20 \end{array}$$

$$\begin{array}{r} 46.9 \quad 50.8 \quad 51.0 \quad 50.7 \quad 49.4 \\ 10.0 \quad 6.1 \quad 5.9 \quad 6.2 \quad 7.5 \\ 20 \quad 12 \quad 8 \quad 13 \quad 17 \end{array}$$

$$\begin{array}{r} 44.5 \quad 44.9 \quad 50.4 \quad 50.0 \quad 50.7 \quad 49.1 \quad 48.5 \quad 48.9 \\ 11.9 \quad 7.0 \quad 6.1 \quad 5.9 \quad 6.2 \quad 7.3 \quad 7.3 \quad 11.6 \\ 13 \quad 13 \quad 11 \quad 8 \quad 12 \quad 13 \quad 14 \quad 17 \end{array}$$

$$\begin{array}{r} 47.5 \quad 50.8 \quad 50.9 \quad 50.5 \quad 46.9 \\ 9.7 \quad 6.1 \quad 6.0 \quad 6.4 \quad 10.0 \\ 18 \quad 12 \quad 8 \quad 13 \quad 16 \end{array}$$

$$\begin{array}{r} 49.2 \quad 47.9 \quad 47.6 \quad 47.9 \quad 50.5 \quad 50.0 \quad 46.4 \quad 46.5 \quad 46.8 \\ 7.7 \quad 9.0 \quad 9.3 \quad 9.0 \quad 6.9 \quad 6.4 \quad 6.9 \quad 10.1 \quad 10.7 \\ 30 \quad 29 \quad 22 \quad 17 \quad 13 \quad 8 \quad 14 \quad 21 \quad 25 \end{array}$$

$$\begin{array}{r} 47.8 \quad 47.9 \quad 47.7 \quad 47.6 \quad 50.5 \quad 50.7 \quad 50.5 \quad 47.7 \quad 47.2 \quad 47.5 \quad 47.6 \\ 7.1 \quad 8.0 \quad 8.2 \quad 8.3 \quad 6.4 \quad 6.2 \quad 6.6 \quad 7.2 \quad 9.7 \quad 9.6 \quad 9.3 \\ 30 \quad 29 \quad 23 \quad 18 \quad 13 \quad 8 \quad 13 \quad 18 \quad 24 \quad 24 \quad 30 \end{array}$$

$$\begin{array}{r} 50.7 \quad 49.2 \quad 49.0 \quad 49.1 \quad 51.0 \quad 51.2 \quad 51.0 \quad 47.5 \quad 47.6 \quad 47.8 \\ 6.2 \quad 7.7 \quad 7.9 \quad 7.8 \quad 5.9 \quad 5.7 \quad 5.9 \quad 9.0 \quad 9.3 \quad 9.7 \quad 9.8 \\ 30 \quad 28 \quad 23 \quad 17 \quad 14 \quad 8 \quad 13 \quad 19 \quad 23 \quad 24 \quad 30 \end{array}$$

$$\begin{array}{r} 51.4 \quad 49.8 \quad 49.5 \quad 49.6 \quad 51.4 \quad 51.1 \quad 51.6 \quad 48.4 \quad 48.4 \quad 48.5 \quad 48.7 \\ 5.5 \quad 7.1 \quad 7.4 \quad 7.1 \quad 5.1 \quad 4.8 \quad 5.3 \quad 8.1 \quad 8.5 \quad 8.6 \quad 8.2 \\ 30 \quad 28 \quad 21 \quad 17 \quad 13 \quad 8 \quad 14 \quad 19 \quad 24 \quad 24 \quad 30 \end{array}$$

$$\begin{array}{r} 51.4 \quad 49.1 \quad 49.0 \quad 49.2 \quad 51.2 \quad 51.0 \quad 51.6 \quad 48.4 \quad 48.4 \quad 48.5 \quad 48.7 \\ 9.4 \quad 11.1 \quad 11.2 \quad 11.0 \quad 9.2 \quad 8.9 \quad 9.0 \quad 12.3 \quad 12.4 \quad 12.3 \quad 11.6 \\ 30 \quad 28 \quad 22 \quad 17 \quad 13 \quad 8 \quad 13 \quad 19 \quad 24 \quad 24 \quad 30 \end{array}$$

$$\begin{array}{r} 51.4 \quad 49.1 \quad 49.0 \quad 49.2 \quad 51.2 \quad 51.0 \quad 51.6 \quad 48.4 \quad 48.4 \quad 48.5 \quad 48.7 \\ 6.2 \quad 8.3 \quad 8.6 \quad 8.4 \quad 6.7 \quad 6.3 \quad 6.7 \quad 9.3 \quad 9.6 \quad 9.8 \quad 8.5 \\ 30 \quad 27 \quad 23 \quad 16 \quad 13 \quad 8 \quad 14 \quad 18 \quad 24 \quad 24 \quad 31 \end{array}$$

Spike root double Maple S. Side Rd. Sta. 266+

Finished 8/14/28 - 5:10 P.M.

D.S. Butterfield - F.R. Krulish - P.G. Hill - Hot and tired.

Channel Change N. of Culv.

Opp. Sta. 220+70

$$60' \times 14' \times 1.7 = 52 \text{ C.Y.}$$

$$52' \times 12' \times 2.0' = 46 \text{ C.Y.}$$

$$\underline{\quad 98 \text{ C.Y.} = \text{Total} \quad}$$

Channel Change S. of Culv.

Opp. Sta. 220+7

$$100' \times 13' \times 1.7 = 81 \text{ C.Y.}$$

Levels on each side of Road
by Culv. on Anthony Land.
Bot. Sec. { 16 - ead
21 - Big cr.

S. Side
Road.

B.M.	3.75	103.75	100.00
00.		4.7	
+90		6.0	
1+00	Ditch	8.8	
1+10		5.6	
2+00		5.8	
2+90		6.8	
3+00	Ditch	7.9	
3+30	* Culv. 4x3	6.7	
4+00		6.5	
6+00		7.0	
6+25		8.1	
8+00		7.8	
10+00		10.00	
10+30		8.4	
11+70		9.8	
12+00		8.4	
14+00		8.5	

N. Side
Road.

S. Hd. wall.
W. of 4x3 approx 100' So. of fence.

		4.9		No. channel				
7.7	9.0	6.4	10.5	10.3	10.8	11.1	10.7	
100	300	500	700	900	1100	1300		
5.0	7.1	4.9	4.4	80.				
300	500	700	900					
	7.6	7.7	8.0					
	9.4							
	9.0							

6/5/30 P.M.

D.S.B.
C.V.C.
B.V.
I.P.Spring Creek Twp. Between Secs.
17, 18-87-11 Levels for Tile W. side
of Road.

22

Sta.	B.S.	H.I.	F.S.	Elev.	Grade	Cut.
B.M.	4.15	104.15		100.00		Spike in Tel. Pole #5105 E. Side of Rd. Approx Sta. 1450
0+00			5.05	99.10	96.50	2.60 W. side of Rd. opp. Tel. Pole #5104, thence N. 2900'
1+00			5.47	98.68	96.31	2.37
2+00			5.85	98.30	96.13	2.17
3+00			6.18	97.97	95.94	2.03
4+00			6.35	97.80	95.75	2.05
5+00			6.96	97.19	95.56	1.63
6+00			7.35	96.80	95.38	1.42
7+00			7.31	96.84	95.19	1.65
○	8.04	104.88	7.31	96.84		
8+00			8.04	96.84	95.00	1.84
9+00			7.92	96.96	94.50.81	1.46 2.15
9+50			7.15	97.73	95.75	1.98
9+54			5.96	98.98	95.77	3.21
9+72			5.99	98.89	95.86	3.03
9+75			6.98	97.90	95.87	2.03
10+00			7.32	97.56	96.00 ^{94.6}	1.56 2.94
11+00			6.91	97.97	96.50 ^{95.20}	1.47 2.73
11+79			6.70	98.18	96.90 ^{95.8}	1.28
11+83			5.69	99.19	96.91	2.28
12+00			5.95	98.93	97.00 ^{95.8}	1.93 3.05
12+04			6.19	98.09		
13+00			6.12	98.76	96.50	2.26
14+00			5.13	98.75		

Sta.	B.S.	H.I.	F.S.	Elev.	Grade	Cut
		104.88				
15+00			3.79	101.09		
①	8.97	110.06	3.79	101.09		
16+00			9.30	100.76		
17+00			8.32	101.74		
18+00			7.19	102.87		
19+00			6.34	103.72		
20+00			6.12	103.94		
21+00			7.36	102.70		
22+00			7.68	102.38		
①	6.91	109.29	7.68	102.38		
23+00			7.63	101.66		
23+81			6.93	102.36		
23+84			5.92	103.37		
24+00			5.86	103.43		
24+06			6.15	103.14		
24+09			6.93	102.36		
25+00			7.19	102.10		
26+00			6.09	103.20		
27+00			4.89	104.40		
28+00			4.05	105.24		
29+00			1.79	107.50		
B.M.			6.57	102.72		

= Toe of W. Shoulder

= Center of W. Ditch

= Toe of W. Back-slope

" " " "

" " " "

= Toe of W. Back-slop

= Toe. of W. shoulder.

= Toe of W. Should & Junction of Outlet Tile East.

Spike in Tel. Pole # 5123 E. Side of Rd. Sta. 24+75

6/6/30

D. J. B.
C. V. C.
J. W.
B. J.

Spring Creek Twp.

24

Levels on Outlet Tile E.

Sta.	B.S.	H.I.	F.S.	Elev.	Grade	Cut
B.M.	2.43	105.15		102.72		
14+71=			3.50	101.65		
23+00			2.39	102.76		
14+68			2.45	102.70		
14+43			4.31	100.84		
14+37			4.59	100.56		
14+30			3.64	101.51		
14+28			5.02	100.13		
14+00			6.28	98.87		
13+00			7.10	98.05		
12+00			7.18	97.97		
11+00			8.54	96.61		
10+00	4.46	101.07	8.54	96.61		
9+00			6.04	95.03		
8+00			6.16	94.91		
7+00			5.58	95.49		
6+00			5.34	95.73		
5+00			5.73	95.34		
4+00			5.92	95.15		
3+00	3.75	98.90	5.92	95.15		
2+00			3.95	94.95		
1+00			5.00	93.90		
0+00			6.23	92.67		
0+08			8.06	90.84		
0+00=			10.47	88.43		
B.M.			4.87	94.03		

Spike in Tel. Pole # 5123 E. side of Rd. Sta. 24+75
= Junction of Outlet Tile E. at toe of W. shoulder.

Outlet
Spike in cut just Sta. 1+25.

Sta.	B.S.	H.I.	F.S.	Elev.	Grade	Cut.
------	------	------	------	-------	-------	------

0+00 = Outlet at ditch

10+00 = Δ

Outlet thru Kraft's
field.

19+40 = Δ

26+13 = Sta. 10+00 on Rd.

Rd. Tile = 1200'

6+00 intake

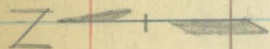
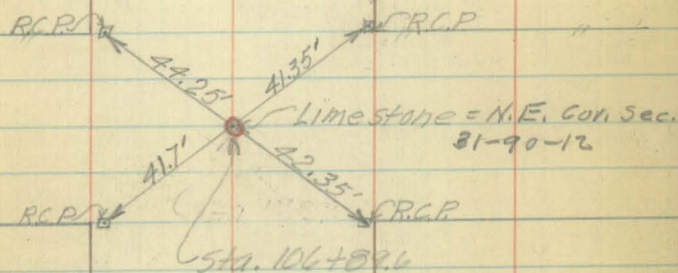
5+25' gravel and pit

0+00 = pole slot = 100' N of $\frac{1}{2}$ 1/2 1/2

Sec. 27-90-12
Bennington Twp.

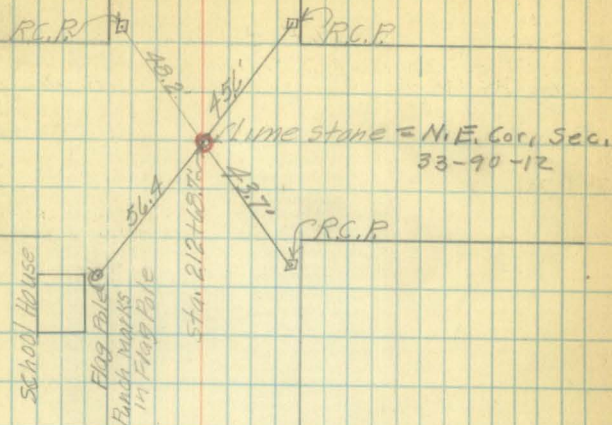
Sec. 32-90-12
Bennington Twp.

Sta. 133+36.1 = N. 1/4 Cor. Sec. 32-90-12
Sec. 29, R.C.P. 31.9' 31.95' R.C.P. Sec. 32-90-12
90-12 Stone Bennington Twp.
Bennington Twp.

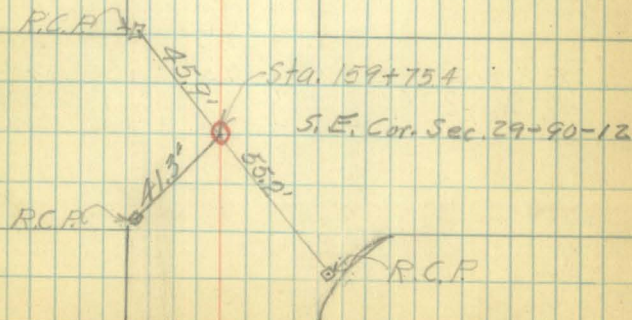


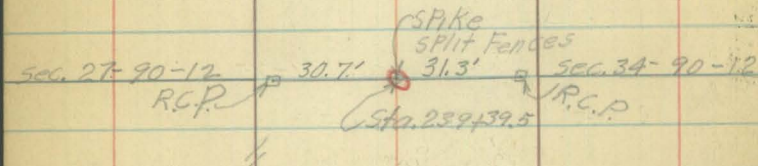
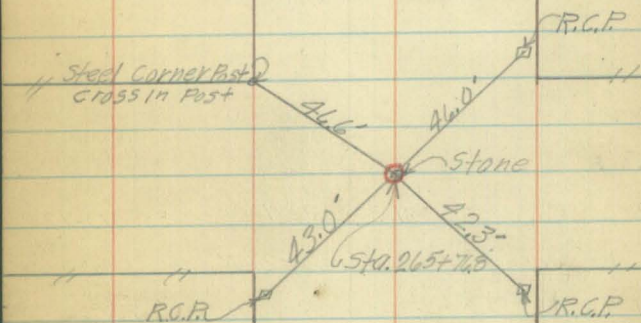
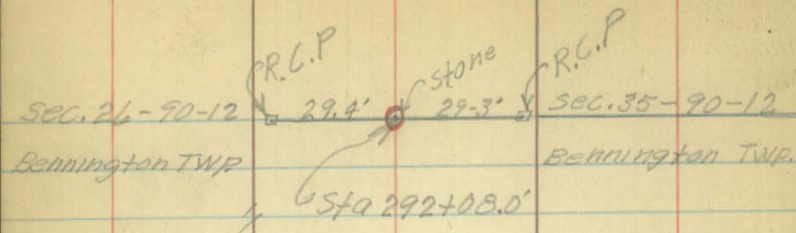
N. 1/4 Cor. Sec. 31-90-12
Sta. 80+41.0'

Sec. 30, R.C.P. 31.5' 33.8' R.C.P. Sec. 31-90-12
90-12 Stone Bennington Twp.
Bennington Twp.



Sec. 28-90-12 R.C.P. 31.3' 31.3' R.C.P. Sec. 33-90-12
Bennington Twp. Bennington Twp.
Sta. 181+24.7' = N. 1/4 Cor.



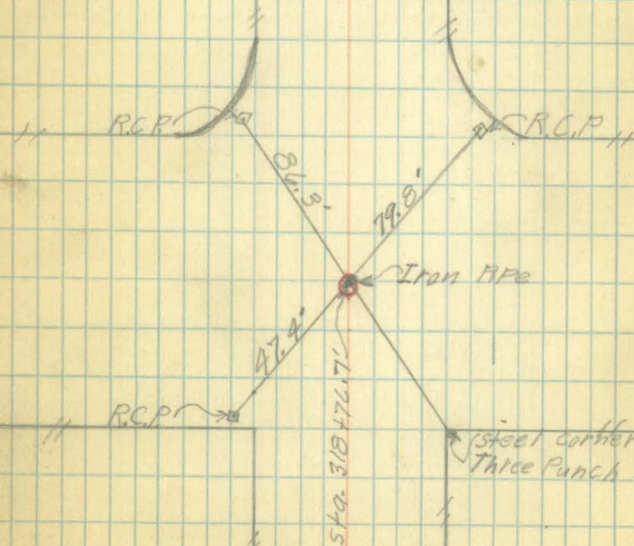


SEC. 25-90-12

Bennington Twp.

SEC. 36-90-12

Bennington Twp.



July 2nd 1936R.S.B.
C.J.C.
B.V.
J.W.Hudson-Hicks Co. Rd.
Tide Profile along toe of S.E.
Shoulder Sta. 69+73 to 83+37

28

30'

Sta.	B.S.	H.I.	F.S.	Elev.	Grade
B.M.	1.78	898.89		897.11	
Outlet			13.02	885.87	
+00 = Sta. 83+37			9.22	889.67	885.90
1+00			8.22	890.67	886.01
1+20			7.67	891.22	886.03
1+26			5.72	893.17	886.04
1+37			5.72	893.17	886.05
1+44			7.38	891.51	886.06
2+00			7.79	891.10	886.13
2+27			7.26	891.63	886.16
2+31			5.66	893.23	886.17
3+00			4.93	893.96	886.25
3+29			5.25	893.64	886.28
3+35			6.62	892.27	886.29
4+00			7.14	891.75	886.37
5+00			7.24	891.65	886.49
0	7.71	899.36	7.24	891.65	
6+00			7.40	891.96	886.60
7+00			7.53	891.83	886.72
8+00			7.69	891.67	886.84
9+00			8.19	891.17	886.96
10+00			8.46	890.90	887.07
11+00			9.06	890.30	887.19

Cut

① Center S.E. Conc. Hdtl. Conc. I-Beam. Sta. 83+85

3.77

4.66

5.19

7.13

7.12

5.45

4.97

5.47

7.06

7.71

7.36

5.98

5.38

5.16

5.36

5.11

4.83

4.21

3.83

3.11

Sta.	B.S.	H.I.	F.S.	Elev.	Grade	Cut
	899.36					
12+00		9.26	890.10	887.31		2.79
13+00		8.92	890.44	887.42		3.02
13+50		9.12	890.24	887.47		2.77
13+60 = $\frac{1}{2}$ Inlet Culv.		10.47	888.89	887.50		1.39
B.M.		5.77	893.56	<u>893.47</u>	Spike in Center S.E. Hdwl. Conc. Culv. Sta. 68+73.5	

July 2nd 1930

D.S.B.
C.J.C.
B.J.
J.W.Spring Creek Twp. Outlet Tile East
thru Kraft field

30

Sta.	B.S.	H.I.	F.S.	Elev.	Grade
B.M.	3.55	101.11		97.56	
B.M.			3.29	97.82	
26+13=10+00			3.55	97.56	94.50
26+10			2.52	98.59	94.47
26+00			2.35	98.76	94.40
25+85			2.76	98.35	94.28
25+80			4.07	97.04	94.24
25+73			4.64	96.47	94.21
25+71			3.24	97.87	94.20
25+00			4.71	96.40	93.70
24+00			5.76	95.35	93.00
23+00			5.79	95.32	92.80
22+00			4.64	96.47	92.60
○	4.88	101.35	4.64	96.47	
24+00			4.31	97.04	92.40
20+00			4.97	96.38	92.20
19+40			5.03	96.32	92.08
19+00			5.63	95.72	92.00
18+00			7.14	94.21	91.00
17+00			7.90	93.45	90.00
○	3.13	96.58	7.90	93.45	
16+00			4.22	92.36	89.00
15+00			5.71	90.87	88.00
14+00			6.43	90.15	87.00
13+00			7.30	89.28	86.00

Cut

Top of Stake Sta. 10+00

Spike in Tel. Pole #5102 E. side Rd. Sta. 10+50

3.06

4.12

4.36

4.07

2.80

2.26

3.67

2.70

2.35

2.52

3.87

4.64

4.18

2.24

2.72

2.21

2.45

2.36

2.87

2.15

2.86

Sta.	B.S.	H.I.	F.S.	Elev.	Grade	Cut
12+00		<u>96.58</u>	7.72	88.86	86.20	2.66
11+00			7.98	88.60	85.85	2.75
①	4.97	93.57	7.98	88.60		
10+00			5.81	87.76	85.41	2.35
9+00			6.30	87.27	84.97	2.30
8+00			6.47	87.10	84.53	2.57
7+00			6.91	86.66	83.89	2.77
6+00			7.62	85.95	83.44	2.51
5+00			7.70	85.87	83.00	2.87
①	2.55	88.42	7.70	85.87		
4+00			3.81	84.61	81.80	2.81
3+00			4.72	83.70	80.60	3.10
2+00			6.35	82.07	79.40	2.67
1+00			7.48	80.94	78.20	2.74
0+00			8.17	80.25	77.00	3.25
0-10			12.02	76.40	75.00	1.40

Sta.	B.S.	H.I.	F.S.	Elev.
------	------	------	------	-------

B.M.	1.75	898.86		897.11
------	------	--------	--	--------

0+00			12.82	
------	--	--	-------	--

1+00			12.22	
------	--	--	-------	--

2+00			11.70	
------	--	--	-------	--

3+00			11.90	
------	--	--	-------	--

4+00			11.98	
------	--	--	-------	--

5+00			11.84	
------	--	--	-------	--

6+00			11.67	
------	--	--	-------	--

①	5.04	899.39	4.51	894.35
---	------	--------	------	--------

7+00			12.16	
------	--	--	-------	--

8+00			12.07	
------	--	--	-------	--

9+00			12.00	
------	--	--	-------	--

10+00			11.85	
-------	--	--	-------	--

11+00			11.71	
-------	--	--	-------	--

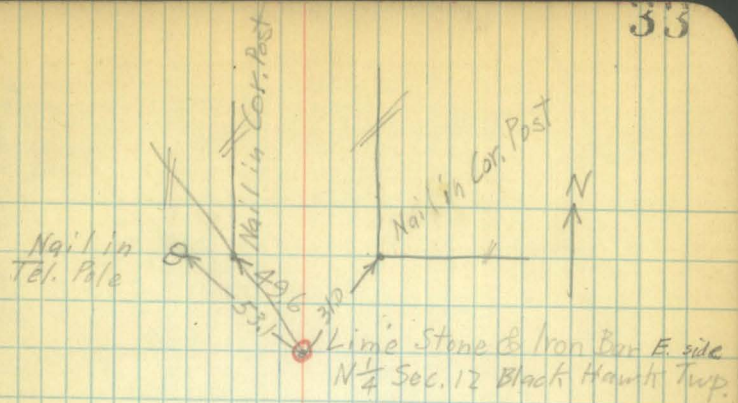
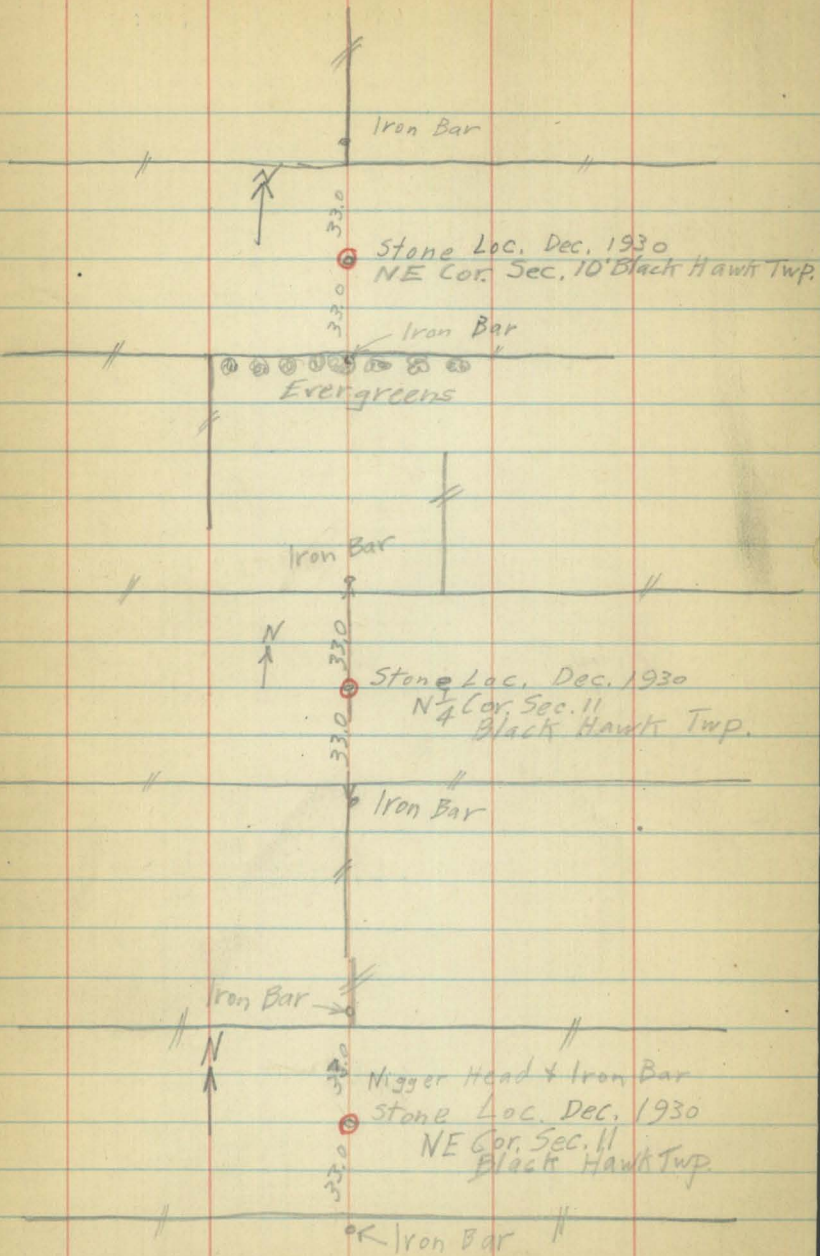
12+00			11.55	
-------	--	--	-------	--

13+00			11.42	
-------	--	--	-------	--

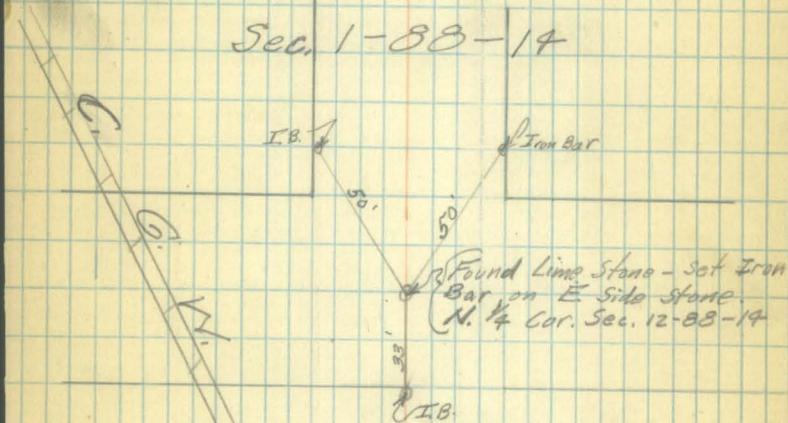
13+60			11.35	
-------	--	--	-------	--

B.M.			5.87	
------	--	--	------	--

① on S.E. Conc. Hdq. Conc. I-Beam Sta. 83+85

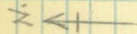


Sec. 1-88-14



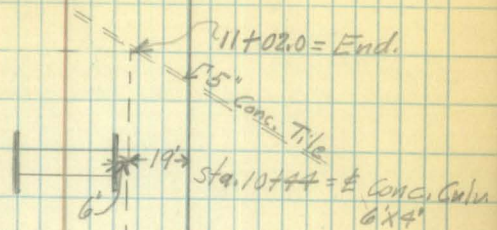
Sec. 12-88-14
Black Hawk Twp.

Sec. 6-90-11
Lester Twp.



Sec. 7-90-11
Lester Twp.

Note: - See Page #35 for Profile



Dec. 11th 1930E. B. Spencer - T
E. Schmidt - #
D. S. Butterfield - NotesTile Profile located between 35
Secs. 687-90-11 Lester Twp.

Sta.	B.S.	H.I.	F.S.	Elev	Grade	Cut.
B.M.	4.04	104.09		100.00		
Outlet			12.80	91.24 ✓		
1+00			10.75	93.29 ✓	91.24	2.05
0+30			7.90	96.14 ✓	92.50	3.64
1+00			5.98	98.06 ✓	94.35	3.71
1+44			4.00	100.04 ✓		
1+47	Drive to South		3.40	100.64 ✓		
1+63			3.10	100.94 ✓		
1+66			3.80	100.24 ✓		
2+00			3.99	100.05 ✓	94.55	5.50
3+00			2.33	101.71 ✓	94.75	6.96
4+00			1.53	102.51 ✓	94.95	7.56
5+00			1.50	102.54 ✓	95.15	7.39
①	1.11	103.65	1.50	102.54 ✓		0.20
6+00			2.09	101.56 ✓	95.35	6.21
7+00			3.57	100.08 ✓	95.55	4.53
8+00			4.76	98.89 ✓	95.75	3.14
9+00			5.00	98.65 ✓	95.95	2.70
10+00			4.33	99.32 ✓	96.15	3.17
10+44 = Fl. Culv.			6.26	97.39 ✓		
11+00			4.44	99.21 ✓	96.35	2.86
11+02 = End & Junction 5" Conc Tile						
Top of 5" Tile			6.80	96.85 ✓		

Blue @ on end of S.E. Wing Conc. T-Beam Sta. 0+20

Note: - See Page 34 for sketch.

	8.15	108.15	100.00	
0+00		11.75	96.40	+4.31
0+30		10.54	97.61	
1+00		8.72	99.43	
2+00		8.54	99.61	
3+00		8.40	99.75	
4+00		8.19	99.96	95.65
.			- 4.31	

95.65
 .79

 94.86

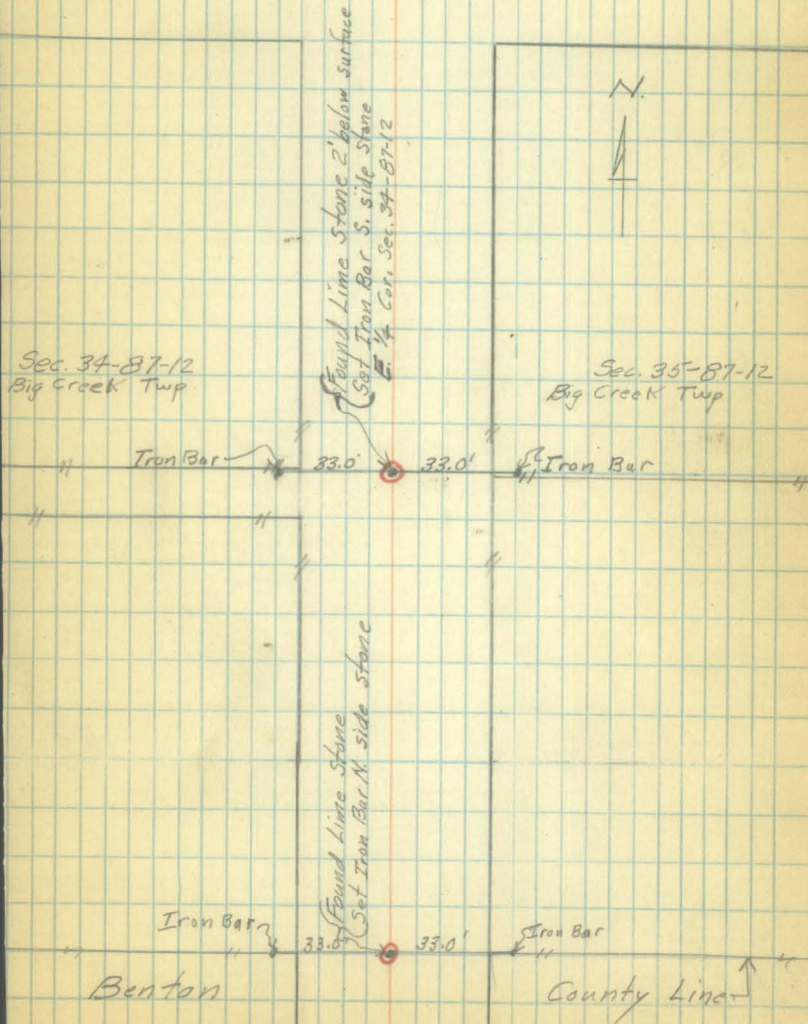
5	5.70	102.45	95.15	7.30
6	6.61	101.54	95.35	6.19
7	8.00	100.15	95.55	4.60

Sec. 27-87-12
Big Creek Twp.

Sec. 26-87-12
Big Creek Twp.

Sec. 34-87-12
Big Creek Twp.

Sec. 35-87-12
Big Creek Twp.

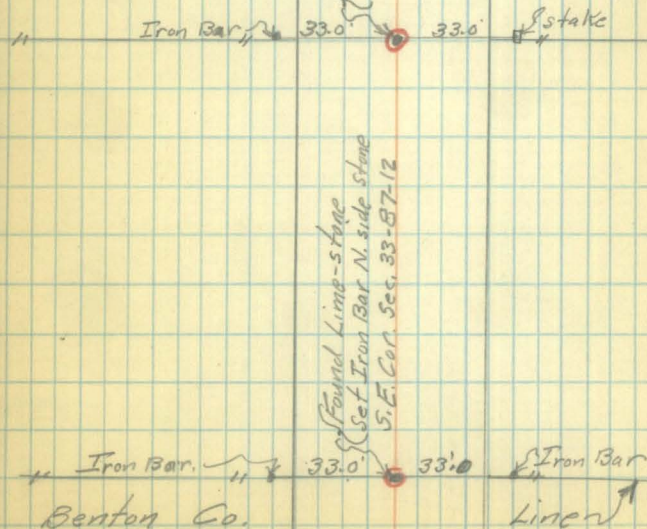


Sec. 28-87-12
Big Creek Twp.

Sec. 27-87-12
Big Creek Twp.

Sec. 33-87-12
Big Creek Twp.

Sec. 34-87-12
Big Creek Twp.



B.M. 0.48 100.48 100.00

Top of floor Elev. = 96.18

96.15

96.25
95.90
35

96.23
96.15

100.48
96.18
43.3
171

8

Top Cast-iron down-spout N.W. Cor. of Co. Jail

96.2
96.1

96.23

96.15
95.84
31

96.15
95.84
31

100.48
4.64
95.84

100.48
96.18
4.30

96.18
95.84
34

100.48
96.23
4.25

100.48
96.09
439

95.84
23
46.09

D.S.B. 40
E.N.W.
B.C.J.
4/30/31

Sec. 5-87-14

Sec. 4-87-14

Sec. 8-87-14
Lincoln Twp.

Sec. 9-87-14
Lincoln Twp.

Sec. 17-87-14

Sec. 16-87-14

D.S.B.
E.M.W.
B.C.J.

41

7/30/31

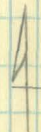
Sec. 18-87-12

Sec. 17-87-12

Sec. 19-87-12
Big Creek Twp.

Sec. 20-87-12
Big Creek Twp.

N.



Stake

33'

33'

Stake

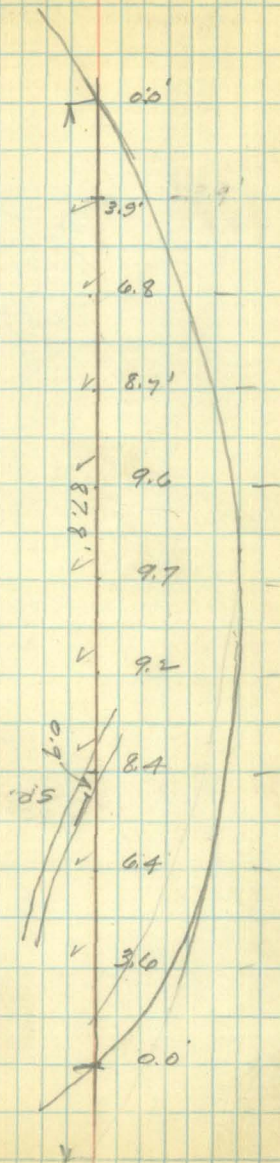
Found Niggerhead

Found stone

Sec. 30-87-12

Sec. 29-87-12

MEASUREMENTS TO



4.40	104.40		100.00	
137°50	4.35	99.87 ✓ 4.53 99.77 ✓ 4.63	4.70	35'
111°40	4.30	99.87 ✓ 4.53 99.74 ✓ 4.66 99.60 ✓	4.75	45'
91°30	4.43	4.80 99.40 ✓ 5.00 99.11 ✓ 5.24	5.18	75'
84°26	4.72	99.80 ✓ 5.60 99.19 ✓ 5.21	5.86	114'
83°20	4.65	99.94 ✓ 5.46 99.97 ✓ 5.43	5.78	113'
79°05	4.94	99.96 ✓ 5.44 99.02 ✓ 5.38	5.99	104'
73°14	4.94	99.10 ✓ 5.30 99.20 ✓ 5.20	5.94	100'
67°47	4.96	99.07 ✓ 5.33 99.22 ✓ 5.18	5.92	96'
61°49	4.93	99.30 ✓ 5.10 99.30 ✓ 5.10	5.87	94'
55°45	4.91	99.30 ✓ 5.10 99.30 ✓ 5.10	5.84	93'
50°0	4.84	99.30 ✓ 5.10 99.30 ✓ 5.10	5.79	94'
44°40	4.72	99.30 ✓ 5.10 99.30 ✓ 5.10	5.69	97'
39°50	4.66	99.30 ✓ 5.10 99.30 ✓ 5.10	5.65	99'
35°55	4.82	99.30 ✓ 5.10 99.30 ✓ 5.10	5.62	102'
30°40	4.57	99.30 ✓ 5.10 99.30 ✓ 5.10	5.64	107'

Top Rail

" "

" "

" "

" "

" "

" "

" "

Curb

" "

" "

" "

" "

" "

" "

" "

" "

" "

Top Rl

" "

Curb

Point of 30' R.

104.40

1	26°30	4.46	<u>99.40</u> ✓ 5.00	5.55	109'	Curb
2	20°10	4.31	<u>99.56</u> ✓ 4.84	5.40	109'	"
3	16°15	4.25	<u>99.63</u> ✓ 4.77	5.30	105'	"
4	13°22	4.33	<u>99.56</u> ✓ 4.84	5.35	102'	"
5	2°35	4.87	<u>99.17</u> ✓ 5.23	5.59	72'	"
6	357°0	4.99	<u>99.12</u> ✓ 5.29	5.59	60' ✓	"
	74°45	4.91	<u>99.47</u> 5.03	5.14	23' ✓	P.C. 36'R. CURVE
	81°08	4.83		5.23	40'	P.C. 36'R. "
7	343°27	5.11	<u>99.06</u> ✓ 5.34	5.57	46' ✓	Curb
8	334°55	4.97	<u>99.11</u> ✓ 5.29	5.59	62'	"
9	346°35	4.93	<u>99.10</u> ✓ 5.30	5.65	72' ✓	"
10	355°55	4.79	<u>99.17</u> ✓ 5.23	5.68	90'	"
	1°55	4.61	<u>99.21</u> 5.19	5.76	115' ✓	"
	718°05	5.05	<u>99.17</u> 5.23	5.42 ✓	37' ✓	"
	293°10	5.08	<u>99.13</u> 5.27	5.47 ✓	39' ✓	"
	251°40	4.75	<u>99.29</u> 5.11	5.47 ✓	72' ✓	"
	238°10	4.43	<u>99.38</u> 5.02	5.62 ✓	119' ✓	"
	232°40	4.09	<u>99.46</u> 4.94	5.80 ✓	171' ✓	"
	225°32	4.01	<u>99.67</u> 4.73	5.44	143' ✓	"
	233°15		<u>99.66</u> 4.74			"
	0°0		<u>99.61</u> 4.79			"
	27°10		<u>99.53</u> 4.87			"
	32°20		<u>99.28</u> 5.12			"
	34°45		<u>98.78</u> 5.67			"

Curb + P.C. 36'R. CURVE

Curb

N. R. L. T.

100'

104.90

36°00	448	98.88 ✓	209	5.52	6.57	
12°35	434	99.34 ✓	146	5.06	5.80	✓
15°00	402	99.50 ✓	176	4.90	5.78	✓
12°30	386	99.56 ✓	195	4.84	5.81	✓
66°47	489	98.95 ✓	113	5.45	6.02	✓
84°55	508	98.54 ✓	151	5.84	6.59	98.76 ✓
86°10	501	98.58 ✓	160	5.82	6.61	✓
87°00	504	98.51 ✓	169	5.80	6.73	✓
87°30	504	98.44 ✓	185	5.96	6.89	✓
87°55	516	98.68 ✓		6.32	7.49	233
88°10	510	97.90 ✓	280	6.50	7.90	
82°35	527	97.88 ✓	250	6.52	7.77	✓
81°45	510	98.35 ✓	190	6.65	7.00	
82°04	503	98.60 ✓	1	5.80	6.58	155
	153	98.38 ✓		6.02		
83°25	472	99.06 ✓		5.34	5.97	125
		98.78 ✓		5.62	72	
349°10	468	99.53 ✓		4.87	5.06	38
192°30	506	100.16 ✓		4.22	5.41	35
3°14	378	100.02 ✓		4.38	5.99	220
283°30	146				272	40

H. RI TR.

Curb

"

"

228' to E edge

Point 12" W. of Pt of slab

Curb

"

"

Pt at Junction of slab

"

"

Top N. RI

" N. RI

N. SW Pt.

S. " "

Top N. RI

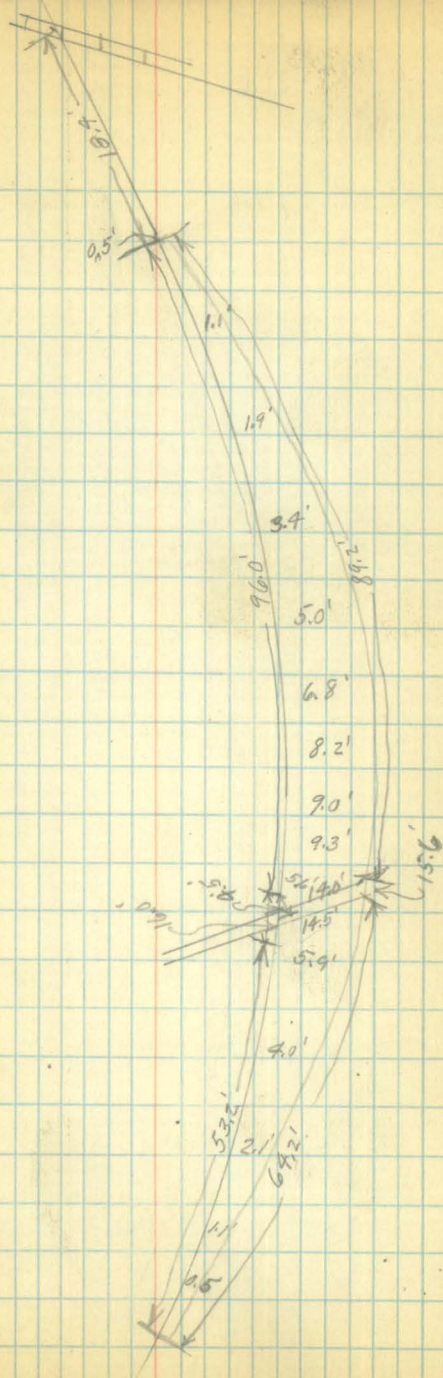
" S. RI

Top SW MH

" "

Curb

Hydr.



20.3 W of SE Cor.

	0°00	20.3		✓
	0°00	7.1'		✓
1	65°12	59.2'	C	✓
	"	59.7	B	✓
2	57°00	55.4	C	✓
	"	58.3	B	✓
3	47°25	51.0	C	✓
		58.8	B	✓
4	38°18	44.8	C	✓
		61.4	B	✓
5	29°17	37.3	C	✓
6	19°50	29.0	C	✓
7	11°15'	19.7	C	✓
8	2°45	10.0	C	✓
9	211°30	33.8	C [✓] Pt at	28.
10	262°40	17.9	C [✓] P.C.	
11	290°10	21.2	C [✓]	
12	299°50	30.1	C [✓]	
13	300°55	36.9	C [✓]	at tracks.
14	14°40	81.7	C [✓]	" "
15	70°0	72.7	B [✓]	
16	76°13	68.5	B	

1	33°45	63.5	B	✓	
2	42°25	59.9	B	✓	
3	295°35	45.9		C at ✓	TR
4	296°15	55.4	C	✓	
5	291°30	64.0	C	✓	
6	286°0	71.5	C	✓	
7	279°45	78.0	C	PC. ✓	0.6' at Rt. L
8	302°10	68.4	B	✓	
9	318°43	70.1	B	✓	
10	332°45	78.4	B	✓	
11	343°07	91.3	B	✓	
12	348°10	96.7	B	✓	
13	353°47	99.7	B	✓	
14	359°30	98.8	B	✓	
15	5°05	95.7	B	✓	
16	10°0	89.7	B	@ 140' ✓	from PC
17	10°45	88.7	B	✓ 141.6	at tracks
18	26°0	89.9	C	✓ at PC	0.6 at CS.
19	31°40	85.0	C	✓	
20	38°05	81.6	C	✓	
21	45°08	80.0	C	✓	
22	52°15	80.1	C	✓	
23	59°10	87.1	C	✓	

1	65°32	85.8	C
2	71°05	90.9	C
3	75°40	97.5	C
4	79°30	105.0	C
5	81°35	109.7	pt. at Tr.
6	82°15	95.9	" " "
7	78°30	88.9	B
8	73°20	82.5	B
9	66°55	78.0	B
10	59°45	75.5	B
11	52°06	75.1	B
12	44°35	76.6	B
13	37°40	79.7	B
14	31°15	83.7	B
15	25°50		P.C.
16	86°19	109.6	B at Tr.
17	85°30	124.0	C " "
18	87°05		C + 10
19	88°15		C + 10
20	89°08		C + 10
21	89°35		C + 10
22	89°45		C + 10
23	89°50	105.7'	P.C.

9.2 to pt

90°05 10' back from P.C.

89°55 10'

89°50 10'

89°35 10'

88°45 10

87°10 10

86°17 4' P.C.

Truck No 25

Lic. No. 7-1790 $\frac{14}{25}$

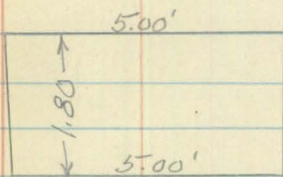
Earl Leper. 2.13 Cu. yds.

Ford B.B

Truck No. 14

Lic. No. 7-496 $\frac{14}{25}$

John Nightengale Ford V-8



Length 6.15 = 2.05 Cu. yds

Truck No. 40

Lic. No. Official 852. - Dodge

Cy. Young 2.10 Cu. yds

Truck No 16

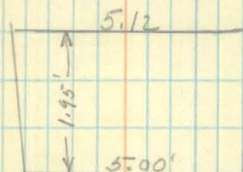
Lic. No Official 851 - Dodge

"Slim" Demire 2.10 Cu. yds.

Truck No 2

Lic. No. 7-1053

Geo. Wallace - Ford V-8

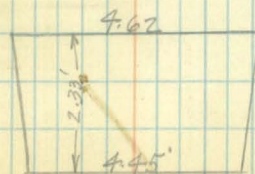


Length 7.18 = 2.62

Truck No. 7

Lic. No. 7-1866 Ford V-8

Bob Dickson



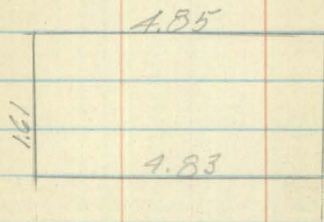
Length = 6.65 2.60 Cu. yds.

Truck NO 3

Lic NO 57-2554 $\frac{19}{30}$

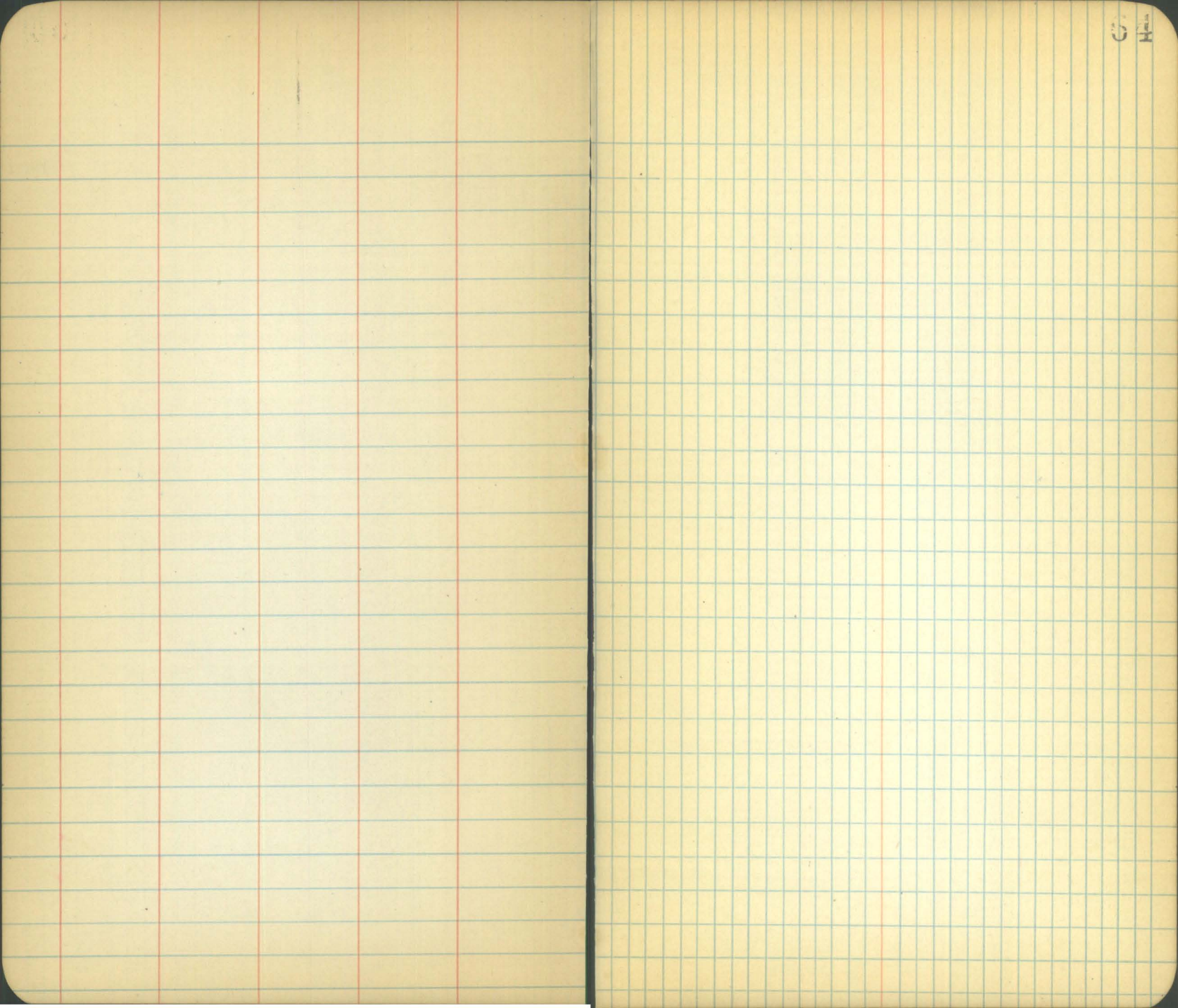
V. H Weibel

Chev



Length 6.07

1.77 gds -





$$\begin{array}{r}
 1.54 \\
 35 \\
 \hline
 770 \\
 462 \\
 \hline
 53.90
 \end{array}$$



7.0 long.

$$\begin{array}{r}
 1.53 \\
 35 \\
 \hline
 815 \\
 489 \\
 \hline
 27 \overline{) 57.05}
 \end{array}$$

104.06

10.12

9.38

.74

$$\begin{array}{r} 5.00 \\ 1.80 \\ \hline 70000 \\ 500 \\ \hline 9.0000 \end{array}$$

16

33

$$\begin{array}{r} 104.06 \\ 99.46 \\ \hline 4.60 \end{array}$$

99.74

28

99.46

28

99.18

104.06

99.74

4.32

6.15

9.00

55.35.00

104.06

99.18

4.88

20.5

27 55.35

54

135

5

