

FIELD BOOK

361

49

KEUFFEL & ESSER CO.

DRAWING MATERIALS

AND

SURVEYING INSTRUMENTS.

NEW YORK.

CHICAGO. ST. LOUIS. SAN FRANCISCO. MONTREAL.

TABLES FOR EXCAVATIONS AND EMBANKMENTS.

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

ROADWAY 18 FEET WIDE. SIDE SLOPES 1 to 1.

FOR SINGLE TRACK EXCAVATION.

"Copyright, 1895, by Keuffel & Esser Co."

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	0
1	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	1
2	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	2
3	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	3
4	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	4
5	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	5
6	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	6
7	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	7
8	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	8
9	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	9
10	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	10
11	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	11
12	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	12
13	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	13
14	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	14
15	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	15
16	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	16
17	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	17
18	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	18
19	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	19
20	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	20
21	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	21
22	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	22
23	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	23
24	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	24
25	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	25
26	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	26
27	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	27
28	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	28
29	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	29
30	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	30
31	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	31
32	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	32
33	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	33
34	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	34
35	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	35
36	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	36

Calculated by Julien A. Hall, M. Am. Soc. C. E.

For Keith's Railroad Curve Tables see end of book.

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IF Lost Please
Return to
County Engr. Office
Court House
Waterloo, Iowa
Black Hawk Co.

BLACK HAWK COUNTY
ENGINEER'S OFFICE
COURT HOUSE
WATERLOO, IOWA 50703

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WATERLOO, IOWA 50703
COURT HOUSE
ENGINEER'S OFFICE
BLACK HAWK COUNTY

CROSS-SECTION KROG Pit Elev.

Base line 327' South of
North line of Sec. 27-89-14
and parallel thereto

June 13, 1924
Spencer
Tarbell
Bown

B.M. 5.25 106.08

Nail in Cor. Post at S-E Cor. new pit

3+05 Corner Post at SE cor.

3+00

2+50

2+00

1+60

1+00

0+60

0+00 S-W cor. of Pit on East side of Rd.

B.M.

11.33

111.33

100.00

$\begin{array}{r} 105.6 \\ 5.7 \\ \hline 0 \end{array}$	$\begin{array}{r} 111.0 \\ 0.3 \\ \hline 69 \end{array}$	$\begin{array}{r} 112.0 \\ 0.7 \\ \hline 75 \end{array}$
$\begin{array}{r} 104.9 \\ 6.4 \\ \hline 0 \end{array}$	$\begin{array}{r} 110.4 \\ 0.9 \\ \hline 75 \end{array}$	
$\begin{array}{r} 103.9 \\ 7.4 \\ \hline 0 \end{array}$	$\begin{array}{r} 107.1 \\ 4.2 \\ \hline 45 \end{array}$	$\begin{array}{r} 109.6 \\ 1.7 \\ \hline 75 \end{array}$
$\begin{array}{r} 102.9 \\ 8.4 \\ \hline 0 \end{array}$	$\begin{array}{r} 104.9 \\ 6.4 \\ \hline 36 \end{array}$	$\begin{array}{r} 109.3 \\ 2.0 \\ \hline 88 \end{array}$
$\begin{array}{r} 101.5 \\ 9.8 \\ \hline 0 \end{array}$	$\begin{array}{r} 102.8 \\ 8.5 \\ \hline 34 \end{array}$	$\begin{array}{r} 106.4 \\ 4.9 \\ \hline 84 \end{array}$
$\begin{array}{r} 99.6 \\ 11.7 \\ \hline 0 \end{array}$	$\begin{array}{r} 100.7 \\ 10.6 \\ \hline 13 \end{array}$	$\begin{array}{r} 103.0 \\ 8.3 \\ \hline 75 \end{array}$
$\begin{array}{r} 99.6 \\ 11.7 \\ \hline 0 \end{array}$	$\begin{array}{r} 100.9 \\ 10.8 \\ \hline 50 \end{array}$	$\begin{array}{r} 102.4 \\ 8.9 \\ \hline 54 \end{array}$
		$\begin{array}{r} 100.4 \\ 10.9 \\ \hline 58 \end{array}$
		$\begin{array}{r} 101.9 \\ 9.4 \\ \hline 75 \end{array}$

111.3

Nail in post at S-W cor. of new pit

KROG PIT

June 13, 1924

Base Line 341.5 ft East
of $\frac{1}{2}$ of Highway
and parallel thereto.

N.E.
Cor. of
Pit

$$\left\{ \begin{array}{l} 52 \times 52 \times 22 = \frac{5944}{27} = 220 \\ 40 \times 75 \times 8.0 = \frac{24000}{27} = 889 \end{array} \right.$$

11 09

2+63 N.E. Cor. post

2+47

2+25

5.65 123.14 1.73 117.49

1+75

1+25

B 0+80

B 0+00 = SE Cor. of Pit

B.M.

13.14

119.22

106.08

Stripping Around Trap 20

North section $\frac{73 \times 102 \times 2.5}{27} = \frac{18615}{27} = 689, 220, 889$

Stripping Est. #2 = 1818 Cu yds.
Est. #1 = 1231 Cu yds.
Est. #3 = 3414 Cu yds.

$$\begin{array}{r} 115.7 \\ 3.5 \\ \hline 0 \end{array} \quad \begin{array}{r} 114.9 \\ 4.3 \\ \hline 75 \end{array} \quad \begin{array}{r} 109.0 \\ 10.2 \\ \hline 70 \end{array}$$

$$\begin{array}{r} 115.1 \\ 4.1 \\ \hline 0 \end{array} \quad \begin{array}{r} 114.8 \\ 4.4 \\ \hline 49 \end{array} \quad \begin{array}{r} 109.9 \\ 9.3 \\ \hline 67 \end{array}$$

$$\begin{array}{r} 114.5 \\ 4.7 \\ \hline 0 \end{array} \quad \begin{array}{r} 114.4 \\ 4.8 \\ \hline 56 \end{array} \quad \begin{array}{r} 115.7 \\ 3.5 \\ \hline 55 \end{array}$$

$$\begin{array}{r} 117.0 \\ 2.2 \\ \hline 0 \end{array} \quad \begin{array}{r} 117.0 \\ 2.2 \\ \hline 5 \end{array} \quad \begin{array}{r} 109.9 \\ 9.3 \\ \hline 67 \end{array}$$

$$\begin{array}{r} 115.1 \\ 4.1 \\ \hline 0 \end{array} \quad \begin{array}{r} 112.3 \\ 6.9 \\ \hline 4 \end{array} \quad \begin{array}{r} 109.6 \\ 9.6 \\ \hline 60 \end{array}$$

$$\begin{array}{r} 109 \\ 8.3 \\ \hline 0 \end{array} \quad \begin{array}{r} 107.1 \\ 12.1 \\ \hline 46 \end{array} \quad \begin{array}{r} 102.2 \\ 17.0 \\ \hline 56 \end{array}$$

119.2

Nail in Cor. post at SE cor. of new pit

(See also next page)

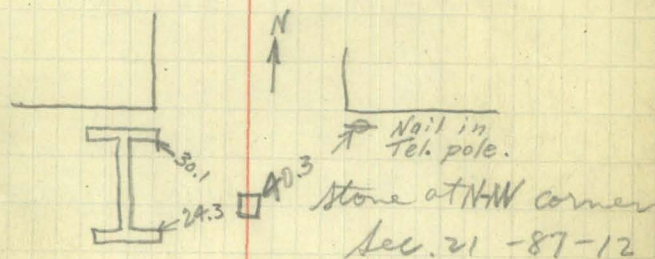
Krog Gravel Pit. Sec 27 Cedar Falls

June 24, 1924

Found stone at N-W corner of
Sec. 21 - 87N-R12W, described as follows:
- Wedge shaped lime stone with
point down, about 15" X 15" in
size and 6" wide at top.

Also found stone at West $\frac{1}{4}$ corner
and chained distance to
NW corner = 2642.2 feet.

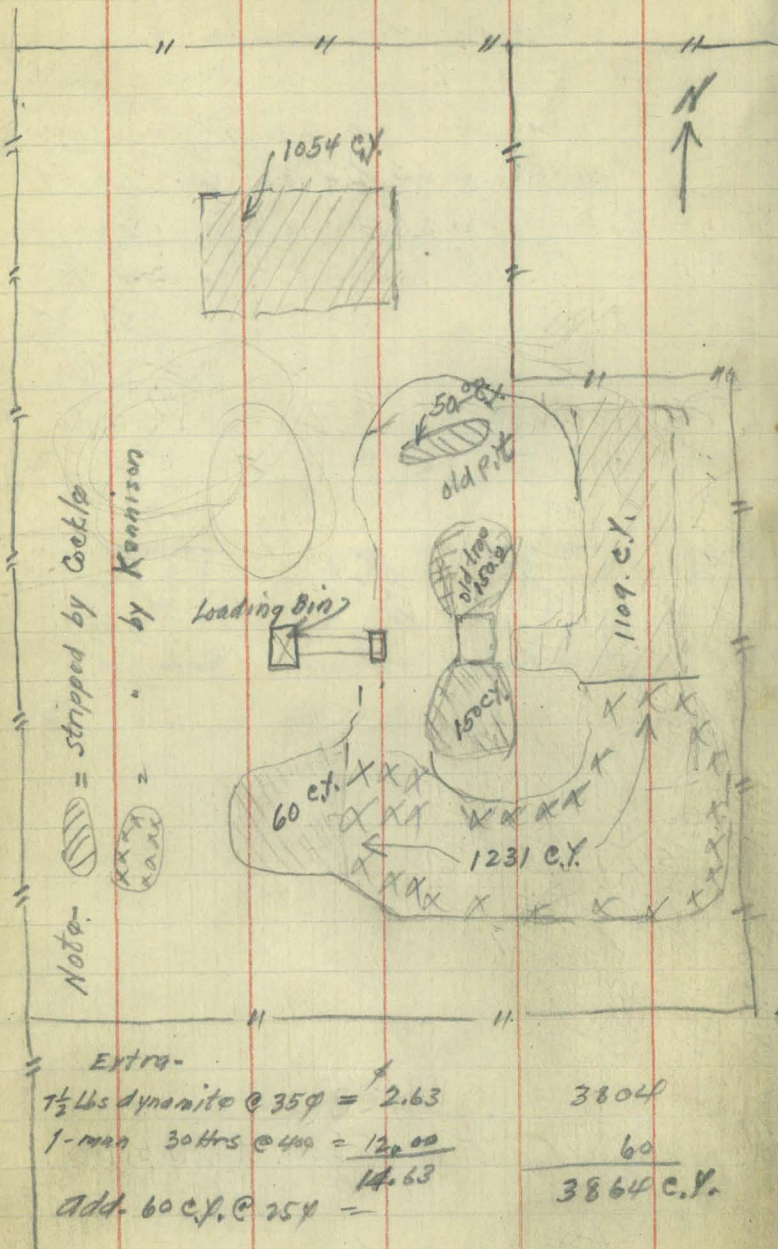
E.B. Spencer
I.P. Wilde



- 1109 cy.
300
1054
170
2633 cy. by Corle
1731 cy. by Kennison
3864 cy.

2642.2 feet
to $\frac{1}{4}$ corner

Public Road.



Sec 30 Big Creek Twp.

T87N-R11W

About 100' S. of SE Cor. NW $\frac{1}{4}$
of NW $\frac{1}{4}$

16.7' b. to b. of old culv.

No Floor under culv.

$4\frac{1}{2} \times 2\frac{1}{2}$ opening

6		4.7	101.0
5		5.0	100.7
4		5.5	100.2
3 + 00	E Culv.	3.8	101.9
2		4.3	101.4
1		4.0	101.7
0	-3.00' south	4.2	101.5

B.M. 5.72 105.72 100.00

June 25, 1924.

West

7.8	6.9	7.0	7.45	9.07	11.29	10.20	101.7	102.7	103.0	99.0	99.2	7.0	7.3	7.9
350	200	100	200	17	9	8	3.8	8	8	9	19	100	200	300

East

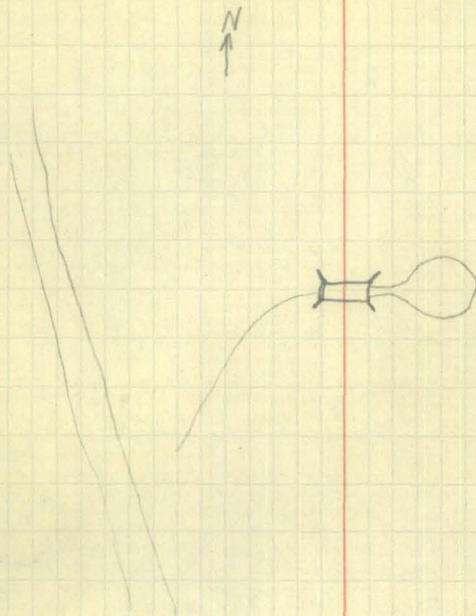
Nail in Tel. pole N. and W. of Culv.

June 25, 1924.

Sec. 30, Big Creek Twp.
 About 500' N. of SE cor. of
 NW $\frac{1}{4}$ of NW $\frac{1}{4}$ Sec. 30 - 87-11
 4' x 3 X 17.3
 Conc. Floor

12	- 222' N. of Culu.	5.6	99.3
11		5.4	99.5
10		4.8	100.1
9+78	& Culu.	4.00	100.9
9+00		5.00	99.9
8+00		4.5	100.4
7+00		3.9	101.00

B.M. 1.5 104.9 3.32 102.40
 105.72



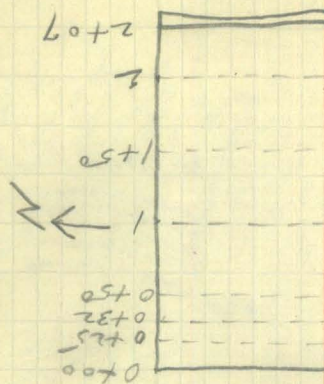
East

$\frac{7.8}{400}$ $\frac{7.5}{300}$ $\frac{6.2}{200}$ $\frac{5.25}{100}$ $\frac{7.3}{25}$ $\frac{7.4}{9}$ $\frac{3.9}{8}$ 40 $\frac{3.8}{8}$ $\frac{2.9}{9}$ $\frac{7.5}{9}$ $\frac{8.3}{25}$
 $\frac{6.7}{200}$ $\frac{7.0}{150}$ $\frac{7.2}{100}$

Nail in Tel. pole West side road, 4th. pole S. of Culu.

W.C. Brandhorst Pit
Preliminary X-Sec.

June 10, 1924
Spencer
Tarbell



2+07 N-E Cor. of Pit

2+00

1+50

1+00

0+50

0+32

0+25

0+00

N-W Cor. of PIT

B.M.

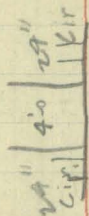
3.75 103.75

100.00

96.0 7.8 0	95.8 8.0 50	95.8 8.0 74		
98.0 5.8 0	98.6 5.2 59			
99.0 4.8 0	99.8 4.0 43	99.3 4.3 50.7	93.2 10.6 166	91.2 12.6 184
98.1 3.7 0	98.3 5.3 50.7	92.3 11.5 114	98.8 15.0 177	92.7 11.1 130
97.3 6.5 0	97.3 6.7 50	92.9 8.9 100	92.2 11.6 130	92.7 11.1 130
97.2 6.6 0	96.9 6.9 50	92.7 11.1 100	90.3 13.5 130	92.7 11.1 130
96.2 7.6 0	96.0 8.8 50	92.7 11.1 100	90.3 13.5 130	92.7 11.1 130

Vail in Cor. post at Middle of North Line

Skew Box Culvert
Sta. 55+11 ± 7x5x26 - 30° Skew



4'-2" Height
2'-0" H. of Arch

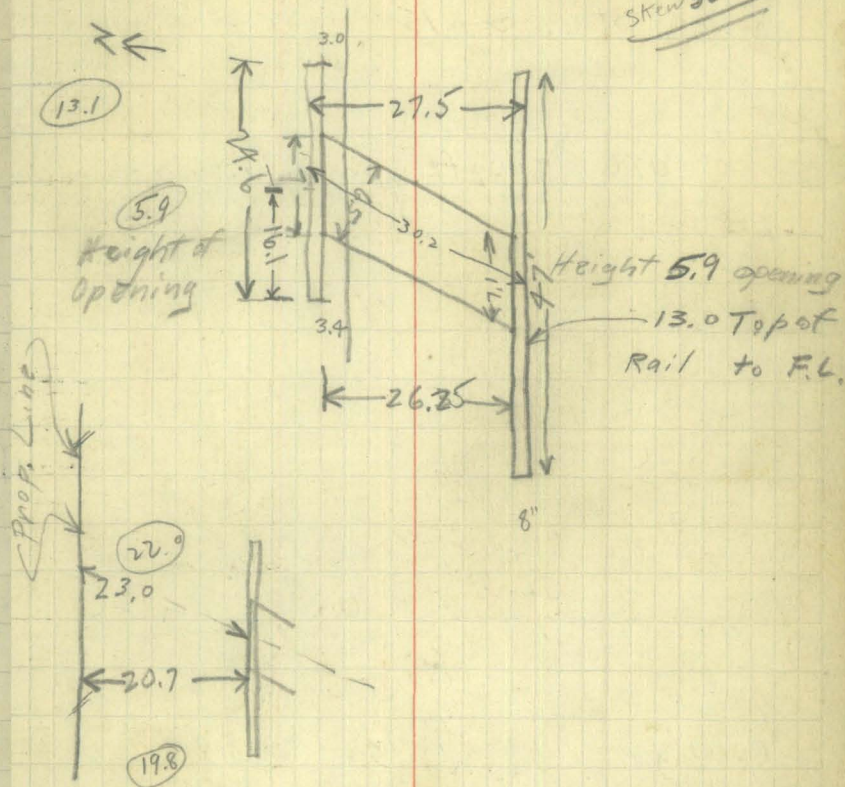
Edge of walk to be 2' from
property line
Side Walk grade = 854.94

Top of Walk Fill East	3.5	854.27
" " " West	3.0	854.77

B.M. 0.73 857.77 857.04

Rainbow Drive

Skew 30°



857.06
S. Hd. wall
0.71
13.4

856.96
N. Hd. wall
0.81
13.4
854.64
3.13
Paving

846.0
43.86
11.8
13.7 Floor
F.L. Present
13.1

E. end S Headwall

F.L. McGIN

Skew Box

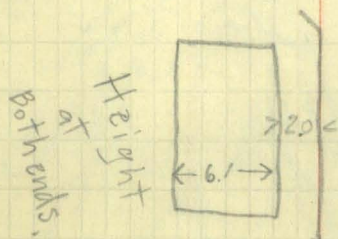
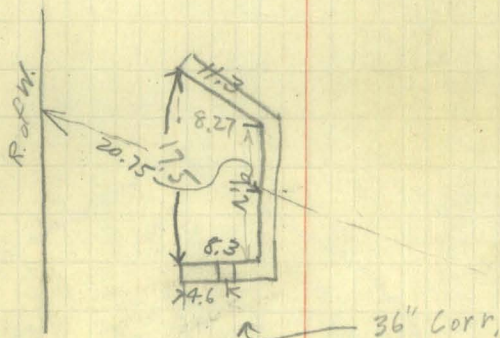
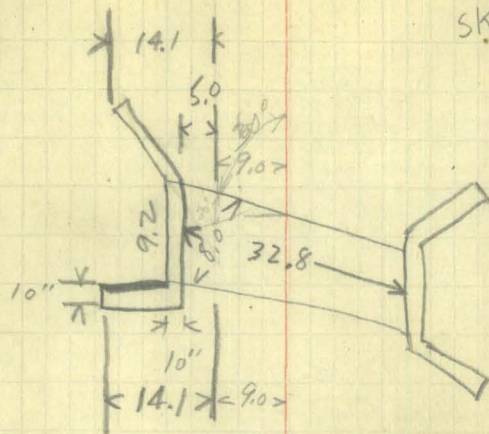
9.2 X 6.1 X 28'

Sta. 102 + 15

8 X 6 = 48 sq. ft. opening

Rainbow Drive.

Skew 30°



Center of South Head wall
E paving at 102 + 22

Driveway	5.0	863.8
F.L. at S. end Culv.	13.2	855.6
Top of Fill East	4.6	864.2
100' down Stream	13.6	855.2
F.L. at R. of W. Line	13.1	855.7
F.L. at N. end	13.2	855.6
Center N. Hd wall	5.45	863.36
B.M.	5.16	863.66
		864.29

x.5v

868.81

Krog Pit

1+25

0+80

0+39

0+34

2+66

Natural Gr.

2+50

2+00

1+50

1+00

0+50

B.M.

10.9

110.9

10000

3.3
x 2 4 7 17 32 44

107.7 107.1 107.3 106.2 107.4
3.2 3.8 3.6 4.7 3.5
15 39 45 50

108.8 108.8 105.7 103.8 105.0 105.7
2.1 2.1 5.2 2.1 5.9 5.2
0 9 20 36 45 53

108.3 108.0 104.4
2.6 2.9 6.5
12 38 42

105.1 102.0 100.9 102.2 104.6 106.6 107.3 102.0
5.8 8.9 10.0 8.7 6.3 4.3 3.6 8.9
7 18 23 28 36 59 76 85

104.9 103.9 102.1 102.6 105.1 106.0 106.2 104.0 103.9 105.1
6.0 7.0 8.8 8.3 5.8 4.9 4.7 6.9 7.0 5.8
13 27 38 49 59 66 77 81 91 104

104.9 104.0 103.1 103.0 104.8 106.7 109.7
6.0 6.9 7.8 7.9 6.1 4.2 1.2
31 44 46 50 71 84 91

103.0 101.8 102.0 103.5 105.0 106.6
7.9 9.1 8.9 7.4 5.9 4.3
43 52 59 63 82 85

99.6 102.2 102.2 103.0 102.8
11.3 8.7 8.7 7.9 8.1
0 43 53 64 71

Post S-W Cor. of Pit

July 19/924

Final CROSS-SECTION

Co. Road thru Fox Twp

July 28, 1924

B.M. #3
11
10
9
8
7
6
5
4
3
2

B.M. #3

4.05

895.03

3.16

890.74

890.98

3.91

894.10

5.91

890.19

1+60

Starting point of project

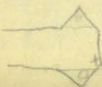
B.M. #2

2.95

896.10

893.15

V-W Cor. of end of cement walk to parsonage



87.1	88.0	89.4	88.6	89.5	88.4	88.7	88.4	88.0	88.0
7.9	7.0	5.6	5.4	5.3	6.6	6.3	6.6	7.0	5.0
19	16	12	12	16	17	19	25	28	30
86.2	88.1	89.2	88.5	89.6	88.2	87.6	87.4	88.8	
8.1	6.9	5.8	5.5	5.4	6.1	7.4	7.5	6.2	
19	15	12	11	11	14	20	28	30	
86.6	88.2	89.2	89.7	89.6	87.1	87.0	88.5		
7.5	5.9	4.9	4.4	4.5	7.0	7.1	5.6		
20	16	12	11	11	18	28	30		
86.4	86.0	86.7	88.8	89.7	87.8	88.0	87.0	89.4	
7.7	6.1	7.4	5.3	4.7	6.3	6.1	7.1	4.7	
26	25	19	14	12	16	21	28	31	
86.2	85.6	85.9	88.8	89.1	89.1	88.0	87.2	89.1	
7.9	8.5	8.2	5.3	5.0	5.0	6.1	6.9	5.0	
27	26	22	13	12	15	27	31		
86.6	86.1	86.1	87.4	88.2	88.7	87.6	87.4	89.5	
7.5	8.0	8.0	6.7	5.2	5.4	6.5	6.7	4.6	
27	26	24	17	13	12	15	27	31	
88.8	87.6	87.5	88.1	89.3	89.6	88.6	88.7	88.4	91.2
5.3	6.3	6.6	6.0	4.8	4.5	5.5	5.4	5.7	2.9
27	25	22	17	12	12	16	18	25	29
90.1	88.8	88.7	89.0	90.3	89.3	89.7	89.4	92.6	
6.0	7.3	7.4	7.1	5.9	5.8	6.8	6.4	6.6	3.5
27	24	21	15	12	12	16	18	25	29
89.1	88.2	88.8	90.6	90.9	90.6	89.5	89.8	89.5	91.9
7.0	7.9	7.3	5.5	5.2	5.5	6.6	6.3	6.6	4.2
26	24	16	11	12	12	16	19	26	29
90.0	88.8	88.7	91.1	89.2	91.0	90.4	89.0	92.2	
6.1	7.3	7.4	5.0	4.9	5.1	5.7	6.2	3.9	
26	23	19	12	11	11	14	22	26	

0 section

12

915.05

904.02

894.26

895.03

Handwritten mathematical calculations on a grid background, showing various arithmetic operations (addition, subtraction, multiplication, division) and results. The calculations are organized into rows and columns, often with multiple steps or intermediate results. Some calculations are circled or underlined, indicating specific results or steps. The numbers are written in a cursive, handwritten style.

B.M. #5 Sta. 41+46 4 in Center of
E. Headwall Culv. Elev. 901.14

14

42

41+50

B.M. #5 6.92 908.06 7.92 901.20 corr. 901.14

41

40

39

38

37+50

37

T.P. 0.62 909.12 11.14 908.50

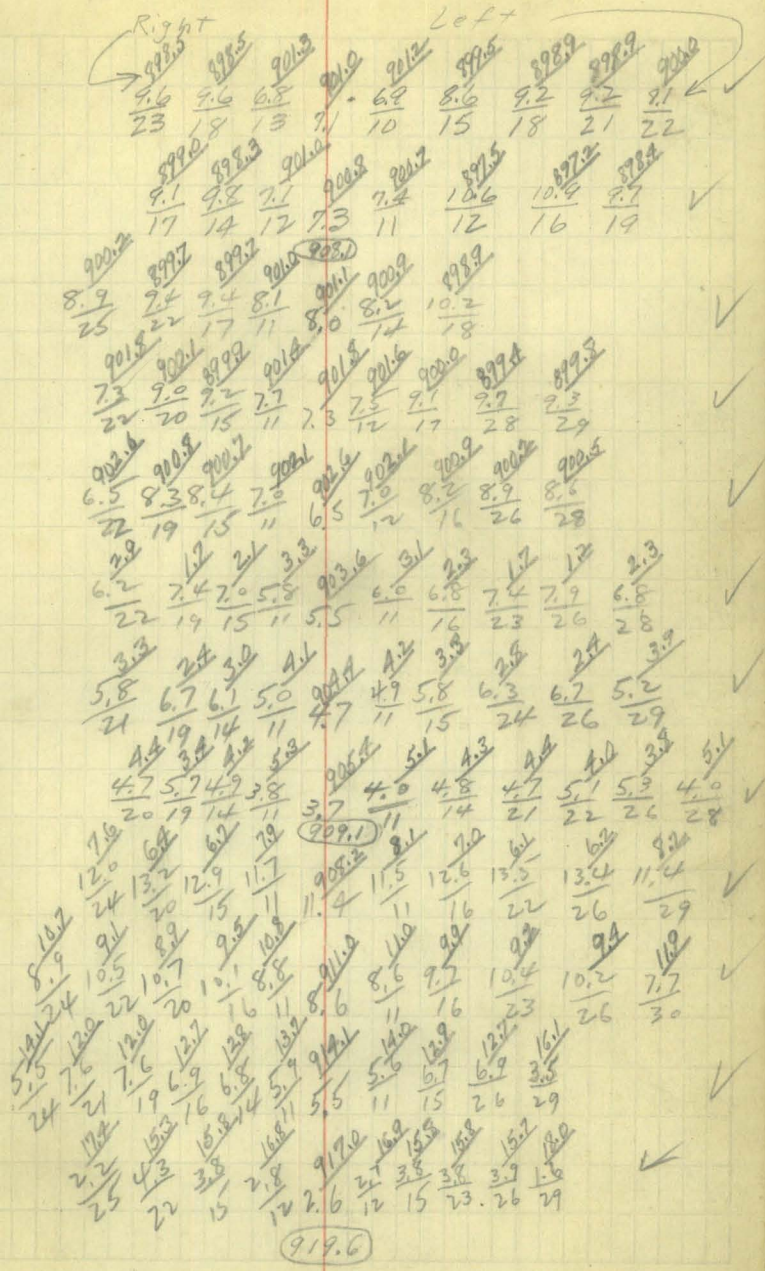
36

35

34

33

0.45 919.64 10.88 919.19



50

49

48 + 50

48

47

T. P.

0.73

898.89

990

898.16

46

45 + 50

45

 $44 + 50$

44

43 + 50

43

908.06

(Handwritten arithmetic problems arranged in columns, showing various divisions and remainders.)

59
T.P. 9.77 (921.96) 2.50 912.19

58

57

56
T.P. 10.5 (914.69) 2.82 904.10

55

54

53

52+65

52+55

52+23

B.M. 6.69 (906.92) 6.69 900.15 900.23

52

T.P. 11.79 (906.84) 3.84 895.05

51

898.89

B.M. 579.52+09 Spike in N.E. Cor.
old Jubilee Blacksmith Shop x roads.
Clas. 900.23 16

16.9 13.2 13.6 14.2 15.1 15.0 13.3 13.5 16.2
5.1 8.8 8.4 7.1 9.15.1 7.0 8.7 8.5 5.8
25 20 16 12 6.9 13 18 21 25
13.1 10.1 11.3 11.8 922.0 11.6 10.4 10.4 12.9
1.6 4.6 4.4 2.5 919.9 3.1 4.3 4.6 1.8
25 21 16 12 2.8 12 16 21 24
907.2 906.7 904.9 903.3 908.8 909.3 907.2 906.2 908.0
5.5 8.0 7.8 6.4 908.8 6.4 7.5 7.8 5.7
26 22 17 13 5.9 13 16 22 24
905.2 904.7 904.7 904.2 906.5 906.0 904.8 904.4 905.3
8.8 10.0 10.0 8.5 906.5 906.0 904.8 904.4 905.3
26 23 17 13 8.2 12 16 22 24
904.8 903.2 903.2 903.0 905.2 904.5 903.2 903.2 903.1
2.1 3.7 3.2 1.9 905.2 2.4 3.7 4.2 3.8
26 23 16 12 17 12 16 25 25
905.0 902.4 902.9 901.1 904.3 903.2 901.5 901.8 902.9
1.9 4.5 4.0 2.8 904.3 3.2 4.4 5.1 4.0
25 22 17 13 2.6 12 16 23 25
903.7 902.0 902.4 902.0 901.7 901.0 900.3 902.9
3.2 4.9 4.5 902.0 5.2 5.9 6.6 4.0
22 19 13 9.9 12 16 22 25
901.5 902.9 901.3 901.0 900.0 900.0 901.1
5.4 6.0 5.6 901.3 5.9 6.9 6.9 5.5
24 19 14 5.6 12 18 22 25
900.6 900.6 901.1 901.1 900.6 900.8 901.3
6.3 6.3 5.8 901.1 6.3 6.1 5.6
26 22 14 5.8 14 23 24
91.2 95.6 97.8 99.9 99.8 99.3 98.1 99.0 99.4
8.2 8.9 9.0 2.0 99.8 7.1 8.8 2.9 7.5
27 22 18 15 7.0 13 20 24 28
99.6 99.2 97.3 96.0 99.1 99.0 98.0 97.1 97.5
8.2 9.8 9.2 8.8 99.1 7.8 8.8 9.7 9.3
26 21 16 11 7.7 12 16 21 24 26
901.1 901.7 901.6 903.3 906.0 906.3 905.9 904.4 904.3 905.3
3.8 4.2 4.3 2.6 906.3 3.0 4.5 4.6 3.0
21 19 16 11 2.6 14 20 23 26
999.9

68

T.P.

-0.34

904.70

12.36

904.36

67

66

65

64+50

2.46

916.72

7.70

914.26

64

63

62

61

60+50

60

59+50

921.96

Handwritten calculations and numbers, including a large grid of numbers and several circled totals (904.70, 916.72, 921.96, 922.0).

904.70

916.72

921.96

922.0

B.M. Sta. 13+16 Spikes in Willow 18
 Stump Left. Elev. 892.57

 $77 + 50$

77

 $76 + 50$

76

 $75 + 50$

75

74
Center Culvert
East Headwall

73

72

71

70

69

759

900.74

11.55

893,15

904.70

89
B.M. 4.59 894.65 4.59 890.10 890.06

88

87

86

85

T.P. 5.31 894.69 6.80 889.38

84

83

82

81

80
B.M. 2.86 896.18 1.39 893.35 corr.
79 893.32

78

900.74

N. Sta. 79. Highest point on Boulder
Elev. 893.32 19

878 869 872 89.3 89.5 89.2 861
6.8 7.7 7.4 5.3 5.1 5.4 8.5
21 20 19 15 13 20
873 862 866 894.6 893 862
7.4 8.5 8.1 5.2 5.4 8.5 8.5 7.4
27 25 18 13 13 19 25 27
861 864 865 871 875 89.5 89.9 89.5 862 864 873
6.6 8.3 8.2 7.6 7.2 5.2 5.2 7.8 8.3 7.3
27 24 19 18 16 12 12 16 26 27
894 872 890 90.0 90.1 89.5 872 872 88.7
5.3 7.5 6.7 4.7 4.6 5.2 7.0 7.5 6.0
27 23 17 13 11 15 24 28
891 874 878 89.9 89.0 89.5 872 872 88.7
5.6 7.1 6.9 4.8 4.7 4.9 6.8 7.7 6.4
28 26 17 13 11 16 25 28
893 876 874 89.7 89.7 89.9 872 872 88.7
7.0 8.6 8.1 6.5 6.4 8.3 9.3 8.0
28 26 17 13 12 16 25 26
892 898 899 904 89.4 901 88.6 872 872
6.5 7.4 7.3 5.8 5.8 6.1 7.6 8.7 7.5
26 24 17 12 12 16 23 26
913 889 894 910 891 902 872 883 893
4.9 7.3 6.8 5.2 5.2 5.5 7.4 7.9 6.9
22 20 15 11 12 17 23 24
918 895 900 912 891 912 896 892 903
4.4 6.7 6.2 4.6 5.2 5.2 6.6 7.0 5.9
22 20 15 11 12 16 20 22
923 899 898 913 891 918 892 896 908
3.9 6.3 6.3 4.4 4.4 4.4 6.4 6.6 5.4
23 21 12 12 11 16 20 22
893 890 890 892 892 892 892 892 892
7.5 10.0 7.9 9.4 8.0 8.0 9.4 9.8 8.8
24 20 17 15 12 12 15 20 22
895 892 892 892 892 892 892 892 892
5.1 1.4 8.2 8.2 8.2 8.2 8.2 8.2 8.2
27 23 16 12 11 17 21 23
900.7

100

99

98

97

96

95

 $94 + 50$

94

93

92

T. P.

91

90

8.12

903.18

2.73

895.06

7.55

897.79

K. 41

890.24

894.65

Handwritten calculations on lined paper, showing a grid of numbers and results, likely a multiplication table or a series of small divisions. The numbers are written in a cursive, handwritten style. The grid is organized into rows and columns, with some numbers appearing to be products or quotients of the numbers in the adjacent rows and columns. The calculations are dense and cover most of the page.

108

T.P.

11.75

(922.29)

1.71

910.54

107

106

105+55

105+50

105+34

105+19

B.M.

105

104

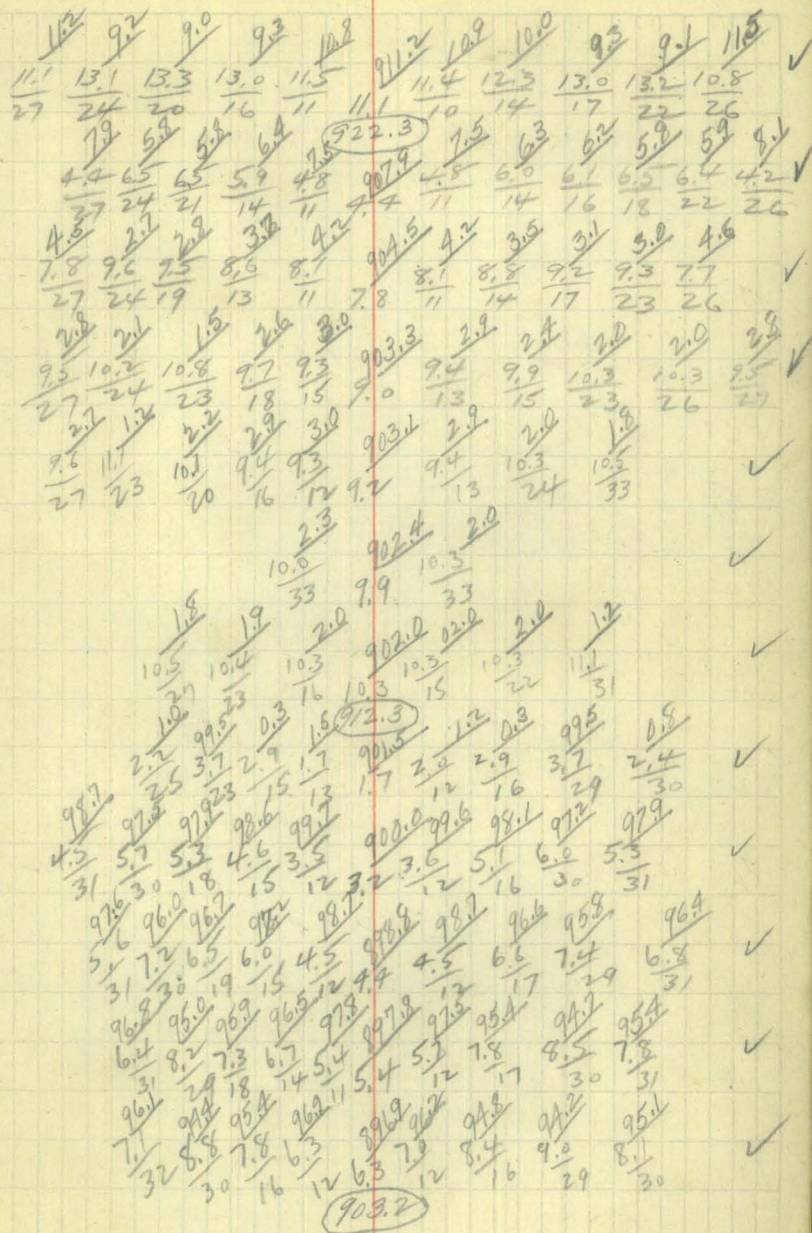
103

102

101

(903.18)

1 m. Sta. 105+48 Top of 7' end 18"x28" pipe left elev. 901.39 21



119

118

117

116

115

114

113

112+74

112

111

110

109

2.71

918.16

12.25

915.45

4.49

927.70

5.85

923.21

2.48

929.06

2.48

926.63

926.58

9.95

929.11

3.13

919.16

922.29

B.M. sta. 112 + 0.5 Spike in maple tree
in yard 90' N.E. Elev. 926.58

22

11.3 9.5 9.5 10.4 11.6 91.6 11.4 10.1 9.4 9.3 10.4
 6.9 8.7 8.7 7.8 6.6 6.8 8.1 8.8 8.9 7.8
 14.0 27 24 21 14 11 10 14 20 24 25
 11.7 11.7 12.4 13.7 13.6 6 7.0 14 20 24 25
 4.2 6.5 6.5 5.8 5.5 4.6 4.6 5.9 7.1 7.2 4.8
 26 24 22 18 14 11 9.3 9 13 18 22 24
 16.4 13.9 14.1 14.8 15.2 16.0 15.7 14.3 13.5 13.5 15.5
 1.8 4.3 4.1 3.4 2.5 2.5 3.9 4.7 4.7 2.7
 26 24 21 15 11 2.2 10 14 18 22 24
 19.8 16.8 17.1 17.5 18.9 18.2 19.4 18.6 16.0 16.0 18.6
 29 10.9 10.6 10.2 8.8 9.3 10.5 11.1 11.7 11.7 9
 26 23 21 14 11 10 13 16 20 21 24
 4.8 8.0 8.3 7.4 6.3 6.1 7.3 8.5 8.3 5.8
 26 23 21 14 10 10 14 20 22 25
 25.2 22.2 22.3 23.0 24.4 24.5 24.2 23.0 22.4 22.4
 2.3 5.4 5.4 4.7 3.3 2.9 3.5 4.7 5.3 5.3 3.2
 26 23 20 14 10 10 14 19 21 24
 2.0 2.3 2.4 2.4 2.6 2.7 2.7 2.7 2.7 2.7
 2.1 4.8 4.7 4.3 3.1 2.6 3.3 4.7 4.9 2.4
 26 24 18 14 11 13 13 23 26
 26.9 24.3 24.4 25.0 26.0 26.0 25.9 24.9 24.6 26.3
 22 4.8 4.7 4.1 3.1 2.9 3.2 4.2 4.5 2.8
 26 24 19 14 11 12 16 16 20 25
 25.8 23.8 22.9 23.6 24.9 24.6 24.4 23.4 23.7 23.0
 3.3 6.3 6.2 5.3 4.7 4.7 4.7 5.7 6.0 6.1
 26 24 18 15 12 12 12 15 18 24
 2.6 2.4 1.9 1.5 1.2 1.2 1.2 1.2 1.2 1.2
 0.5 3.0 3.0 2.3 2.0 2.1 2.1 2.1 2.1 2.1
 27 24 18 15 11 11 11 11 11 11
 18.0 15.3 16.1 15.7 16.2 17.6 17.6 17.6 17.6 17.6
 4.3 6.3 6.2 5.3 4.7 4.7 4.7 5.7 6.0 6.1
 27 24 18 15 12 12 12 15 18 24
 1.7 10.1 9.7 9.0 7.9 7.9 7.9 7.9 7.9 7.9
 27 24 19 14 11 11 11 11 11 11
 11.7 10.1 9.7 9.0 7.9 7.9 7.9 7.9 7.9 7.9
 27 24 19 14 11 11 11 11 11 11
 922.3

B.M. 5.28 899.24 8.56 893.88

131

130

129

128

127

126

125

124

123

122

121

120

2.10

902.44

9.11

900.34

1.28

909.45

9.89

908.27

918.16

Corr.
893.96

B.M. Sta. 131 + 95 2 x 2 40 B. 32.4
Brace Post left on 1/4 sec fence Corr. 23
El. 893.71 El. 893.96

93.7 93.6 93.5 93.4 93.3 93.2 93.1 93.0 92.9 92.8 92.7 92.6 92.5 92.4 92.3 92.2 92.1 92.0 91.9 91.8 91.7 91.6 91.5 91.4 91.3 91.2 91.1 91.0 90.9 90.8 90.7 90.6 90.5 90.4 90.3 90.2 90.1 90.0 89.9 89.8 89.7 89.6 89.5 89.4 89.3 89.2 89.1 89.0 88.9 88.8 88.7 88.6 88.5 88.4 88.3 88.2 88.1 88.0 87.9 87.8 87.7 87.6 87.5 87.4 87.3 87.2 87.1 87.0 86.9 86.8 86.7 86.6 86.5 86.4 86.3 86.2 86.1 86.0 85.9 85.8 85.7 85.6 85.5 85.4 85.3 85.2 85.1 85.0 84.9 84.8 84.7 84.6 84.5 84.4 84.3 84.2 84.1 84.0 83.9 83.8 83.7 83.6 83.5 83.4 83.3 83.2 83.1 83.0 82.9 82.8 82.7 82.6 82.5 82.4 82.3 82.2 82.1 82.0 81.9 81.8 81.7 81.6 81.5 81.4 81.3 81.2 81.1 81.0 80.9 80.8 80.7 80.6 80.5 80.4 80.3 80.2 80.1 80.0 79.9 79.8 79.7 79.6 79.5 79.4 79.3 79.2 79.1 79.0 78.9 78.8 78.7 78.6 78.5 78.4 78.3 78.2 78.1 78.0 77.9 77.8 77.7 77.6 77.5 77.4 77.3 77.2 77.1 77.0 76.9 76.8 76.7 76.6 76.5 76.4 76.3 76.2 76.1 76.0 75.9 75.8 75.7 75.6 75.5 75.4 75.3 75.2 75.1 75.0 74.9 74.8 74.7 74.6 74.5 74.4 74.3 74.2 74.1 74.0 73.9 73.8 73.7 73.6 73.5 73.4 73.3 73.2 73.1 73.0 72.9 72.8 72.7 72.6 72.5 72.4 72.3 72.2 72.1 72.0 71.9 71.8 71.7 71.6 71.5 71.4 71.3 71.2 71.1 71.0 70.9 70.8 70.7 70.6 70.5 70.4 70.3 70.2 70.1 70.0 69.9 69.8 69.7 69.6 69.5 69.4 69.3 69.2 69.1 69.0 68.9 68.8 68.7 68.6 68.5 68.4 68.3 68.2 68.1 68.0 67.9 67.8 67.7 67.6 67.5 67.4 67.3 67.2 67.1 67.0 66.9 66.8 66.7 66.6 66.5 66.4 66.3 66.2 66.1 66.0 65.9 65.8 65.7 65.6 65.5 65.4 65.3 65.2 65.1 65.0 64.9 64.8 64.7 64.6 64.5 64.4 64.3 64.2 64.1 64.0 63.9 63.8 63.7 63.6 63.5 63.4 63.3 63.2 63.1 63.0 62.9 62.8 62.7 62.6 62.5 62.4 62.3 62.2 62.1 62.0 61.9 61.8 61.7 61.6 61.5 61.4 61.3 61.2 61.1 61.0 60.9 60.8 60.7 60.6 60.5 60.4 60.3 60.2 60.1 60.0 59.9 59.8 59.7 59.6 59.5 59.4 59.3 59.2 59.1 59.0 58.9 58.8 58.7 58.6 58.5 58.4 58.3 58.2 58.1 58.0 57.9 57.8 57.7 57.6 57.5 57.4 57.3 57.2 57.1 57.0 56.9 56.8 56.7 56.6 56.5 56.4 56.3 56.2 56.1 56.0 55.9 55.8 55.7 55.6 55.5 55.4 55.3 55.2 55.1 55.0 54.9 54.8 54.7 54.6 54.5 54.4 54.3 54.2 54.1 54.0 53.9 53.8 53.7 53.6 53.5 53.4 53.3 53.2 53.1 53.0 52.9 52.8 52.7 52.6 52.5 52.4 52.3 52.2 52.1 52.0 51.9 51.8 51.7 51.6 51.5 51.4 51.3 51.2 51.1 51.0 50.9 50.8 50.7 50.6 50.5 50.4 50.3 50.2 50.1 50.0 49.9 49.8 49.7 49.6 49.5 49.4 49.3 49.2 49.1 49.0 48.9 48.8 48.7 48.6 48.5 48.4 48.3 48.2 48.1 48.0 47.9 47.8 47.7 47.6 47.5 47.4 47.3 47.2 47.1 47.0 46.9 46.8 46.7 46.6 46.5 46.4 46.3 46.2 46.1 46.0 45.9 45.8 45.7 45.6 45.5 45.4 45.3 45.2 45.1 45.0 44.9 44.8 44.7 44.6 44.5 44.4 44.3 44.2 44.1 44.0 43.9 43.8 43.7 43.6 43.5 43.4 43.3 43.2 43.1 43.0 42.9 42.8 42.7 42.6 42.5 42.4 42.3 42.2 42.1 42.0 41.9 41.8 41.7 41.6 41.5 41.4 41.3 41.2 41.1 41.0 40.9 40.8 40.7 40.6 40.5 40.4 40.3 40.2 40.1 40.0 39.9 39.8 39.7 39.6 39.5 39.4 39.3 39.2 39.1 39.0 38.9 38.8 38.7 38.6 38.5 38.4 38.3 38.2 38.1 38.0 37.9 37.8 37.7 37.6 37.5 37.4 37.3 37.2 37.1 37.0 36.9 36.8 36.7 36.6 36.5 36.4 36.3 36.2 36.1 36.0 35.9 35.8 35.7 35.6 35.5 35.4 35.3 35.2 35.1 35.0 34.9 34.8 34.7 34.6 34.5 34.4 34.3 34.2 34.1 34.0 33.9 33.8 33.7 33.6 33.5 33.4 33.3 33.2 33.1 33.0 32.9 32.8 32.7 32.6 32.5 32.4 32.3 32.2 32.1 32.0 31.9 31.8 31.7 31.6 31.5 31.4 31.3 31.2 31.1 31.0 30.9 30.8 30.7 30.6 30.5 30.4 30.3 30.2 30.1 30.0 29.9 29.8 29.7 29.6 29.5 29.4 29.3 29.2 29.1 29.0 28.9 28.8 28.7 28.6 28.5 28.4 28.3 28.2 28.1 28.0 27.9 27.8 27.7 27.6 27.5 27.4 27.3 27.2 27.1 27.0 26.9 26.8 26.7 26.6 26.5 26.4 26.3 26.2 26.1 26.0 25.9 25.8 25.7 25.6 25.5 25.4 25.3 25.2 25.1 25.0 24.9 24.8 24.7 24.6 24.5 24.4 24.3 24.2 24.1 24.0 23.9 23.8 23.7 23.6 23.5 23.4 23.3 23.2 23.1 23.0 22.9 22.8 22.7 22.6 22.5 22.4 22.3 22.2 22.1 22.0 21.9 21.8 21.7 21.6 21.5 21.4 21.3 21.2 21.1 21.0 20.9 20.8 20.7 20.6 20.5 20.4 20.3 20.2 20.1 20.0 19.9 19.8 19.7 19.6 19.5 19.4 19.3 19.2 19.1 19.0 18.9 18.8 18.7 18.6 18.5 18.4 18.3 18.2 18.1 18.0 17.9 17.8 17.7 17.6 17.5 17.4 17.3 17.2 17.1 17.0 16.9 16.8 16.7 16.6 16.5 16.4 16.3 16.2 16.1 16.0 15.9 15.8 15.7 15.6 15.5 15.4 15.3 15.2 15.1 15.0 14.9 14.8 14.7 14.6 14.5 14.4 14.3 14.2 14.1 14.0 13.9 13.8 13.7 13.6 13.5 13.4 13.3 13.2 13.1 13.0 12.9 12.8 12.7 12.6 12.5 12.4 12.3 12.2 12.1 12.0 11.9 11.8 11.7 11.6 11.5 11.4 11.3 11.2 11.1 11.0 10.9 10.8 10.7 10.6 10.5 10.4 10.3 10.2 10.1 10.0 9.9 9.8 9.7 9.6 9.5 9.4 9.3 9.2 9.1 9.0 8.9 8.8 8.7 8.6 8.5 8.4 8.3 8.2 8.1 8.0 7.9 7.8 7.7 7.6 7.5 7.4 7.3 7.2 7.1 7.0 6.9 6.8 6.7 6.6 6.5 6.4 6.3 6.2 6.1 6.0 5.9 5.8 5.7 5.6 5.5 5.4 5.3 5.2 5.1 5.0 4.9 4.8 4.7 4.6 4.5 4.4 4.3 4.2 4.1 4.0 3.9 3.8 3.7 3.6 3.5 3.4 3.3 3.2 3.1 3.0 2.9 2.8 2.7 2.6 2.5 2.4 2.3 2.2 2.1 2.0 1.9 1.8 1.7 1.6 1.5 1.4 1.3 1.2 1.1 1.0 0.9 0.8 0.7 0.6 0.5 0.4 0.3 0.2 0.1 0.0

142

141

T. P.

7.22

899.49

7.12

892.27

140+18

139+95

139

138

137

7.47

899.39

7.32

891.92

136

135

134

133

132

899.24

92.7 90.1 91.1 93.9 94.2 94.8 91.6 91.2 91.3 92.0 92.7
 6.8 8.4 7.8 5.6 5.3 7.9 8.3 8.2 7.5 6.8
 31 29 19 13 5.3 13 14 31 32 37 43
 91.8 90.6 90.9 91.7 93.9 94.1 93.7 91.1 90.6 91.8
 7.7 8.9 8.6 7.8 5.6 5.8 8.4 8.9 7.7
 3.6 32 26 17 13 5.4 14 19 39 40
 91.7 90.5 90.7 90.9 899.25 94.1 94.4 90.6 90.1
 7.7 8.9 8.7 8.5 5.3 5.3 5.0 8.8 9.3
 41 39 28 20 12 5.3 10 17 27
 91.2 91.4 90.5 94.2 94.3 94.3 94.0 92.8 91.0 91.1
 8.2 8.0 8.2 5.2 5.1 5.4 6.6 8.4 8.3
 26 24 21 11 5.1 5 11 15 19 22
 91.8 91.0 90.9 91.6 94.1 94.2 94.1 91.1 90.8 90.8 91.4
 7.6 8.4 8.5 7.8 5.3 5.3 8.3 8.5 8.6 8.0
 41 39 33 19 13 5.2 14 19 33 40 41
 93.0 92.0 91.5 91.8 94.2 94.2 93.9 91.5 91.4 91.5 92.1
 6.4 7.4 7.9 8.2 5.2 5.5 7.9 8.0 7.9 7.3
 41 38 26 20 14 5.2 14 19 32 40 42
 91.9 91.2 91.4 94.2 94.1 91.4 91.2 91.8
 7.5 8.2 8.0 5.2 5.2 5.3 8.0 8.2 7.6
 40 38 17 12 5.2 13 20 40 42
 91.7 91.1 91.1 899.25 93.9 93.7 90.8 91.0 91.8
 7.5 8.1 8.1 5.3 5.3 5.5 8.4 8.2 7.4
 24 20 17 13 5.3 14 19 23 25
 91.7 91.6 91.6 93.6 93.8 93.7 91.2 90.9 91.8
 7.5 7.6 7.6 5.6 5.4 5.5 8.0 8.3 7.3
 28 23 19 14 5.4 15 19 25 26
 92.2 91.7 92.0 93.8 94.0 93.6 91.6 91.7 92.1
 7.0 7.5 7.2 5.3 5.2 5.6 7.6 7.5 7.1
 23 22 18 14 5.2 14 19 22 24
 92.8 92.1 92.3 92.5 92.5 94.0 94.1 93.6 92.1 92.3 92.7
 6.4 7.1 6.9 6.7 6.7 5.2 5.1 5.6 7.1 6.9 6.5
 26 24 23 22 18 14 5.1 14 18 23 24
 93.5 92.5 93.0 94.2 94.1 93.9 92.9 93.1 93.0
 5.7 6.7 6.2 5.0 5.1 5.3 6.3 6.1 6.2
 27 25 16 12 5.1 13 17 24 31
 (899.2)

155

154

153

152

T.P. 6.53 (900.49) 6.03 893.96

151

150

149

148

147

B.M.
T.P.

146

145

144

143

899.49

95.1 93.0 93.6 94.0 95.1 95.6 94.8 93.7 92.8 94.2 ✓ 25
 5.4 7.5 6.9 6.5 5.4 11.4 9 5.7 6.8 7.7 6.3
 32 29 19 16 12 16 30 32
 95.0 93.0 93.6 93.9 95.3 95.1 93.5 92.7 94.3 ✓
 5.5 7.5 7.0 6.6 5.2 8 95.3 5.4 7.0 7.8 6.2
 31 29 19 15 11 52 11 16 30 32
 94.9 92.8 93.8 95.1 95.3 94.7 93.2 92.6 93.9 ✓
 5.6 7.7 6.7 5.4 5.8 7.3 7.9 6.6
 31 29 14 10 52 12 16 30 32
 94.6 93.0 92.3 94.6 94.8 93.3 92.2 93.8 ✓
 5.9 7.5 7.2 5.9 895.1 5.7 7.2 8.3 6.7
 31 29 15 11 54 12 16 30 31
 94.6 92.5 92.8 93.2 94.7 900.5 94.9 93.0 92.5 92.2 93.8 ✓
 5.4 7.5 7.2 6.8 5.3 895.2 5.1 7.0 7.5 7.8 6.2
 31 29 19 15 11 48 12 16 20 30 32
 94.4 92.6 93.0 93.4 94.8 894.9 94.7 93.2 92.4 93.5 ✓
 5.6 7.4 7.0 6.6 5.2 11 5.1 5.3 6.8 7.6 6.2
 31 29 19 15 11 51 11 15 29 31
 894.7 92.8 93.0 93.4 94.9 895.3 94.9 93.2 92.0 93.5 ✓
 5.3 7.2 7.0 6.6 5.1 11 4.7 5.1 6.8 8.0 6.5
 31 29 18 15 11 47 11 16 28 31
 94.9 92.7 93.0 93.3 94.8 895.2 94.9 93.1 92.2 93.9 ✓
 5.1 7.3 7.0 6.7 5.2 11 4.8 5.1 6.9 7.8 6.1
 31 29 19 16 11 48 11 16 28 31
 95.0 93.0 94.0 94.9 95.1 94.8 93.0 92.1 94.1 ✓
 5.0 7.0 6.0 5.1 5.2 7.0 7.9 5.9
 30 28 17 14 49 12 17 29 31
 95.0 92.2 93.4 94.0 94.8 93.0 92.9 94.0 ✓
 4.2 7.3 6.1 4.8 95.0 4.7 6.5 7.6 5.5
 30 28 14 10 4.5 13 17 29 31
 93.8 92.1 92.9 94.3 94.6 94.6 93.1 91.2 93.3 ✓
 5.7 7.4 6.8 5.2 4.9 4.9 6.4 7.8 6.2
 30 28 14 11 4.9 13 16 29 31
 93.4 91.8 92.7 94.3 94.3 94.2 92.4 91.7 93.0 ✓
 6.1 7.7 6.8 5.2 5.3 7.1 7.8 6.5
 31 29 16 12 52 14 18 29 31
 93.5 91.2 92.0 92.4 94.2 94.3 92.6 91.4 93.5 ✓
 6.0 8.3 7.5 7.1 5.3 5.2 6.9 8.1 6.0
 32 29 15 16 12 52 13 17 30 32
 (899.5)

166

165

498

(90 2.62

4.23

897 .64

164

163

162

161

160

159

B M.

158 + 85

4.65

(901.87)

3.28

89722

897.21

158 + 44

 $158 + 25$

158

157

156

90049

900.5

C. M. Sta. 170 + 54 Spike in Poplar
Tree 200' Rt. Elev. 896.91

27

173

172

5.59

(902.50)

5.73

896.89

corr.
896.91

171

(902.50)

170

169

168

167+40

167+26

167

166+81

166+73

166+55

(902.62)

91 974 98.0 12
2.4 5.1 4.5 2.3 900.4 2.5 4.5 5.6 3.4
29 26 16 12 2.1 13 19 30 32
98.9 96.4 97.1 99.4
3.6 6.1 5.4 3.1 899.6 99.2 97.2 96.7 96.6 98.6
29 27 18 12 2.7 13 18 22 29 32
98.0 95.8 96.5 98.5
4.5 6.7 6.0 4.0 899.6 99.4 96.5 95.3 97.5
30 28 18 12 3.9 12 18 29 31
97.8 95.3 95.9 97.1 97.5 902.5 97.6 96.1 95.6 95.0 97.4
2.8 2.1 6.7 5.5 4.8 5.0 6.5 7.0 7.6 5.2
29 27 19 15 12 4.5 13 18 22 29 32
96.9 94.0 94.7 97.3
5.8 8.6 7.9 5.3 897.5 97.3 95.9 95.0 94.2 96.7
29 26 19 13 5.1 13 18 21 29 32
94.5 93.5 94.2 97.4 899.4 97.1 95.0 94.0 93.2 95.4
2.8 9.1 8.4 5.2 5.5 7.6 8.6 8.9 7.2
28 25 18 12 5.2 13 18 24 29 32
93.2 93.2 97.3
9.4 9.3 5.3 897.5 97.1 94.1 93.4 94.6
26 23 14 5.1 13 21 28 31
95.6 97.2 897.5 97.3 93.3 93.4 94.6
2.0 5.4 5.3 9.3 9.2 8.0
17 14 5.1 13 25 29 31
91.9 97.4 897.3 97.4
1.7 5.2 5.2
22 13 5.3 14
92.9 96.9 897.2 97.0 91.2
9.7 5.7 5.6 11.4
21 12 5.4 13 21
92.4 93.1 97.0 897.2 96.6 97.1
10.2 2.5 5.6 5.0 10.5
22 19 11 5.4 13 20
93.5 93.2 97.2 897.1 96.6 95.2 94.5 93.5 91.5
9.1 8.9 5.4 6.0 2.4 8.1 9.1 11.1
22 18 11 5.5 12 16 19 22 24
(902.6)

185

B.M.

184

183

182

Hub Sta 181
H. T.P.

181

180

179

178

177

176

175

174

5.26 907.71

8.10

912.77

2.98

904.87

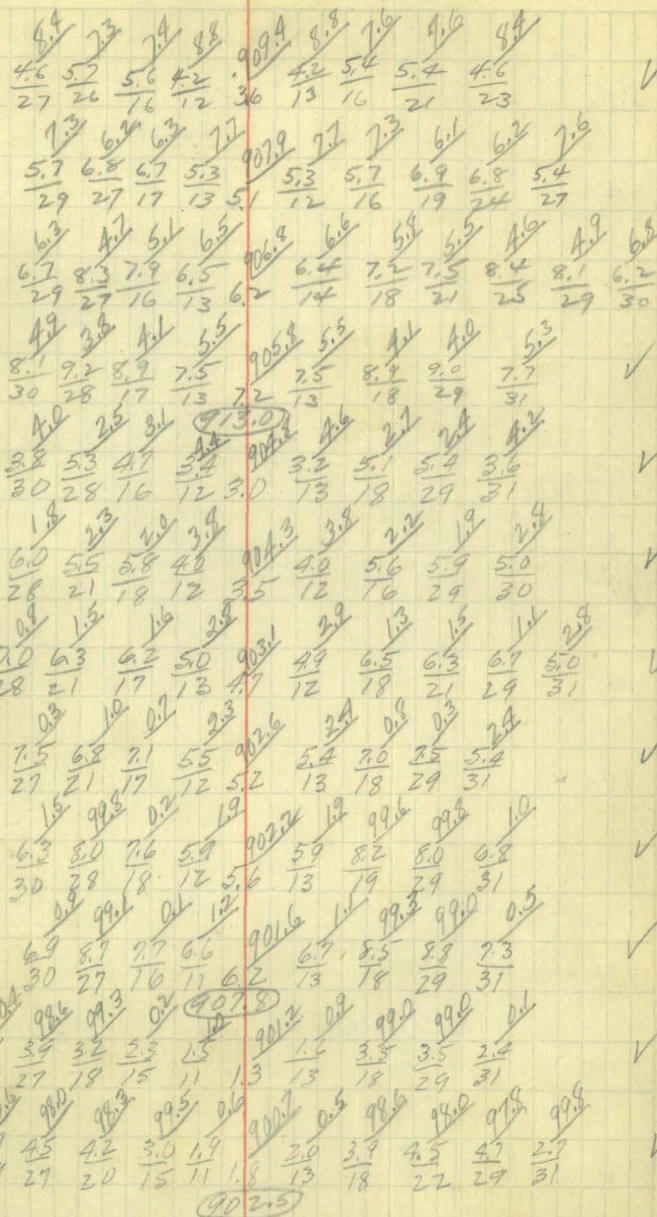
6.69

902.85

1.34

901.16

902.50

B.M. 184+22 x 2 Hub 5.57 Second Post 28
Left Cl. 907.63

196

195+50

195

194

193

192

191

T.R.

190

189

188

187

186

9.66

943.48

1.07

933.82

12.65

934.89

0.77

922.24

10.87

923.01

0.83

912.14

912.97

42.7	39.1	39.7	40.6	41.1	40.8	39.3	39.1	40.9
0.8	4.4	3.8	2.9	2.4	2.7	4.2	4.4	2.6
29	24	16	13	2.4	12	18	23	25
42.7	39.1	39.7	40.6	41.1	40.8	39.3	39.1	40.9
0.7	4.5	3.9	3.0	2.7	3.3	4.2	4.5	2.3
29	24	16	13	2.7	13	18	22	25
42.7	39.1	39.7	40.6	41.1	40.8	39.3	39.1	40.9
1.3	5.5	5.0	4.5	3.8	3.5	4.1	4.8	5.6
27	23	19	15	12	3.5	13	17	22
42.7	39.1	39.7	40.6	41.1	40.8	39.3	39.1	40.9
5.0	8.9	8.3	7.6	7.1	7.2	9.0	9.3	5.6
27	23	16	13	12	12	17	22	26
42.7	39.1	39.7	40.6	41.1	40.8	39.3	39.1	40.9
1.4	4.9	4.5	3.5	3.1	3.4	4.6	5.0	1.7
27	23	16	13	13	13	16	23	26
42.7	39.1	39.7	40.6	41.1	40.8	39.3	39.1	40.9
6.5	9.2	8.5	8.4	2.3	2.7	2.7	2.6	2.7
27	24	21	16	13	2.3	13	17	24
42.7	39.1	39.7	40.6	41.1	40.8	39.3	39.1	40.9
1.8	13.1	12.9	10.9	10.8	11.2	13.4	13.1	11.9
26	25	18	12	10.8	13	19	24	26
42.7	39.1	39.7	40.6	41.1	40.8	39.3	39.1	40.9
3.0	4.1	4.3	2.4	2.0	2.2	2.4	4.8	5.0
27	26	17	13	2.2	13	13	20	24
42.7	39.1	39.7	40.6	41.1	40.8	39.3	39.1	40.9
7.2	8.2	7.5	6.3	1.7	1.7	1.6	1.4	1.5
27	25	16	13	5.6	13	17	8.5	7.5
42.7	39.1	39.7	40.6	41.1	40.8	39.3	39.1	40.9
10.1	10.9	10.6	10.1	9.0	9.1	10.9	11.0	10.1
27	26	20	17	13	8.1	12	17	22
42.7	39.1	39.7	40.6	41.1	40.8	39.3	39.1	40.9
1.8	2.7	2.6	1.2	0.9	0.9	2.7	2.8	1.8
27	25	16	13	0.9	12	16	20	22
42.7	39.1	39.7	40.6	41.1	40.8	39.3	39.1	40.9
3.2	4.5	4.2	2.5	2.5	2.5	4.2	4.5	3.1
27	25	18	12	2.3	12	16	20	22

913.0

B.M. 20760 Height + Ft. on largest
Boulder near J. cor. Rt. El. 935.74

30

T.P. 207 0.00 942.66

206

205

204+385 Culv.

204

203

B.M. 7.52 942.66 8.50 935.07 Cor. Elev 935.14

202

201

200

199

198

197

T.P. 3.36 943.57 3.27 940.21

943.48

2070 39.9 40.6 41.4 41.4 41.1 40.1 40.0 41.9
0.7 2.8 2.1 1.3 1.6 2.6 2.7 0.8
28 24 16 12 13 16 22 24

31.9 36.2 36.5 38.5 39.2 39.0 37.1 36.5 38.7
4.8 6.5 6.2 4.2 3.7 3.7 5.6 6.2 4.0
28 26 17 12 3.5 11 18 20 22

34.8 33.8 34.1 36.7 37.3 37.1 33.9
7.9 8.9 8.6 6.0 5.4 5.6 8.8
28 27 19 12 10 17

30.4 33.4 33.2 35.2 35.2 36.3 36.4 36.2 32.3
8.3 7.3 7.5 7.5 7.5 6.4 6.5 10.4
29 27 19 15 14 12 13 18

35.1 33.4 34.4 36.3 36.2 35.8 34.9 32.6 32.5 33.0
7.6 9.3 9.3 6.4 6.9 7.8 10.1 10.2 9.7
28 26 18 12 11 14 19 24 25

35.9 34.2 34.0 36.3 36.2 35.9 33.0 32.7 33.3
7.7 9.4 9.6 7.3 7.7 7.7 10.6 10.9 10.3
28 26 18 13 12 18 23 25

38.0 34.4 34.4 35.3 36.0 36.8 36.7 36.9 35.4 34.9 36.4
5.6 8.2 8.2 7.8 7.6 6.7 6.7 8.2 8.7 7.2
28 25 21 18 15 13 13 19 24 25

40.1 36.9 36.4 37.0 38.0 38.3 38.1 36.6 36.1 38.6
2.9 6.7 7.2 6.6 5.6 5.5 7.0 7.5 4.8
28 24 19 16 12 12 17 23 26

40.3 37.3 37.8 38.6 38.5 38.5 37.4 36.7 38.3
3.3 6.3 5.8 5.0 5.1 5.1 6.3 6.9 5.3
29 25 15 12 12 12 15 23 25

39.2 37.8 38.1 38.5 38.5 38.5 37.6 36.9 36.8 37.3
3.9 5.8 5.5 4.1 4.1 4.1 6.0 6.7 6.8 6.3
28 25 16 12 12 12 16 17 24 25

41.0 39.6 38.8 40.4 40.4 40.1 37.9 37.0 38.6
2.6 5.0 4.8 3.2 3.2 3.5 5.7 5.6 5.0
28 26 19 13 12 12 18 23 25

943.6

950.2

223

222

221

220

219

218

217

216+77

216

 $215 + 50$

215

214

916

957.86

3.95

948.70

9

(952.65)

52.7	51.5	51.6	52.6	52.3	53.5	53.1	51.9	51.1	51.4
5.2	6.4	6.3	5.3	5.6	4.0	4.8	6.0	6.8	6.5
30	26	22	76	14	12	12	15	22	23
53.1	51.2	51.1	52.1	51.6	52.9	52.5	51.0	51.5	50.8
4.8	6.7	6.8	5.8	6.3	5.0	5.4	6.9	6.4	7.1
30	26	21	18	14	11	12	15	17	19
53.2	50.4	50.3	50.9	50.6	51.7	52.0	51.5	50.1	50.6
4.7	7.5	7.6	7.0	7.3	6.2	6.0	7.8	7.3	7.9
30	23	21	17	15	11	13	16	18	25
51.8	49.1	49.1	49.8	49.4	50.2	50.4	49.1	49.8	49.0
6.1	8.8	8.8	8.7	8.5	7.7	7.5	8.8	8.1	8.9
31	23	20	76	74	71	13	16	18	24
47.8	47.8	48.4	48.0	48.2	48.3	49.3	47.9	47.7	48.9
4.4	4.9	4.3	4.7	4.5	3.6	3.4	4.8	3.0	3.8
24	20	15	15	13	12	12	16	25	30
47.9	46.9	46.8	47.7	47.2	48.4	48.3	46.9	46.3	47.5
4.8	5.8	5.9	5.0	5.5	2.3	4.4	5.8	6.4	5.2
30	27	20	15	14	10	12	15	24	28
47.1	45.9	46.0	46.7	47.8	48.2	47.3	46.6	46.0	45.4
5.6	6.8	6.7	6.0	3.9	4.5	5.4	7.1	7.7	7.3
31	25	19	17	12	9	12	19	29	29
47.2	46.1	46.7	47.8	48.4	47.5	45.8	45.3		
5.5	6.6	6.0	4.9	4.8	5.2	6.9	7.4		
31	26	14	12	43	14	17	28		
47.9	46.3	45.9	46.8	46.9	47.6	47.2	46.1	45.4	46.5
4.8	6.4	6.8	5.9	5.8	5.1	5.5	6.6	7.3	6.2
30	26	18	15	13	9	12	14	21	30
48.9	46.1	46.3	47.0	46.2	47.3	47.1	45.9	45.6	47.6
3.8	6.6	6.4	5.7	6.5	5.4	5.6	6.8	7.1	5.1
30	22	14	15	14	11	13	16	25	31
48.1	45.6	46.2	45.9	46.7	46.8	46.6	45.4	45.2	47.4
4.6	7.1	6.5	6.8	6.0	4.6	6.1	7.3	7.5	5.3
30	21	17	14	12	54	12	15	23	31
45.6	44.1	44.4	45.6	45.9	45.2	43.8	43.9	45.8	
7.1	7.6	8.3	7.1	4.9	7.5	8.9	8.8	6.9	
30	24	14	12	68	13	16	24	30	
(952.7)									

B.M. 23+77 spike in square
gate post of 4 1/4 sec. F. RT. Co. 952.55 33

234

6.43 (972.31) 5.50 965.88

233

232

231

230+50

230

229

T.P.

228

227

226

225

224

B.M. 10.64 (963.19) 5.26 952.60 952.55

957.86

62.9 62.3 62.1 62.3 62.5 64.1 62.5 62.9 64.0 ✓
9.4 10.0 10.2 8.0 8.2 7.8 9.4 8.3
30 28 20 11 7.8 13 16 27 31

61.7 61.3 61.6 61.3 64.7 62.0 62.2 62.8 ✓
9.7 10.1 7.8 2.1 6.5 6.7 7.4 9.2 8.6
30 28 20 12 6.5 12 18 28 32

63.9 63.0 62.5 62.9 65.1 65.3 65.0 63.5 63.5 64.0 ✓
7.5 8.4 8.9 8.5 6.3 6.4 7.9 7.9 7.4
31 28 22 19 12 6.1 12 15 25 30

66.4 64.6 64.9 65.1 64.6 64.2 66.1 66.7 66.4 65.0 65.4 65.3 66.8 67.2 ✓
5.0 6.8 7.1 6.3 6.8 6.6 5.3 9.6 5.0 6.4 6.0 6.1 4.6 4.2
31 28 24 17 17 15 12 4.7 10 14 16 21 26 30

66.9 65.1 64.8 65.2 64.8 66.0 66.2 66.0 65.8 65.9 65.5 65.8 66.8 ✓
4.5 6.3 6.6 6.2 6.6 5.4 5.4 6.1 5.6 5.9 5.6 4.6
31 23 22 19 17 13 11 14 15 20 23 25

67.1 64.6 65.2 64.7 65.6 66.8 65.6 66.7 ✓
4.3 6.6 6.2 6.7 5.75 9.6 5.8 4.7
33 23 19 18 13 5.6 7 27

64.7 62.9 63.1 63.5 62.8 63.6 63.6 63.5 62.9 62.8 63.2 63.1 64.1 ✓
6.7 8.5 8.3 7.9 8.6 7.8 7.8 7.9 8.6 8.2 8.3 7.3
31 26 21 19 18 15 10 12 13 14 19 21

67.9 66.2 66.6 66.0 66.1 67.4 61.1 60.4 60.4 60.9 60.5 61.0 ✓
7.3 3.0 2.6 3.2 3.2 2.1 6.1 2.1 2.8 2.8 2.3 2.7 2.2
31 23 17 16 15 12 1.8 12 14 15 17 27 29

59.5 57.8 57.7 58.8 59.4 59.2 58.2 58.4 57.8 57.7 59.0 ✓
3.7 5.4 5.5 4.4 4.0 5.2 4.8 5.4 5.5 4.2
31 25 14 11 3.8 12 14 16 22 26 30

56.9 56.5 56.0 59.4 57.7 59.4 56.2 56.6 55.7 56.0 56.7 ✓
6.3 7.7 7.2 5.8 5.8 5.8 6.6 7.5 7.2 6.5
31 26 15 11 5.5 12 15 17 22 29 30

55.0 53.6 53.9 54.8 54.5 54.5 55.8 56.1 55.7 54.5 54.7 53.6 53.7 54.4 ✓
8.2 8.6 8.3 8.4 8.7 8.7 7.4 7.1 7.5 8.7 8.5 7.6 7.5 8.8
31 26 19 16 15 14 11 7.1 13 16 18 25 29 31

53.8 52.5 53.3 54.3 54.8 54.3 53.0 52.8 52.1 52.8 ✓
9.4 10.7 9.9 8.9 8.4 8.9 10.2 10.4 11.1 10.4
29 23 13 11 8.4 12 15 18 28 30

(963.2)

245

244

243

242

241+75

T.P.

2.18

975.84

0.32

973.66

241

240

239

238

B.M.

5.61

973.98

4.01

968.30

Corr.

968.37

237

236

235

68.4	67.4	67.6	69.5	69.7	69.3	66.7	66.2	66.8	✓				
7.4	8.4	8.2	6.3	6.1	6.5	9.1	9.6	9.2					
30	27	18	13	6.1	15	20	29	30					
70.0	68.8	68.8	69.2	70.4	67.9	67.7	67.3	67.9	✓				
5.8	7.0	7.0	6.6	5.4	5.9	8.1	8.5	7.9					
31	27	17	14	12	5.2	12	18	28	29				
72.0	70.2	70.2	71.3	97.16	71.0	69.7	69.9	70.0	70.5	✓			
3.8	5.6	5.6	4.5	4.8	6.1	5.9	5.8	5.3					
29	25	14	11	4.2	12	15	17	30	31				
73.9	71.1	71.4	71.3	72.2	97.24	72.2	71.3	71.0	72.5	✓			
1.9	4.7	4.4	4.5	3.6	3.4	3.6	4.5	4.8	3.3				
30	25	16	14	13	3.4	12	15	27	30				
4.5	71.3	71.8	71.3	71.4	72.4	72.3	71.4	71.2	72.8	✓			
1.3	4.5	4.0	4.5	4.4	3.4	3.5	4.4	4.6	3.0				
30	25	17	15	14	12	3.4	13	15	26	31			
72.6	71.0	71.1	71.0	71.0	72.2	97.26	72.2	71.2	71.0	71.5	71.6	73.0	✓
1.4	3.0	2.9	3.0	3.0	1.8	1.8	2.8	3.0	2.5	2.4	1.0		
30	27	17	16	15	12	1.5	12	14	16	17	27	30	
70.0	69.7	69.1	69.2	70.0	97.12	71.0	69.8	69.8	70.1	70.2	71.5	✓	
4.0	4.3	4.9	4.1	3.9	3.9	3.0	4.2	4.2	3.9	3.8	2.5		
30	24	19	15	12	2.8	12	15	16	17	26	30		
68.3	67.9	68.3	69.7	97.01	69.8	68.7	68.6	68.7	68.6	70.1	✓		
5.7	6.1	5.7	4.3	4.2	4.2	5.3	5.4	5.3	5.4	3.9			
30	24	14	11	3.9	12	14	16	17	26	30			
67.6	67.8	67.2	67.7	68.6	69.2	69.2	67.7	68.3	67.8	69.1	69.8	✓	
6.4	6.8	6.8	6.3	5.4	4.8	4.8	6.3	5.7	6.2	4.9	4.2		
30	29	18	16	12	4.8	11	14	16	26	28	30		
67.1	66.6	67.3	67.8	68.0	67.1	64.4	66.5	69.9	✓				
4.6	5.7	5.0	4.5	4.3	5.2	5.9	5.8	2.4					
29	24	15	13	4.2	11	14	16	22	30				
67.1	65.4	65.4	66.7	66.9	66.8	65.2	65.6	65.8	68.0	✓			
5.2	6.9	6.9	5.6	5.8	7.1	6.7	6.5	4.3					
26	21	14	11	5.4	12	15	19	26	30				
64.5	63.6	63.9	65.4	65.7	65.2	63.7	64.1	65.9	✓				
7.8	8.7	8.4	6.9	7.1	8.6	8.2	6.4						
27	21	16	11	6.6	12	16	26	30					
972.3													

972.31

255

254

253+86

Rock

253

1.80

976.86

2.24

975.06

252

251

4.32

977.30

2.48

972.98

250

249

248

247

4.93

975.46

5.31

970.53

246

975.84

Sta. 250+23, splice in 1st post
on 1/4 sec fence
Left. El. 973.01

71.5	68.4	69.7	70.7	70.8	70.6	69.8	69.0	68.8	71.5
5.4	8.5	7.2	6.2	6.1	6.3	7.1	7.9	8.1	5.4
31	28	15	12	61	12	15	22	26	30

75.0	70.4	71.2	72.4	72.7	72.6	71.4	70.4	74.8
1.9	6.5	5.7	4.5	4.3	5.5	6.5	7.1	3.1
30	26	14	11	7.2	11	15	27	31

75.1	71.0	71.3	71.9	72.6	72.9	72.6	71.5	70.6	74.8
1.8	5.9	5.6	5.0	4.3	4.3	5.4	6.3	7.1	2.1
30	26	18	13	11	4.0	12	15	27	31

73.7	70.6	70.8	72.2	72.3	71.3	70.8	70.4	73.1
3.6	6.7	6.5	5.1	5.0	6.9	6.5	6.9	4.2
29	26	15	12	4.7	12	16	19	29

70.7	69.5	69.4	69.1	71.5	72.0	71.5	69.5	69.1	69.1	69.8
6.6	7.8	7.9	7.2	5.8	5.8	5.8	7.8	8.2	8.2	7.5
24	26	19	15	13	5.3	13	18	20	28	29

70.5	69.1	69.7	71.0	71.4	70.8	68.6	68.1	69.1
6.8	8.2	7.6	6.3	6.4	6.4	8.7	9.2	8.2
29	23	14	11	5.9	14	18	25	26

977.3

71.7	69.2	69.9	70.5	70.9	70.7	69.5	69.1	71.0
3.8	6.3	5.6	5.0	4.8	4.8	6.0	6.4	4.5
30	26	13	12	4.6	13	15	24	28

70.7	68.6	69.1	70.1	70.3	70.2	69.0	68.9	68.6	70.7
4.8	6.9	6.4	5.4	5.3	6.5	6.5	6.6	6.7	4.8
28	26	14	12	5.2	12	14	23	25	28

69.9	66.9	67.6	68.0	69.8	69.9	69.4	68.2	67.8	67.3	67.1	68.1
5.6	8.6	7.9	7.5	5.7	6.1	6.1	7.3	7.7	8.2	8.4	7.4
29	28	18	15	12	5.6	12	14	21	23	27	29

68.6	66.7	67.4	69.5	69.7	69.3	66.8	66.1	66.6
6.4	8.4	8.4	6.0	6.2	8.7	9.1	8.9	8.9
30	26	18	13	5.8	13	18	28	30

68.5	66.5	66.9	69.0	69.4	69.1	66.9	66.4	66.0	66.8
7.3	9.3	8.9	6.8	6.4	6.2	8.9	9.4	9.8	7.0
29	27	18	14	6.4	13	17	20	29	31

975.8

B.M. 6.55 964.24 8.95 957.65 ^{Corr.} 957.69

263+50

263+40

263

262+50

262+17

262

261

260

259

258

T.P. 2.73 966.60 12.99 963.87

257

256

56.3 58.2 58.3 58.5 56.4 55.9 56.9
 10.3 9.4 8.3 8.1 10.2 10.2 9.7
 29 24 23 18 23 35 37
 56.1 58.3 58.3 58.2 56.5 55.8 56.2 56.7
 10.5 8.3 8.3 8.4 10.1 10.8 10.4 9.9
 35 31 8.3 21 24 32 36 38
 58.3 58.3 58.4 58.4 58.3 56.3 56.4 57.0
 8.3 8.3 8.2 8.3 10.3 10.2 9.6
 33 23 14 19 23 33 35

58.9 57.0 56.9 58.7 58.5 56.6 56.4 57.4
 7.7 9.6 9.2 7.9 8.1 10.0 10.2 9.2
 31 27 20 16 16 19 28 29

58.2 57.1 57.5 58.6 59.2 58.8 56.5 56.9 58.5
 8.4 9.5 9.6 8.0 7.4 7.8 10.1 9.7 9.1
 29 26 15 12 15 20 29 30

59.1 57.4 57.4 58.7 59.3 58.9 58.2 56.8 57.1 57.6
 7.5 9.2 9.2 7.9 7.7 8.4 9.8 9.5 9.0
 31 29 16 13 11 15 20 30 31

59.3 58.3 58.5 59.7 60.3 59.9 58.1 58.3 59.7
 7.3 8.3 8.1 6.9 6.9 7.7 8.3 6.9
 31 29 15 12 6.3 12 16 27 30

60.2 59.0 59.3 60.9 61.5 61.3 60.9 59.7 62.4
 6.4 7.6 7.3 5.7 5.1 5.3 6.7 6.9 8.2
 30 26 15 12 5.1 13 16 25 31

62.0 60.6 60.8 62.3 62.6 62.1 61.0 60.9 62.4
 4.6 6.0 5.9 4.3 4.5 5.6 5.7 4.2
 30 27 14 11 4.0 13 16 27 30

64.0 62.0 62.5 63.6 64.2 63.4 62.1 62.3 63.0
 2.6 4.6 4.1 3.6 3.2 4.5 4.3 3.6
 30 26 15 12 12 15 28 29

65.4 64.4 64.2 65.7 64.6 64.1 65.2
 11.5 12.5 12.3 11.2 12.9 12.8 11.7
 30 28 15 12 16 26 29

68.1 66.3 66.9 68.1 68.5 68.0 66.4 66.4 67.9
 8.8 10.6 10.0 8.4 8.9 10.5 10.5 9.0
 31 28 15 12 12 15 26 29

976.9

976.86

273

272

271

270

269

268

267

266+15

266

265

264+14

264

7.08

968.81

251

961.73

$$\begin{array}{r} 64.7 \\ 41 \\ 30 \end{array} \begin{array}{r} 63.3 \\ 5.5 \\ 26 \end{array} \begin{array}{r} 63.8 \\ 5.0 \\ 14 \end{array} \begin{array}{r} 64.4 \\ 4.4 \\ 12 \end{array} \begin{array}{r} 64.7 \\ 4.1 \\ 12 \end{array} \begin{array}{r} 64.3 \\ 4.5 \\ 12 \end{array} \begin{array}{r} 63.6 \\ 5.2 \\ 15 \end{array} \begin{array}{r} 63.3 \\ 5.5 \\ 27 \end{array} \begin{array}{r} 66.5 \\ 2.5 \\ 30 \end{array}$$

$$\begin{array}{r} 64.5 \\ 4.3 \\ 30 \end{array} \begin{array}{r} 62.8 \\ 6.0 \\ 25 \end{array} \begin{array}{r} 62.8 \\ 6.0 \\ 17 \end{array} \begin{array}{r} 63.6 \\ 5.2 \\ 12 \end{array} \begin{array}{r} 64.3 \\ 4.5 \\ 13 \end{array} \begin{array}{r} 63.7 \\ 5.1 \\ 15 \end{array} \begin{array}{r} 63.1 \\ 5.7 \\ 15 \end{array} \begin{array}{r} 62.7 \\ 6.1 \\ 18 \end{array} \begin{array}{r} 62.8 \\ 6.0 \\ 26 \end{array} \begin{array}{r} 64.9 \\ 3.9 \\ 31 \end{array}$$

$$\begin{array}{r} 63.0 \\ 5.8 \\ 30 \end{array} \begin{array}{r} 61.9 \\ 6.9 \\ 28 \end{array} \begin{array}{r} 61.7 \\ 7.1 \\ 21 \end{array} \begin{array}{r} 62.0 \\ 6.8 \\ 18 \end{array} \begin{array}{r} 62.5 \\ 6.3 \\ 15 \end{array} \begin{array}{r} 63.1 \\ 5.7 \\ 12 \end{array} \begin{array}{r} 63.7 \\ 5.1 \\ 11 \end{array} \begin{array}{r} 63.2 \\ 5.6 \\ 14 \end{array} \begin{array}{r} 62.0 \\ 6.8 \\ 14 \end{array} \begin{array}{r} 61.8 \\ 7.0 \\ 27 \end{array} \begin{array}{r} 63.3 \\ 5.5 \\ 30 \end{array}$$

$$\begin{array}{r} 61.3 \\ 7.5 \\ 30 \end{array} \begin{array}{r} 60.8 \\ 8.0 \\ 29 \end{array} \begin{array}{r} 60.8 \\ 8.0 \\ 28 \end{array} \begin{array}{r} 60.5 \\ 8.3 \\ 25 \end{array} \begin{array}{r} 61.9 \\ 8.5 \\ 16 \end{array} \begin{array}{r} 61.9 \\ 6.9 \\ 12 \end{array} \begin{array}{r} 62.4 \\ 6.5 \\ 6.3 \end{array} \begin{array}{r} 60.7 \\ 6.4 \\ 11 \end{array} \begin{array}{r} 60.4 \\ 8.1 \\ 16 \end{array} \begin{array}{r} 60.4 \\ 8.4 \\ 18 \end{array} \begin{array}{r} 61.6 \\ 8.4 \\ 28 \end{array} \begin{array}{r} 61.6 \\ 7.2 \\ 30 \end{array}$$

$$\begin{array}{r} 60.1 \\ 8.7 \\ 26 \end{array} \begin{array}{r} 59.8 \\ 9.0 \\ 25 \end{array} \begin{array}{r} 60.0 \\ 8.8 \\ 16 \end{array} \begin{array}{r} 61.4 \\ 7.4 \\ 12 \end{array} \begin{array}{r} 61.8 \\ 7.1 \\ 11 \end{array} \begin{array}{r} 61.7 \\ 9.0 \\ 17 \end{array} \begin{array}{r} 59.7 \\ 9.1 \\ 28 \end{array} \begin{array}{r} 60.4 \\ 8.4 \\ 30 \end{array}$$

$$\begin{array}{r} 59.5 \\ 4.7 \\ 27 \end{array} \begin{array}{r} 58.9 \\ 5.3 \\ 26 \end{array} \begin{array}{r} 59.3 \\ 4.9 \\ 16 \end{array} \begin{array}{r} 60.8 \\ 3.4 \\ 11 \end{array} \begin{array}{r} 61.4 \\ 2.8 \\ 11 \end{array} \begin{array}{r} 61.2 \\ 3.0 \\ 16 \end{array} \begin{array}{r} 59.3 \\ 4.2 \\ 28 \end{array} \begin{array}{r} 59.8 \\ 4.9 \\ 29 \end{array} \begin{array}{r} 60.2 \\ 4.0 \\ 29 \end{array}$$

$$\begin{array}{r} 60.9 \\ 2.3 \\ 30 \end{array} \begin{array}{r} 59.5 \\ 4.7 \\ 27 \end{array} \begin{array}{r} 59.3 \\ 4.9 \\ 19 \end{array} \begin{array}{r} 59.8 \\ 4.4 \\ 15 \end{array} \begin{array}{r} 60.3 \\ 3.9 \\ 13 \end{array} \begin{array}{r} 61.0 \\ 3.2 \\ 12 \end{array} \begin{array}{r} 60.5 \\ 3.7 \\ 12 \end{array} \begin{array}{r} 59.5 \\ 4.7 \\ 16 \end{array} \begin{array}{r} 59.3 \\ 4.9 \\ 24 \end{array} \begin{array}{r} 61.8 \\ 2.4 \\ 29 \end{array}$$

$$\begin{array}{r} 61.5 \\ 2.7 \\ 30 \end{array} \begin{array}{r} 59.1 \\ 5.1 \\ 23 \end{array} \begin{array}{r} 59.1 \\ 5.1 \\ 18 \end{array} \begin{array}{r} 59.8 \\ 4.4 \\ 15 \end{array} \begin{array}{r} 60.2 \\ 4.0 \\ 12 \end{array} \begin{array}{r} 60.3 \\ 3.9 \\ 12 \end{array} \begin{array}{r} 60.1 \\ 4.1 \\ 14 \end{array} \begin{array}{r} 59.3 \\ 4.9 \\ 18 \end{array} \begin{array}{r} 59.6 \\ 5.6 \\ 26 \end{array} \begin{array}{r} 60.2 \\ 2.0 \\ 31 \end{array}$$

$$\begin{array}{r} 61.8 \\ 2.4 \\ 28 \end{array} \begin{array}{r} 59.6 \\ 5.0 \\ 24 \end{array} \begin{array}{r} 59.2 \\ 5.0 \\ 17 \end{array} \begin{array}{r} 60.0 \\ 4.2 \\ 13 \end{array} \begin{array}{r} 60.0 \\ 4.2 \\ 13 \end{array} \begin{array}{r} 58.9 \\ 5.3 \\ 17 \end{array} \begin{array}{r} 58.9 \\ 5.3 \\ 25 \end{array} \begin{array}{r} 61.5 \\ 2.2 \\ 30 \end{array}$$

$$\begin{array}{r} 58.8 \\ 5.4 \\ 29 \end{array} \begin{array}{r} 57.5 \\ 6.7 \\ 25 \end{array} \begin{array}{r} 57.8 \\ 6.4 \\ 16 \end{array} \begin{array}{r} 58.9 \\ 5.3 \\ 13 \end{array} \begin{array}{r} 59.6 \\ 4.6 \\ 11 \end{array} \begin{array}{r} 59.1 \\ 5.1 \\ 11 \end{array} \begin{array}{r} 57.5 \\ 6.7 \\ 17 \end{array} \begin{array}{r} 59.4 \\ 6.8 \\ 25 \end{array} \begin{array}{r} 59.2 \\ 5.0 \\ 29 \end{array}$$

$$\begin{array}{r} 56.4 \\ 7.8 \\ 16 \end{array} \begin{array}{r} 58.2 \\ 6.0 \\ 11 \end{array} \begin{array}{r} 58.8 \\ 5.4 \\ 11 \end{array} \begin{array}{r} 58.3 \\ 5.9 \\ 12 \end{array} \begin{array}{r} 56.6 \\ 7.6 \\ 17 \end{array} \begin{array}{r} 56.3 \\ 7.9 \\ 17 \end{array} \begin{array}{r} 57.1 \\ 7.6 \\ 30 \end{array} \begin{array}{r} 57.1 \\ 7.6 \\ 31 \end{array}$$

$$\begin{array}{r} 56.3 \\ 7.9 \\ 17 \end{array} \begin{array}{r} 58.3 \\ 5.9 \\ 12 \end{array} \begin{array}{r} 58.7 \\ 5.8 \\ 12 \end{array} \begin{array}{r} 58.3 \\ 5.8 \\ 16 \end{array} \begin{array}{r} 56.3 \\ 7.9 \\ 16 \end{array} \begin{array}{r} 56.0 \\ 7.9 \\ 19 \end{array} \begin{array}{r} 56.1 \\ 8.4 \\ 29 \end{array} \begin{array}{r} 56.9 \\ 7.3 \\ 31 \end{array}$$

964.24

964.24

B.M. 275+25 Spike in Lone Thistle (38)
at SE. Cor. of House 100' left E. 967.18

285
T.P. 4.98 (968.46) 5.90 963.48

284

283

282

281

280

T.P. 5.17 (969.38) 5.50 964.21
279

278

277

276

275

T.P. 4.80 (969.71) 3.90 964.91
274

(968.8)

64.9 61.9 62.9 63.3 63.7 63.4 62.3 61.4 63.4 ✓
3.6 6.6 5.6 5.2 5.1 6.2 7.1 5.1
28 25 15 11 4.8 12 16 26 28

64.5 61.5 62.5 63.8 (968.5) 63.5 61.9 62.0 60.7 62.6 ✓
7.7 7.9 6.9 5.8 63.9 5.9 7.5 7.4 8.7 6.8
29 26 16 12 5.5 12 16 19 26 28

62.9 61.5 61.6 63.6 63.6 61.0 61.5 61.4 61.6 ✓
6.5 7.9 7.9 5.8 64.1 5.8 8.4 7.9 8.0 7.8
28 26 18 13 5.3 13 19 24 30 31

6.2 61.2 61.2 64.0 63.8 61.6 61.3 61.7 ✓
6.6 7.7 8.2 5.4 64.2 5.6 7.8 8.1 7.7
28 26 18 14 5.2 13 18 21 25

63.6 61.4 62.2 64.2 64.4 64.0 61.9 61.6 62.4 ✓
5.8 8.0 7.2 5.2 5.4 7.5 7.8 7.0
28 26 17 13 5.0 13 18 27 28

63.9 61.6 62.0 64.2 64.7 64.2 64.0 61.8 62.6 ✓
5.5 7.8 7.4 5.2 5.2 7.2 7.6 6.8
28 20 17 13 4.7 14 19 27 28

63.2 61.3 62.2 64.5 (969.4) 64.3 61.7 61.3 62.0 ✓
6.5 8.4 7.5 5.2 64.6 5.4 8.0 8.4 7.7
29 27 17 13 5.1 13 17 27 28

62.9 61.2 62.3 64.1 64.5 64.1 61.8 61.6 62.0 ✓
6.8 8.5 7.4 5.6 5.6 7.9 8.1 7.7
28 27 17 13 5.2 14 19 28 29

63.4 62.1 62.4 64.5 64.8 64.3 62.2 62.2 61.9 62.7 ✓
6.3 7.6 7.3 5.2 5.4 7.6 7.5 7.8 7.0
28 27 18 13 4.9 14 18 24 27 28

64.9 62.4 63.1 64.8 65.2 64.4 63.0 62.9 63.7 ✓
4.8 7.3 6.6 4.9 5.3 6.7 7.0 6.0
28 26 17 12 4.5 13 17 28 29

66.2 63.1 63.4 63.9 64.6 64.8 64.0 63.2 65.7 ✓
3.5 6.6 6.6 5.8 5.1 4.9 5.7 6.5 4.0
28 26 20 14 7.1 11 14 21 19

66.3 64.1 64.1 64.5 64.5 (969.7) 64.7 64.9 65.0 65.4 65.6 66.9 ✓
2.5 4.7 4.7 4.3 4.3 4.1 3.7 3.8 3.4 3.2 1.9
30 27 18 16 14 12 16 20 23 29 31

(968.8)

Figure ditch sec.
Here

B.M. 288+81 Spike in 1/4 Rec. Cor.
Post Left. E.I. 962.91

39

295
T. P. 0.55 960.32 8.22 959.77

294

293

292

291+50

291

290

289+74

289

288

287

286

5.08 967.99 5.62 962.84 962.91

968.46

961.3	58.4	58.3	59.7	59.8	59.8	58.4	59.6		
4.0	1.9	2.0	0.6	0.5	0.5	1.9	0.7		
30	25	20	12	0.5	12	21	29		
61.5	59.7	59.3	59.9	60.8	61.0	60.9	59.5	59.1	60.4
6.5	8.3	8.7	8.1	7.2	7.1	8.5	8.9	7.6	
29	25	21	16	13	7.0	12	17	21	26
61.6	60.5	60.7	61.5	61.9	61.7	60.0	60.0	60.9	
6.4	7.5	7.3	6.5	6.1	6.3	8.0	8.0	7.1	
28	27	17	14	6.1	12	17	22	24	
63.4	61.2	62.0	62.4	62.7	62.6	61.3	62.3		
4.6	6.8	6.0	5.6	5.4	5.4	6.7	5.7		
30	27	16	12	5.3	12	19	24		
63.8	61.2	62.1	62.8	62.9	62.7	61.6	61.7	63.0	
4.2	6.8	5.9	5.2	5.3	5.3	6.4	6.3	5.0	
30	26	16	11	5.1	12	16	21	25	
63.2	61.0	61.1	61.4	62.0	62.9	63.1	62.6	60.8	61.3
4.8	7.0	6.9	6.6	6.0	5.1	5.4	7.2	6.7	6.0
30	27	23	18	16	12	4.9	12	19	23
62.1	60.2	61.0	63.2	63.4	63.0	60.0	60.3	60.5	
5.9	7.8	7.0	4.8	4.6	5.0	8.0	7.7	7.5	
31	27	18	10	4.6	13	18	24	26	
61.8	60.6	60.9	62.1	63.5	63.6	63.3	60.7	62.1	60.6
6.2	7.4	7.1	5.9	4.5	4.7	7.3	5.9	7.4	7.6
30	28	23	15	12	4.4	12	14	19	25
61.7	61.1	60.5	60.9	63.1	63.5	62.9	60.5	60.7	61.4
6.3	6.9	7.5	7.1	4.9	5.1	7.5	7.3	6.9	
31	29	28	21	12	4.5	14	19	26	28
63.7	61.2	62.6	63.0	63.4	63.4	62.0	61.5	63.1	
4.8	7.3	5.9	5.2	5.1	5.1	6.5	7.0	5.4	
30	27	15	12	5.0	11	10	25	28	
61.6	61.4	62.0	63.8	63.5	63.0	62.1	61.3	63.3	
3.9	7.1	6.0	5.2	5.5	5.5	6.4	7.2	5.2	
29	26	19	11	5.0	13	16	25	26	
64.9	61.9	62.8	63.3	63.6	63.4	62.3	61.5	63.5	
3.6	6.8	5.7	5.2	5.1	5.1	6.2	7.0	5.0	
29	26	16	12	4.9	13	17	26	28	

B.M. Sta. 303+23 S.W. Cor. of Walk
(Conc.) at S.W. Cor. of House Left
E1. 955.87 40

305

51.8	49.8	49.7	52.6	52.8	52.7	49.3	48.9
6.2	8.2	8.3	5.4	5.2	5.3	8.7	9.1
33	29	20	12	11	21	31	

304+81

51.9	50.2	50.4	52.5	52.9	52.4	49.6	49.2
6.1	7.8	7.6	5.5	5.6	5.6	8.4	8.8
33	29	20	13	5.1	11	19	28

304

53.0	51.0	51.0	52.5	52.7	52.1	50.4	49.9	50.3	50.7
5.0	7.0	7.0	5.5	5.7	5.9	7.6	8.1	7.7	7.3
33	28	20	15	5.3	12	17	23	26	27

B.M.

2.15

958.02

1.56

955.81

Conc.
955.87

303

53.4	50.4	52.5	52.4	52.4	50.3	50.2	51.4
4.0	7.0	5.2	5.4	5.3	7.1	7.2	6.0
31	21	14	5.0	13	20	25	28

302

52.8	49.9	51.8	52.1	51.6	50.0	49.4	50.3
4.6	7.5	5.6	5.2	5.8	7.4	8.0	7.1
32	22	14	5.3	13	18	23	30

301

50.9	49.7	49.4	51.4	51.9	51.5	49.2
6.5	7.7	8.0	6.0	5.9	5.9	8.2
31	27	20	14	5.5	12	17

957.4

300+86

T.P.

4.35

957.37

7.30

953.02

300

50.9	49.6	49.8	51.5	51.8	51.3	50.7	48.8	48.7	48.8
9.4	10.7	10.5	8.8	8.5	9.0	9.6	11.5	11.6	11.3
31	28	18	14	8.5	12	14	20	25	27

299

52.4	51.3	51.0	51.8	52.5	52.9	52.1	50.3	49.9	50.4
7.9	9.0	9.3	8.5	7.8	8.2	8.2	10.0	10.4	9.9
29	27	20	16	12	14	12	17	21	25

298

54.0	52.7	52.5	53.1	54.0	54.1	54.1	52.3	52.0	52.6	52.9
6.3	7.6	7.8	7.2	6.3	6.2	8.0	8.3	7.7	7.4	
29	27	20	16	12	5.9	11	17	23	24	27

297

56.5	54.4	55.7	55.9	55.9	55.9	55.0	55.6	
3.8	5.9	5.2	4.4	4.4	4.9	5.3	4.7	
30	25	16	12	3.9	11	14	20	27

296

58.9	56.3	57.2	58.2	58.4	58.2	57.6	56.8	57.7
1.4	4.0	3.1	2.1	2.1	2.1	2.7	3.5	2.6
30	25	15	12	19	12	16	21	27

960.31

960.32

B.M. 315+30 Highest point large
Boulder E. side Twp. Rd. 100'S E1. 930.20 41

314+90

29.9 28.8 28.8 31.5 31.6 31.6 30.3
10.4 11.5 11.5 8.8 8.7 8.7 10.0 ✓
30 29 19 13 11 11 27

314

31.6 29.9 30.3 34.0 33.9 30.9 30.7
8.7 10.4 10.0 6.3 6.4 9.4 9.6 ✓
29 27 19 13 11 17 24

313

34.9 34.1 35.0 37.4 37.3 34.0 33.7 35.0
5.4 6.2 5.3 2.9 3.4 3.0 6.3 6.6 5.3 ✓
29 27 17 13 13 18 26 28

312

4.05 940.32 12.23 936.27

40.4 38.5 39.5 41.2 41.3 39.1 38.5 40.8
8.1 10.0 9.0 7.3 7.2 9.4 10.0 7.7 ✓
30 27 18 14 12 18 27 30

311

2.07 948.50 10.48 946.43

47.0 43.7 43.2 44.1 45.3 45.3 44.3 43.3 47.4
1.5 4.8 5.3 4.4 3.2 3.2 4.2 5.2 1.1 ✓
30 27 24 16 13 12 16 25 30

310

51.9 47.6 47.8 48.8 49.4 48.6 47.2 50.5
5.0 9.3 9.1 8.5 7.5 4.5 4.3 6.4 ✓
31 27 21 17 12 11 14 25 30

309

50.2 50.1 50.0 51.1 51.8 51.3 51.7 51.0 50.1 53.0
2.7 6.8 6.3 5.8 5.1 5.2 5.9 6.8 3.9 ✓
31 26 21 15 12 13 16 25 28

308

3.74 956.91 4.85 953.17

50.1 50.4 49.9 50.7 53.5 53.4 52.7 52.1 55.9
0.8 4.5 5.0 4.2 3.4 3.5 4.2 4.8 1.0 ✓
31 27 24 15 12 13 16 24 29

307+46

52.7 52.1 52.6 53.7 53.8 53.1 52.5 56.2
1.3 5.9 5.4 4.3 4.2 4.9 5.5 1.8 ✓
30 26 17 13 13 17 23 31

307

55.5 52.3 52.6 53.6 53.7 53.7 52.9 52.5 55.7
2.5 5.1 5.4 4.4 4.3 4.3 5.1 5.5 2.3 ✓
31 25 18 13 13 16 24 31

306

53.3 51.3 51.9 53.1 53.5 53.2 51.4 51.2 52.2
4.7 6.7 6.1 4.9 4.8 4.8 6.6 6.8 5.8 ✓
32 26 16 13 13 15 26 30

958.02

958.0

323

322

321

320

319

318

317

316

315+27

315+24

B.M.
315+16

315

1.97

916.88

11.65

914.91

1.04

926.56

9.78

925.52

5.10

935.30

5.10

930.17

Corr.
930.20

4.54

935.17

9.59

930.73

(940.32)

10.9	08.9	09.4	10.7	10.6	10.6	08.1	08.9	12.2
6.0	8.0	7.5	6.2	6.3	6.3	7.8	8.0	4.7
30	29	16	11	12	16	26	29	

15.6	13.1	13.4	14.8	14.5	14.7	13.4	13.0	15.9
1.3	3.8	3.5	2.1	2.4	2.2	3.5	3.9	1.0
30	27	16	12	12	19	27	29	

19.7	16.4	16.2	17.2	17.6	19.0	18.6	18.0	17.0	20.0
6.9	10.2	10.4	9.4	9.0	7.6	8.3	8.0	9.6	6.6
30	28	22	20	15	11	12	15	27	29

24.4	20.1	20.1	21.5	22.0	22.8	22.6	22.8	22.2	21.6	20.8	23.8
2.2	6.5	6.5	5.1	4.6	3.8	4.0	3.8	4.4	5.0	5.8	2.8
31	28	21	20	15	12	12	15	21	27	29	

28.3	23.3	24.8	26.0	25.9	26.2	25.3	24.0	25.9
7.0	12.0	10.5	9.3	9.3	9.3	10.0	11.3	9.4
30	27	20	13	14	15	27	29	

30.4	27.5	26.8	27.9	29.0	28.6	28.7	27.2	26.1	27.2
4.9	7.8	8.5	7.4	6.3	6.7	6.6	8.1	9.2	8.1
31	28	24	18	12	12	16	27	28	

31.1	27.6	28.6	29.7	29.5	27.2	26.5	27.7
4.2	7.7	6.7	5.6	5.8	8.1	8.8	7.6
31	27	19	11	13	17	27	29

31.1	28.0	28.5	28.7	30.3	30.1	28.8	26.9	26.5	27.0
4.2	7.3	6.8	6.6	5.0	5.2	5.5	8.4	8.8	8.3
31	27	21	15	12	12	18	25	26	

Same as +16

31.0	30.9	30.4	28.6	28.0
4.3	4.4	4.9	6.7	7.3
14	21	28	30	

Same as +16

31.1	30.9	30.0	28.1	27.2
4.7	4.9	5.3	7.2	7.5
12	27	35		

30.0	28.6	28.6	31.2	30.9	30.6	29.9
5.3	6.7	6.7	4.1	4.5	4.7	5.4
30	29	19	14	17	31	46

30.1	28.6	28.6	31.3	31.3	30.5	30.1
10.2	11.7	11.7	9.0	9.4	9.8	10.2
30	28	19	14	11	24	39

(940.3)

B.M. 326+25 Spike in 1st. Tel. pole
S. of Rev. Left. El. 903.50

43

T.P. 10.91 922.03 1.93 911.12
331

330

329

328

327

B.M. 9.55 (913.05) 6.61 903.40 903.50
326

325+66

325+26

325+20

325

+30

324

0.37 (910.01) 7.24 909.64

(916.88)

913.0 06.6 9.0 09.5 10.5 11.6 11.6 11.3 10.5 09.1 08.8 08.5 12.0 ✓
+00 4.4 4.0 3.5 2.5 1.4 1.4 1.7 2.5 3.9 4.2 4.5 1.0
31 28 23 22 15 13 1.4 11 13 21 22 27 30

07.9 06.5 07.1 08.4 09.2 06.9 06.6 07.2 ✓
5.1 6.5 5.9 3.6 09.2 3.8 6.1 6.4 5.8
31 30 18 13 3.5 13 18 28 28

05.9 05.4 05.0 07.4 07.5 07.4 04.5 04.4 ✓
7.1 7.9 8.0 5.6 07.5 5.6 8.5 8.6
31 30 19 14 5.5 13 19 22

05.9 08.2 03.5 06.8 06.7 06.7 03.1 03.0 ✓
7.1 9.8 9.5 6.2 06.7 6.3 9.9 10.0
32 24 20 15 6.3 13 20 23

08.8 07.0 07.1 07.2 07.4 ✓
10.2 6.0 07.0 5.9 10.8 10.6
22 14 6.0 12 21 25

02.0 02.4 07.6 (913.0) 02.0 02.0 ✓
8.0 7.6 2.4 08.0 07.7 8.0
24 22 13 2.0 12 21

01.7 05.1 07.7 07.7 07.7 01.7 ✓
8.3 4.9 2.3 07.7 2.3 8.3
19 13 6 2.3 7 17

00.8 00.2 05.3 06.9 07.6 07.6 03.0 ✓
7.2 9.8 4.7 06.9 2.4 07.7 2.4 7.0
32 26 13 31 12 7 2.3 6 17

02.6 02.2 08.1 08.1 08.2 02.5 ✓
7.4 7.8 1.9 08.1 1.8 7.5
31 25 11.9 12 22

04.5 05.1 08.3 08.4 08.4 04.3 04.4 05.2 ✓
5.5 4.4 1.7 08.4 08.4 5.7 5.6 4.8
32 18 11.6 11 19 26 27

06.2 05.9 06.1 09.1 (910.0) 08.7 06.7 06.4 ✓
10.7 11.0 10.8 1.8 08.7 8.2 10.2 10.3
32 30 17 11 8.2 11 17 27
(916.8)

+26

+18

341

11,08

(952.91)

181

941.83

340

339

 $338 + 50$

12.45

943.64

2.90

931.19

338

337

336

T.P.

12.81

934.09

0.75

921 28

335

334

333

33v

922.03

922.00

94

351

350

10.76

969.17

2.35

958.43

349

348

347

346

345

Nail in Tel. pole 10.14

960.78

2.36

950.64

344

343

342

4.05

953.00

4.05

948.86

948.95

+63

+55

+42

952.71

$\begin{array}{r} 64.2 \\ 5.0 \\ 30 \end{array}$
 $\begin{array}{r} 62.2 \\ 7.0 \\ 27 \end{array}$
 $\begin{array}{r} 61.8 \\ 7.4 \\ 23 \end{array}$
 $\begin{array}{r} 61.5 \\ 7.7 \\ 21 \end{array}$
 $\begin{array}{r} 61.7 \\ 7.5 \\ 15 \end{array}$
 $\begin{array}{r} 63.0 \\ 6.2 \\ 11 \end{array}$
 $\begin{array}{r} 62.1 \\ 6.1 \\ 6.1 \end{array}$
 $\begin{array}{r} 67.6 \\ 6.6 \\ 13 \end{array}$
 $\begin{array}{r} 61.6 \\ 7.6 \\ 17 \end{array}$
 $\begin{array}{r} 61.2 \\ 8.0 \\ 28 \end{array}$
 $\begin{array}{r} 67.1 \\ 7.1 \\ 31 \end{array}$

$\begin{array}{r} 63.0 \\ 6.2 \\ 30 \end{array}$
 $\begin{array}{r} 61.3 \\ 7.9 \\ 27 \end{array}$
 $\begin{array}{r} 60.7 \\ 8.5 \\ 23 \end{array}$
 $\begin{array}{r} 60.2 \\ 9.0 \\ 20 \end{array}$
 $\begin{array}{r} 60.1 \\ 9.1 \\ 15 \end{array}$
 $\begin{array}{r} 61.4 \\ 7.8 \\ 11 \end{array}$
 $\begin{array}{r} 61.3 \\ 7.9 \\ 7.9 \end{array}$
 $\begin{array}{r} 61.1 \\ 8.1 \\ 12 \end{array}$
 $\begin{array}{r} 59.7 \\ 9.5 \\ 17 \end{array}$
 $\begin{array}{r} 59.5 \\ 9.7 \\ 23 \end{array}$
 $\begin{array}{r} 60.2 \\ 9.0 \\ 24 \end{array}$

$\begin{array}{r} 59.6 \\ 1.2 \\ 30 \end{array}$
 $\begin{array}{r} 58.4 \\ 2.4 \\ 24 \end{array}$
 $\begin{array}{r} 57.8 \\ 3.0 \\ 17 \end{array}$
 $\begin{array}{r} 58.9 \\ 1.9 \\ 12 \end{array}$
 $\begin{array}{r} 58.3 \\ 2.0 \\ 20 \end{array}$
 $\begin{array}{r} 58.9 \\ 1.9 \\ 13 \end{array}$
 $\begin{array}{r} 57.8 \\ 3.9 \\ 16 \end{array}$
 $\begin{array}{r} 57.8 \\ 3.0 \\ 27 \end{array}$
 $\begin{array}{r} 59.1 \\ 1.7 \\ 32 \end{array}$

$\begin{array}{r} 56.6 \\ 4.2 \\ 30 \end{array}$
 $\begin{array}{r} 54.9 \\ 5.9 \\ 26 \end{array}$
 $\begin{array}{r} 55.3 \\ 5.5 \\ 16 \end{array}$
 $\begin{array}{r} 56.6 \\ 4.2 \\ 11 \end{array}$
 $\begin{array}{r} 56.8 \\ 4.0 \\ 4.0 \end{array}$
 $\begin{array}{r} 56.7 \\ 4.1 \\ 12 \end{array}$
 $\begin{array}{r} 55.4 \\ 5.4 \\ 17 \end{array}$
 $\begin{array}{r} 55.2 \\ 5.6 \\ 27 \end{array}$
 $\begin{array}{r} 57.0 \\ 3.8 \\ 31 \end{array}$

$\begin{array}{r} 53.9 \\ 6.9 \\ 30 \end{array}$
 $\begin{array}{r} 53.0 \\ 7.8 \\ 27 \end{array}$
 $\begin{array}{r} 52.0 \\ 7.8 \\ 21 \end{array}$
 $\begin{array}{r} 53.5 \\ 7.3 \\ 16 \end{array}$
 $\begin{array}{r} 54.7 \\ 6.1 \\ 11 \end{array}$
 $\begin{array}{r} 54.2 \\ 6.2 \\ 6.1 \end{array}$
 $\begin{array}{r} 54.6 \\ 6.2 \\ 12 \end{array}$
 $\begin{array}{r} 53.2 \\ 7.6 \\ 17 \end{array}$
 $\begin{array}{r} 53.1 \\ 7.7 \\ 24 \end{array}$
 $\begin{array}{r} 55.5 \\ 5.3 \\ 30 \end{array}$

$\begin{array}{r} 52.6 \\ 8.2 \\ 30 \end{array}$
 $\begin{array}{r} 51.0 \\ 7.8 \\ 23 \end{array}$
 $\begin{array}{r} 50.9 \\ 9.9 \\ 20 \end{array}$
 $\begin{array}{r} 51.5 \\ 9.3 \\ 18 \end{array}$
 $\begin{array}{r} 51.8 \\ 9.0 \\ 15 \end{array}$
 $\begin{array}{r} 53.0 \\ 7.8 \\ 11 \end{array}$
 $\begin{array}{r} 53.0 \\ 7.8 \\ 11 \end{array}$
 $\begin{array}{r} 52.9 \\ 7.9 \\ 4.0 \end{array}$
 $\begin{array}{r} 51.4 \\ 9.4 \\ 17 \end{array}$
 $\begin{array}{r} 51.2 \\ 9.6 \\ 24 \end{array}$
 $\begin{array}{r} 54.2 \\ 6.6 \\ 30 \end{array}$

$\begin{array}{r} 50.1 \\ 10.7 \\ 29 \end{array}$
 $\begin{array}{r} 49.6 \\ 11.2 \\ 27 \end{array}$
 $\begin{array}{r} 50.1 \\ 10.7 \\ 15 \end{array}$
 $\begin{array}{r} 51.0 \\ 9.8 \\ 9.8 \end{array}$
 $\begin{array}{r} 51.5 \\ 9.1 \\ 11 \end{array}$
 $\begin{array}{r} 51.7 \\ 9.1 \\ 12 \end{array}$
 $\begin{array}{r} 50.3 \\ 10.8 \\ 17 \end{array}$
 $\begin{array}{r} 50.1 \\ 10.7 \\ 24 \end{array}$
 $\begin{array}{r} 52.1 \\ 8.7 \\ 30 \end{array}$
 $\begin{array}{r} 52.4 \\ 8.4 \\ 33 \end{array}$

$\begin{array}{r} 48.7 \\ 4.3 \\ 29 \end{array}$
 $\begin{array}{r} 47.9 \\ 5.1 \\ 27 \end{array}$
 $\begin{array}{r} 47.8 \\ 5.2 \\ 23 \end{array}$
 $\begin{array}{r} 48.3 \\ 4.7 \\ 17 \end{array}$
 $\begin{array}{r} 50.1 \\ 6.1 \\ 11 \end{array}$
 $\begin{array}{r} 50.3 \\ 6.3 \\ 2.7 \end{array}$
 $\begin{array}{r} 50.4 \\ 6.4 \\ 11 \end{array}$
 $\begin{array}{r} 50.0 \\ 3.0 \\ 14 \end{array}$
 $\begin{array}{r} 49.0 \\ 4.0 \\ 16 \end{array}$
 $\begin{array}{r} 48.6 \\ 4.4 \\ 19 \end{array}$
 $\begin{array}{r} 49.0 \\ 4.4 \\ 24 \end{array}$
 $\begin{array}{r} 51.0 \\ 2.0 \\ 30 \end{array}$

$\begin{array}{r} 48.5 \\ 4.5 \\ 30 \end{array}$
 $\begin{array}{r} 47.2 \\ 5.8 \\ 27 \end{array}$
 $\begin{array}{r} 47.0 \\ 6.0 \\ 24 \end{array}$
 $\begin{array}{r} 47.3 \\ 5.7 \\ 20 \end{array}$
 $\begin{array}{r} 47.5 \\ 5.5 \\ 16 \end{array}$
 $\begin{array}{r} 49.0 \\ 4.0 \\ 11 \end{array}$
 $\begin{array}{r} 49.1 \\ 3.9 \\ 3.9 \end{array}$
 $\begin{array}{r} 49.1 \\ 3.9 \\ 12 \end{array}$
 $\begin{array}{r} 47.8 \\ 5.2 \\ 16 \end{array}$
 $\begin{array}{r} 47.5 \\ 5.5 \\ 18 \end{array}$
 $\begin{array}{r} 47.4 \\ 5.6 \\ 22 \end{array}$
 $\begin{array}{r} 50.8 \\ 2.2 \\ 30 \end{array}$

$\begin{array}{r} 46.9 \\ 6.1 \\ 30 \end{array}$
 $\begin{array}{r} 45.6 \\ 7.4 \\ 26 \end{array}$
 $\begin{array}{r} 46.0 \\ 7.0 \\ 18 \end{array}$
 $\begin{array}{r} 47.4 \\ 5.6 \\ 13 \end{array}$
 $\begin{array}{r} 47.6 \\ 5.4 \\ 9 \end{array}$
 $\begin{array}{r} 47.8 \\ 5.2 \\ 5.2 \end{array}$
 $\begin{array}{r} 48.0 \\ 5.0 \\ 11 \end{array}$
 $\begin{array}{r} 46.6 \\ 6.4 \\ 16 \end{array}$
 $\begin{array}{r} 46.4 \\ 6.6 \\ 21 \end{array}$
 $\begin{array}{r} 49.6 \\ 3.4 \\ 29 \end{array}$

$\begin{array}{r} 46.0 \\ 6.9 \\ 30 \end{array}$
 $\begin{array}{r} 45.2 \\ 7.7 \\ 29 \end{array}$
 $\begin{array}{r} 44.8 \\ 8.1 \\ 26 \end{array}$
 $\begin{array}{r} 45.2 \\ 7.7 \\ 19 \end{array}$
 $\begin{array}{r} 46.6 \\ 6.5 \\ 14 \end{array}$
 $\begin{array}{r} 46.5 \\ 6.5 \\ 11 \end{array}$
 $\begin{array}{r} 47.0 \\ 5.9 \\ 11 \end{array}$
 $\begin{array}{r} 46.4 \\ 6.5 \\ 23 \end{array}$
 $\begin{array}{r} 46.5 \\ 6.4 \\ 26 \end{array}$
 $\begin{array}{r} 46.0 \\ 6.9 \\ 30 \end{array}$
 $\begin{array}{r} 45.8 \\ 7.1 \\ 34 \end{array}$

$\begin{array}{r} 46.0 \\ 6.9 \\ 31 \end{array}$
 $\begin{array}{r} 44.8 \\ 8.1 \\ 28 \end{array}$
 $\begin{array}{r} 44.7 \\ 8.2 \\ 26 \end{array}$
 $\begin{array}{r} 45.3 \\ 7.6 \\ 17 \end{array}$
 $\begin{array}{r} 46.4 \\ 6.5 \\ 13 \end{array}$
 $\begin{array}{r} 46.5 \\ 6.4 \\ 6.4 \end{array}$
 $\begin{array}{r} 46.6 \\ 6.3 \\ 10 \end{array}$
 $\begin{array}{r} 47.0 \\ 5.9 \\ 20 \end{array}$
 $\begin{array}{r} 46.6 \\ 6.3 \\ 33 \end{array}$

$\begin{array}{r} 45.7 \\ 7.2 \\ 31 \end{array}$
 $\begin{array}{r} 44.3 \\ 8.6 \\ 27 \end{array}$
 $\begin{array}{r} 44.8 \\ 8.1 \\ 17 \end{array}$
 $\begin{array}{r} 46.2 \\ 6.7 \\ 12 \end{array}$
 $\begin{array}{r} 46.0 \\ 6.9 \\ 9 \end{array}$
 $\begin{array}{r} 46.3 \\ 6.3 \\ 6.6 \end{array}$
 $\begin{array}{r} 46.6 \\ 6.3 \\ 14 \end{array}$
 $\begin{array}{r} 47.5 \\ 5.4 \\ 33 \end{array}$

952.9

363

1.48

949.71

12.52

948.23

362

361+50

361

360

359

1.11

960.75

9.61

959.64

358

357

356

355

4.73

969.25

4.73

964.46

964.52

354

353

352

969.19

sta. 354+60

Post RT.

80.964.52

46

47.7	44.7	46.2	46.2	46.6	46.7	46.7	45.0	44.9	47.6	✓
50.0	50.0	45.3	36.3	31.0	30.0	4.7	4.8	2.1		
30	27	15	13	9	12			30		
8.6	50.0	47.9	46.1	48.5	49.7	49.6	48.6	47.8	51.8	✓
31	30	27	19	16	14	12	13	15	27	29
53.7	48.9	50.8	51.1	51.1	51.1	50.3	50.1	50.2	49.8	✓
7.0	11.8	9.9	9.0	9.6	9.6	10.4	10.6	10.5	10.9	12.0
31	26	17	14	9.6	12	14	18	19	21	24
48.6	60.4	60.7	61.3	62.6	62.6	61.8	61.7	60.7	62.3	✓
6.2	10.3	10.0	9.4	8.1	8.2	8.9	9.0	10.0	8.4	
32	27	22	16	13	12	15	20	27	28	
65.3	60.5	62.9	63.9	65.5	66.2	65.0	64.2	63.1	63.8	✓
5.4	8.2	7.8	6.8	5.2	5.2	5.7	6.5	7.6	6.9	
31	28	22	17	13	5.5	13	17	27	29	
57.9	58.1	55.9	56.2	56.8	57.7	57.4	56.5	55.8	55.7	✓
2.8	4.9	5.2	4.8	4.5	3.9	3.0	3.5	4.2	4.9	5.0
32	29	24	22	17	15	12	3.3	12	14	30
60.2	58.3	58.0	58.1	59.7	59.7	58.4	57.4	56.6	56.4	✓
9.0	10.9	11.2	11.1	9.5	9.5	9.8	10.8	11.8	12.6	12.8
31	29	26	17	12	9.7	12	15	20	26	30
61.5	60.1	59.3	59.0	59.6	61.0	60.9	60.7	59.3	58.4	58.2
7.7	9.1	9.7	10.2	9.6	8.2	8.2	9.9	10.8	11.0	✓
32	30	26	25	16	12	8.3	12	18	26	30
62.1	60.8	60.6	62.0	60.4	61.1	61.9	61.6	60.9	60.1	59.7
7.1	8.4	8.6	9.2	8.8	8.1	7.3	6.2	7.6	8.3	9.1
32	30	24	23	18	14	11	7.2	12	14	20
62.7	61.6	61.5	61.1	61.7	62.6	62.6	60.9	60.4	60.5	✓
6.3	7.6	7.7	8.1	7.3	6.6	6.6	8.3	8.8	8.7	
32	31	25	24	15	14	12	19	24	31	
63.7	62.1	62.3	62.5	62.5	62.5	62.5	62.0	62.5	62.5	✓
5.5	7.1	6.9	5.7	5.7	5.7	6.7	7.2	6.7	6.7	
31	30	18	13	5.6	11	15	27	30		
64.4	62.6	63.5	62.2	62.7	63.8	63.9	62.4	62.3	62.8	63.7
4.8	6.6	5.7	6.3	6.5	5.4	5.3	6.8	6.9	6.4	5.5
29	27	23	21	16	13	5.3	12	19	25	31
64.6	63.1	62.4	62.5	63.2	63.5	62.2	61.7	63.2	63.2	✓
4.6	6.1	6.8	6.7	5.5	5.5	5.7	7.0	7.5	6.0	
29	27	20	17	12	5.5	13	18	26	31	

969.2

370

369

10.87

955.14

4.035

944.27

P.T. +52.6

368

+50

367

+57.5

+50.

+44.

+37

T.P.

366

365

364

10.48

948.31

11.87

937.84

B.M.

949.71

48.5	45.7	45.7	47.1	41.5	47.2
6.6	9.4	9.4	8.0	7.9	7.9
26	20	18	13	7.6	13

46.1	43.6	43.9	44.2	45.0	955.1	45.1	45.0	44.2	44.4
2.2	4.5	4.4	4.1	3.3	45.1	45.0	44.2	44.4	44.4
29	24	19	17	15	32	33	31	3.9	3.9
						14	16	20	

43.4	41.0	41.0	41.5	42.7	42.8	42.7	41.9	41.2
4.9	7.3	7.3	6.8	5.6	5.5	5.6	6.4	7.1
30	25	22	19	14		19	21	31

40.6	39.1	39.0	40.7	40.1	40.4	39.4	38.5
2.2	9.2	9.3	7.6	7.6	7.9	8.2	9.8
30	28	19	14		23	26	31

38.3	37.5	37.5	39.1	39.4	39.2	35.4
10.0	10.8	10.8	9.2	8.9	9.1	12.9
32	30	18	14		14	24

36.5	36.2	38.8	39.2	38.9	35.3	34.8
11.8	12.1	9.5	9.1	9.4	13.0	13.5
30	16	11		15	22	32

36.3	35.8	35.9	38.6	39.1	38.8	35.5	34.9
12.0	12.5	12.4	9.7	9.2	9.5	12.8	13.4
29	20	15	11		16	19	24

37.8	38.5	39.0	38.9	37.9
12.5	9.8	9.3	9.4	10.4
14	12		16	17

36.4	36.1	35.8	34.5	38.6	39.0	38.7	35.8	35.1	34.9
11.9	12.0	12.5	13.8	9.8	9.3	9.6	12.5	13.2	13.4
29	28	23	19	13		15	19	26	39

36.7	36.1	36.3	38.6	948.3	36.2	35.2
13.0	13.6	13.4	11.1	10.7	10.5	14.2
29	28	18	13		13	33

38.0	37.6	37.9	40.5	40.5	40.6	38.3	38.3	38.8
11.7	12.1	11.8	9.2	9.2	9.1	11.5	11.4	10.9
29	27	19	13		14	19	29	33

42.5	41.2	41.4	43.2	43.4	43.4	41.8	41.7	42.0
12.3	8.5	8.3	6.5	6.3	6.3	10.8	8.0	7.1
29	27	16	13		14	19	29	30

949.7

Spr. Creek Sec. 10-11
 Tile line down center
 of roadway near middle
 of mile.

5450	4.24	101.27	98.30	— 2.97	2'-11½"
5	4.24	101.27	98.04	3.23	3'-3"
4	4.67	100.84	97.78	3.06	3'-1"
3	5.05	100.46	97.52	2.94	2'-11½"
2	5.40	100.11	97.26	2.85	2'-10"
1	5.53	99.98	97.00	2.98	3'-0"
0+25.	5.48	100.03	96.80	— 3.23	3'-3"
0	8.23	97.28	96.5	0.78	0'-9½"

B.M. 5.51 105.51 100.00

Outlet-south end of
 line, on East side of
 road.

Tile Line down
Center of Co. Road
Spr. Creek Twp Sec. 10-11
near middle

Sept. 5, 1924
Spencer
Wilde.

1			6.25	99.65	0.30
B.M.			6.11	99.89	0.21
5+50			4.77	101.13	98.30
5			4.75	101.15	98.04
4	5.18	105.90	4.43	100.72	97.98
3			4.75	100.40	97.52
2			4.99	100.16	97.26
1			5.20	99.95	97.00
0+25			5.21	99.94	96.80
0			7.97	97.18	96.50
B.M.	5.15	105.15		100.00	

0.26% grade

2.83	2'-10"
3.11	3'-1 1/2"
2.94	2'-11 1/2"
2.88	2'-10 1/2"
2.90	2'-11"
2.95	2'-11 1/2"
3.14	3'-2"
0.68	0'-8 1/2"

See Page
48

Oak
Tree

38.5

x Stone & Stake

39.0

Tel. pole

NE Corn

Sec. 27-87-11

Spr. Creek Twp.

Sept. 5, 1924

Krog Pit

0+75

0+70

0+50

0+25

0+13

0
-3'

100.00

+23 +0.8 0.2
8 11

2.0 3.7 3.3
11 84 90

100.8 99.5 99.6 97.4 96.0 95.0 95.7
+0.8 0.5 0.4 2.6 4.0 5.0 4.3
10 12 16 55 79 96 97
99.6 98.0 98.8 98.9 97.1 95.7 94.3 93.9 94.2
0.4 2.0 1.2 1.1 2.9 4.3 5.7 6.1 5.8
10 13 14 20 56 80 98 106 108
99.3 96.2 95.5 93.0 92.9 92.6 92.3 92.3 93.9
0.3 3.8 4.5 7.0 7.1 7.4 7.7 7.3 6.1
8 14 20 32 48 45 100 107 109
99.5 93.7 92.0 93.0 91.2 90.8 91.7 93.0
0.5 6.3 8.0 4.3 7.0 8.8 9.2 8.3 1.0
6 6 8 43 62 91 111 112 117
98.6 92.8 92.0 91.4 90.8 90.5 91.7 91.7
0.7 1.4 1.8 0.4 0.8 0.5 0.7 0.7
0 8 20 34 44 61 78 100 113 114
99.9 99.2 98.6 98.5 98.4 98.5 98.7 98.6
0.1 0.5 0.4 0.3 0.4 0.5 0.7 0.6
0 7 13 21 27 33 40 46 53
2.6 93.4 92.7 91.6 91.4 91.5 90.7 91.4
1.4 6.6 7.3 8.4 8.2 8.5 8.6 8.6
23 45 83 100 114

10 yds. off of corner

Lester Twp. sec. 26-35

Sept. 6, 1924. 51

Johnston
Spencer
Wilde

18+48.5 E. end Main Br.

16+94.9 ∇ W. end Main Br.

91.5
16+03.4 Δ $\angle 38^\circ 26'$ Right W. end Br.
 $\angle 38^\circ 38'$ Right E. end of Main.

15+31 Cross Fence

12+81.3 Δ $\angle 54^\circ 38'$ Left

11+29.2 E. end Br. East Bank

10+51.2 W. end Prop. Br.

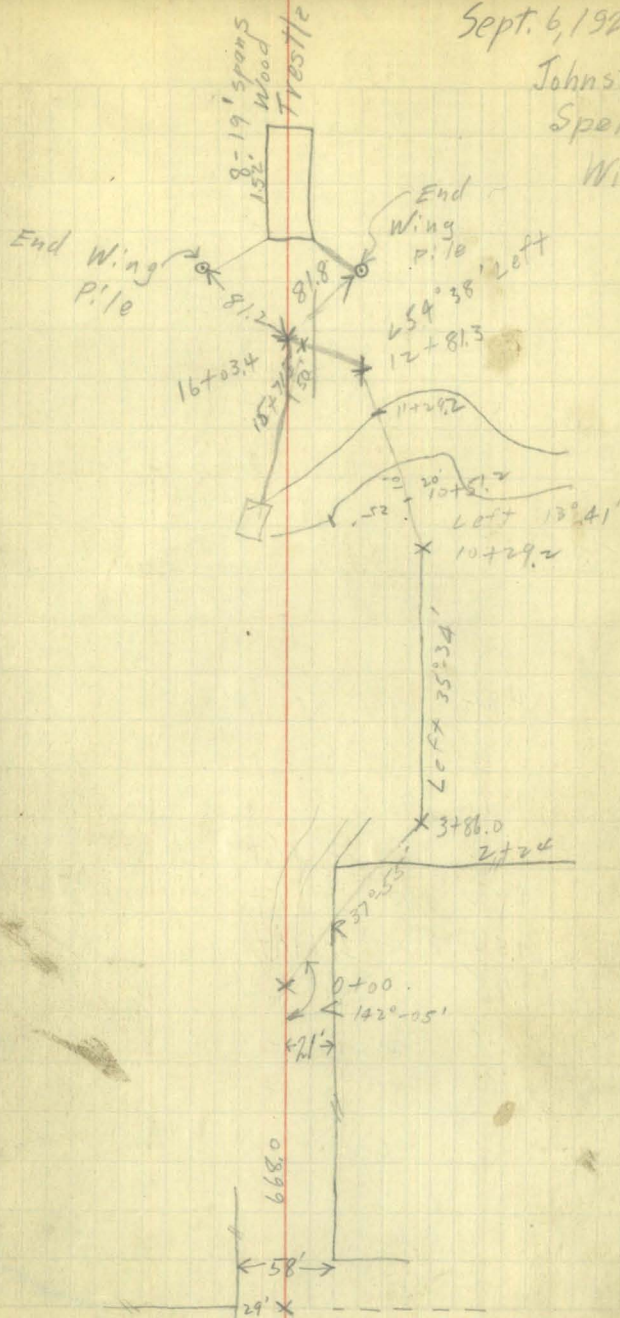
10+29.2A $\angle$ Left $13^\circ 41'$

3+86.0 Δ $\angle$ Left $35^\circ 34'$

2+24 N.Y.S. Fence

0+00 $\angle$ Rt. $37^\circ 55'$

668.0 to starting point



Dist.

Azi.

1

5.78

63° 02' Rt.

E Wood Br.

12+81.3

0° 00' Back site

15+71.5 Δ

9

4.84

111° 07'

Over Flow Wood Br.

8

2.36

94° 10'

Bank

7

1.97

100° 05'

Fence

6

1.63

80° 32' Rt.

Creek Bank

5

1.52

80° 32' Rt.

Fence

4

1.56

41° 31' Rt.

Edge Wash - Creek Bank

3

1.45

41° 31' Rt.

Fence

2

2.48

20° 10' Rt.

Bank Creek

1

2.14

15° 00' Rt.

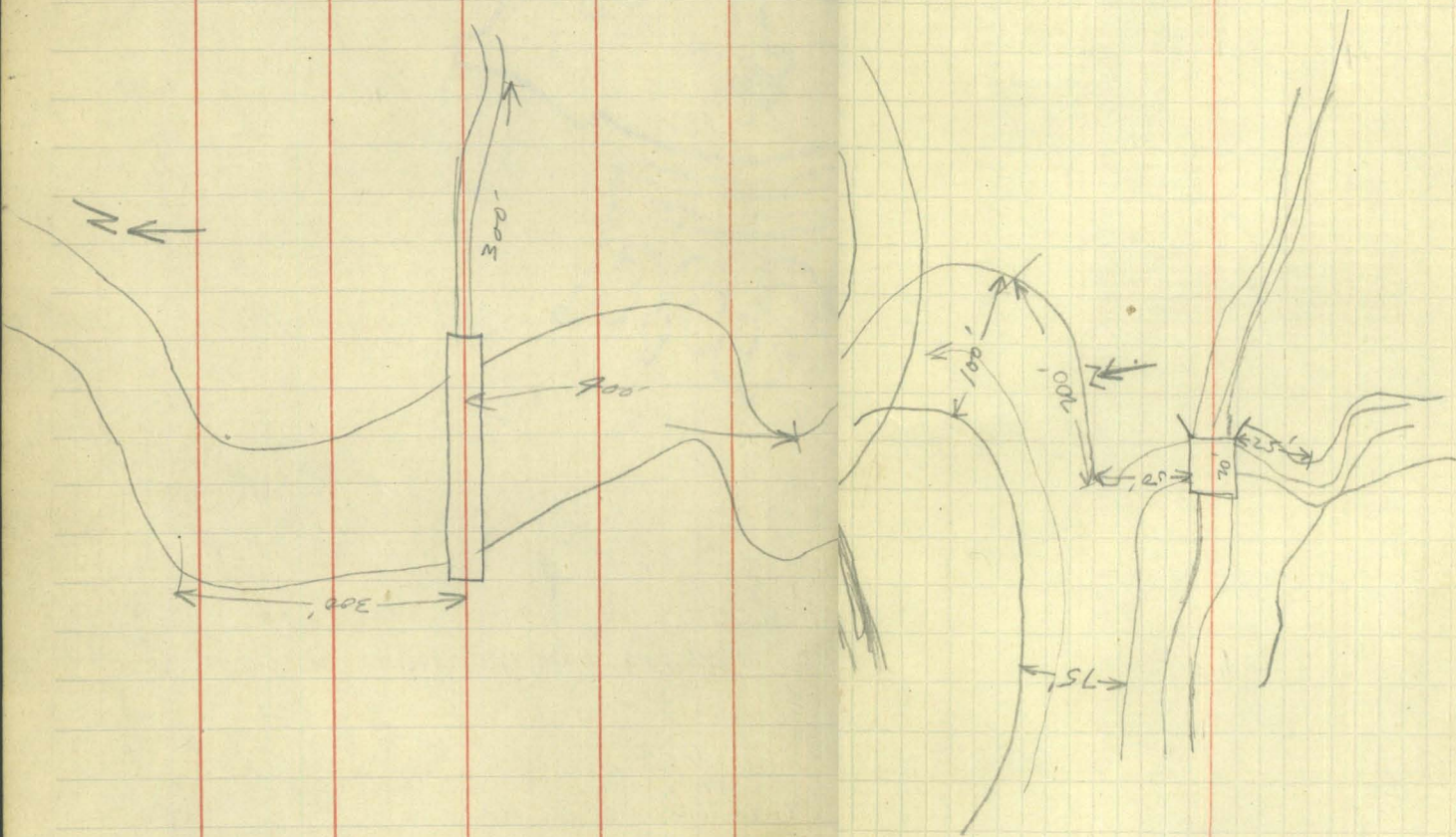
Fence Corner

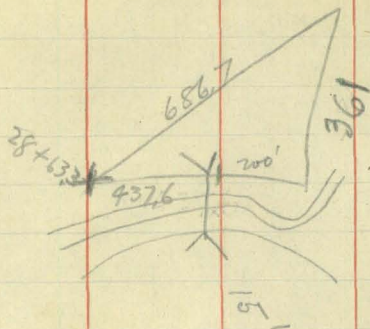
Sta. 0+00

0° 00' Back site

Δ 3+86.0

Lester Sec. 26-35

Sketch of OverFlow Br.
on Wapsie Br.



35+50 Δ End on Fence Line

29 In Corn.

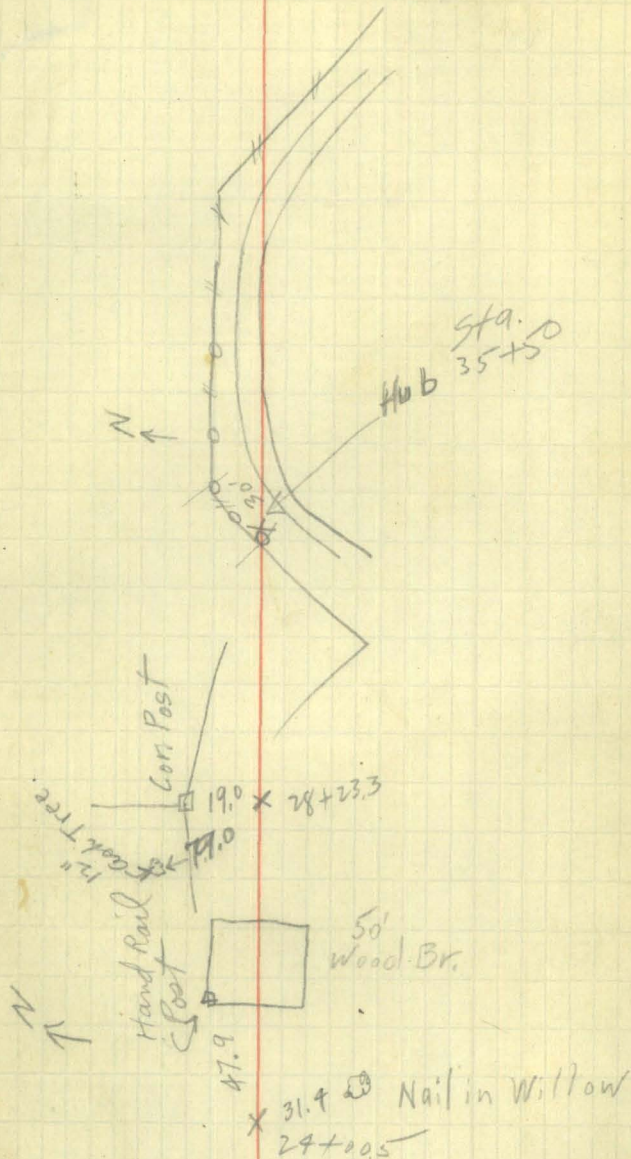
28 + 63.3 E & W. Fence

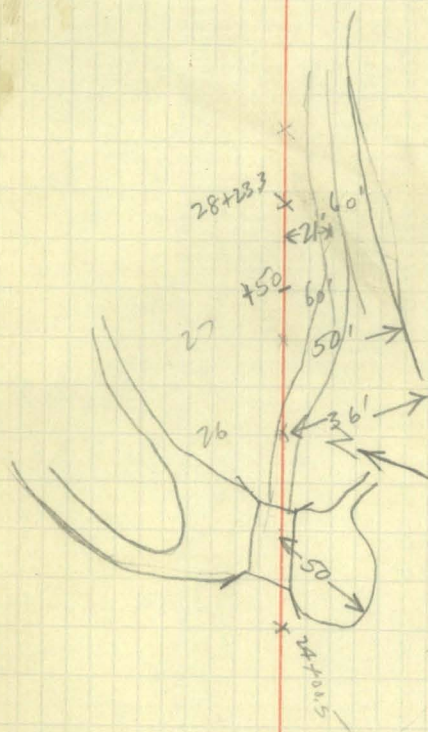
$28 + 23.3 \Delta \angle \text{Right } 14^\circ 27'$

24+97 E. end Br,

24 + 47 W. end Wood Br.

2A + 00.5 Δ L Left 13° 33'





Check on Stadia Readings

Chain
Dist. Rod
Intersep.

1	114	1.12
2	214	2.12
3	314	3.11
4	414	4.11

W. C. Branchorst Pit
Re-Cross Section

Oct. 7, 1924

Spencer
C. Weepie

2+02 Same as 2+00

2+00

1+50

1+00

0+50.0

B.M.

2.41

102.41

100.00

95.9 6.5 0	95.9 6.5 8	95.2 7.2 10	94.7 7.7 32	94.5 7.9 44	94.6 7.8 50	94.6 7.8 63	94.7 7.7 76
98.0 4.4 0	97.7 4.7 2	96.8 5.6 3	97.0 5.4 24	97.2 5.2 36	97.4 5.0 49	97.1 5.3 60	96.4 6.0 6
98.9 3.5 0	98.9 3.5 2	98.3 4.1 3	97.6 4.8 19	97.2 5.2 30	97.3 5.1 40	97.6 4.8 43	97.8 4.6 51
98.1 4.3 0	98.0 4.4 5	97.9 4.5 6	97.3 5.1 7	96.6 5.8 11	96.8 5.6 23	96.9 5.5 31	96.7 5.7 33

102.4

Wapsie
Lester Sec.

57

Sept. 9, 1924

T.P. 3.72 103.21 8.00 99.49

5+48

5

4

3+86

3

2+33

2

1

0+35

0+23

0+00

100' West

B.M.

7.49

107.49

100.00

$\begin{array}{r} 98.8 \\ 8.7 \\ \hline 50 \end{array}$ $\begin{array}{r} 97.9 \\ 8.6 \\ \hline 50 \end{array}$ $\begin{array}{r} 99.1 \\ 8.4 \\ \hline 50 \end{array}$ $\begin{array}{r} 99.4 \\ 8.1 \\ \hline 50 \end{array}$

$\begin{array}{r} 99.7 \\ 7.8 \\ \hline 50 \end{array}$ $\begin{array}{r} 99.7 \\ 7.8 \\ \hline 50 \end{array}$ $\begin{array}{r} 99.6 \\ 7.9 \\ \hline 50 \end{array}$

$\begin{array}{r} 99.6 \\ 7.9 \\ \hline 50 \end{array}$ $\begin{array}{r} 99.4 \\ 8.1 \\ \hline 50 \end{array}$ $\begin{array}{r} 99.4 \\ 8.1 \\ \hline 50 \end{array}$

$\begin{array}{r} 99.6 \\ 7.9 \\ \hline 50 \end{array}$ $\begin{array}{r} 99.5 \\ 8.0 \\ \hline 50 \end{array}$ $\begin{array}{r} 99.4 \\ 8.1 \\ \hline 50 \end{array}$

$\begin{array}{r} 99.3 \\ 8.2 \\ \hline 50 \end{array}$ $\begin{array}{r} 99.2 \\ 8.3 \\ \hline 50 \end{array}$ $\begin{array}{r} 98.9 \\ 8.6 \\ \hline 50 \end{array}$

$\begin{array}{r} 99.2 \\ 8.3 \\ \hline 50 \end{array}$ $\begin{array}{r} 97.6 \\ 8.9 \\ \hline 50 \end{array}$ $\begin{array}{r} 98.6 \\ 8.9 \\ \hline 22 \end{array}$ $\begin{array}{r} 99.1 \\ 8.4 \\ \hline 24 \end{array}$ $\begin{array}{r} 99.9 \\ 7.6 \\ \hline 50 \end{array}$

$\begin{array}{r} 100.9 \\ 6.6 \\ \hline 50 \end{array}$ $\begin{array}{r} 101.8 \\ 5.7 \\ \hline 25 \end{array}$ $\begin{array}{r} 102.3 \\ 5.2 \\ \hline 21 \end{array}$ $\begin{array}{r} 102.4 \\ 5.1 \\ \hline 51 \end{array}$ $\begin{array}{r} 102.7 \\ 4.8 \\ \hline 50 \end{array}$

$\begin{array}{r} 100.1 \\ 7.4 \\ \hline 49 \end{array}$ $\begin{array}{r} 101.4 \\ 6.1 \\ \hline 34 \end{array}$ $\begin{array}{r} 101.1 \\ 6.4 \\ \hline 23 \end{array}$ $\begin{array}{r} 101.5 \\ 6.0 \\ \hline 19 \end{array}$ $\begin{array}{r} 101.8 \\ 5.7 \\ \hline 51 \end{array}$ $\begin{array}{r} 103.1 \\ 4.4 \\ \hline 50 \end{array}$

$\begin{array}{r} 99.7 \\ 7.8 \\ \hline 31 \end{array}$ $\begin{array}{r} 99.8 \\ 7.7 \\ \hline 11 \end{array}$ $\begin{array}{r} 99.5 \\ 8.0 \\ \hline 8 \end{array}$ $\begin{array}{r} 100.0 \\ 7.5 \\ \hline 6 \end{array}$ $\begin{array}{r} 100.8 \\ 6.7 \\ \hline 12 \end{array}$ $\begin{array}{r} 101.0 \\ 6.5 \\ \hline 17 \end{array}$ $\begin{array}{r} 101.1 \\ 6.4 \\ \hline 17 \end{array}$ $\begin{array}{r} 101.7 \\ 5.8 \\ \hline 23 \end{array}$ $\begin{array}{r} 102.1 \\ 5.4 \\ \hline 50 \end{array}$

$\begin{array}{r} 99.4 \\ 8.1 \\ \hline 23 \end{array}$ $\begin{array}{r} 100.0 \\ 7.5 \\ \hline 21 \end{array}$ $\begin{array}{r} 100.1 \\ 7.4 \\ \hline 7 \end{array}$ $\begin{array}{r} 99.6 \\ 7.9 \\ \hline 79 \end{array}$ $\begin{array}{r} 100.8 \\ 6.2 \\ \hline 8 \end{array}$ $\begin{array}{r} 101.3 \\ 6.2 \\ \hline 17 \end{array}$ $\begin{array}{r} 101.2 \\ 6.3 \\ \hline 22 \end{array}$ $\begin{array}{r} 102.0 \\ 5.5 \\ \hline 28 \end{array}$ $\begin{array}{r} 102.9 \\ 5.4 \\ \hline 42 \end{array}$ $\begin{array}{r} 102.1 \\ 5.4 \\ \hline 50 \end{array}$

$\begin{array}{r} 100.1 \\ 7.4 \\ \hline 29.4 \\ 8.1 \end{array}$

107.5

ail in Oak Tree 60' East of 0+00 on N. Fence Line

12

11+50

11+29.2

B.M.

Top of Water

Cr. Bottom

10+51.2

10+29.2

10+00

T.P.

9

8+70

8+48

8

7

6

5.46

96.31

8.7

93.0

10.00

91.7

4.12

101.71

5.62

97.59

103.21

Nail in Birch Rt. of 10+70 - 12' out.

$$\begin{array}{r} 93.6 \\ 8.1 \\ \hline 50 \end{array} \quad \begin{array}{r} 93.6 \\ 8.1 \\ \hline 34 \end{array} \quad \begin{array}{r} 94.9 \\ 6.8 \\ \hline 5.0 \end{array} \quad \begin{array}{r} 96.7 \\ 5.0 \\ \hline 5.0 \end{array}$$

$$\begin{array}{r} 95.6 \\ 6.1 \\ \hline 50 \end{array} \quad \begin{array}{r} 95.5 \\ 6.2 \\ \hline 22 \end{array} \quad \begin{array}{r} 94.7 \\ 7.0 \\ \hline 11 \end{array} \quad \begin{array}{r} 95.0 \\ 6.7 \\ \hline 6.7 \end{array} \quad \begin{array}{r} 95.8 \\ 5.9 \\ \hline 12 \end{array} \quad \begin{array}{r} 95.0 \\ 6.7 \\ \hline 23 \end{array} \quad \begin{array}{r} 95.5 \\ 6.2 \\ \hline 29 \end{array} \quad \begin{array}{r} 94.8 \\ 6.9 \\ \hline 35 \end{array} \quad \begin{array}{r} 95.79 \\ 6.0 \\ \hline 40 \end{array} \quad \begin{array}{r} 95.0 \\ 6.7 \\ \hline 3 \end{array} \quad \begin{array}{r} 92.9 \\ 8.8 \\ \hline 6 \end{array} \quad \begin{array}{r} 92.7 \\ 9.0 \\ \hline 40 \end{array}$$

$$\begin{array}{r} 95.7 \\ 6.0 \\ \hline 48 \end{array} \quad \begin{array}{r} 95.6 \\ 6.1 \\ \hline 42 \end{array} \quad \begin{array}{r} 96.1 \\ 5.6 \\ \hline 36 \end{array} \quad \begin{array}{r} 96.5 \\ 5.2 \\ \hline 9 \end{array} \quad \begin{array}{r} 95.9 \\ 5.8 \\ \hline 3.8 \end{array} \quad \begin{array}{r} 95.0 \\ 6.7 \\ \hline 3 \end{array} \quad \begin{array}{r} 92.9 \\ 8.8 \\ \hline 6 \end{array} \quad \begin{array}{r} 92.7 \\ 9.0 \\ \hline 40 \end{array}$$

$$\begin{array}{r} 93.1 \\ 8.6 \\ \hline 22 \end{array} \quad \begin{array}{r} 97.3 \\ 4.4 \\ \hline 16 \end{array} \quad \begin{array}{r} 98.1 \\ 3.6 \\ \hline 9 \end{array} \quad \begin{array}{r} 98.2 \\ 3.5 \\ \hline 18 \end{array} \quad \begin{array}{r} 97.4 \\ 4.3 \\ \hline 26 \end{array} \quad \begin{array}{r} 97.6 \\ 4.1 \\ \hline 26 \end{array} \quad \begin{array}{r} 97.4 \\ 4.3 \\ \hline 30 \end{array}$$

$$\begin{array}{r} 93.1 \\ 8.6 \\ \hline 42 \end{array} \quad \begin{array}{r} 98.4 \\ 3.3 \\ \hline 37 \end{array} \quad \begin{array}{r} 98.3 \\ 3.4 \\ \hline 3.4 \end{array} \quad \begin{array}{r} 97.1 \\ 2.6 \\ \hline 11 \end{array} \quad \begin{array}{r} 95.3 \\ 6.4 \\ \hline 21 \end{array} \quad \begin{array}{r} 95.5 \\ 6.2 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 98.4 \\ 3.3 \\ \hline 50 \end{array} \quad \begin{array}{r} 98.3 \\ 3.4 \\ \hline 26 \end{array} \quad \begin{array}{r} 97.1 \\ 4.6 \\ \hline 25 \end{array} \quad \begin{array}{r} 96.4 \\ 5.3 \\ \hline 33 \end{array} \quad \begin{array}{r} 95.1 \\ 6.6 \\ \hline 33 \end{array} \quad \begin{array}{r} 96.3 \\ 5.4 \\ \hline 60 \end{array}$$

$$\begin{array}{r} 97.2 \\ 6.0 \\ \hline 50 \end{array} \quad \begin{array}{r} 96.9 \\ 6.3 \\ \hline 21 \end{array} \quad \begin{array}{r} 101.7 \\ 95.2 \\ \hline 7.8 \end{array} \quad \begin{array}{r} 94.4 \\ 8.8 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 95.4 \\ 7.8 \\ \hline 50 \end{array} \quad \begin{array}{r} 94.9 \\ 8.3 \\ \hline 33 \end{array} \quad \begin{array}{r} 95.6 \\ 7.6 \\ \hline 33 \end{array} \quad \begin{array}{r} 94.4 \\ 8.8 \\ \hline 21 \end{array} \quad \begin{array}{r} 94.1 \\ 9.1 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 98.2 \\ 5.0 \\ \hline 50 \end{array} \quad \begin{array}{r} 98.0 \\ 5.2 \\ \hline 25 \end{array} \quad \begin{array}{r} 97.4 \\ 5.8 \\ \hline 25 \end{array} \quad \begin{array}{r} 96.1 \\ 7.1 \\ \hline 40 \end{array} \quad \begin{array}{r} 94.4 \\ 8.8 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 98.9 \\ 2.3 \\ \hline 50 \end{array} \quad \begin{array}{r} 98.9 \\ 4.3 \\ \hline 4.3 \end{array} \quad \begin{array}{r} 98.0 \\ 5.2 \\ \hline 39 \end{array} \quad \begin{array}{r} 97.2 \\ 6.0 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 99.6 \\ 3.6 \\ \hline 50 \end{array} \quad \begin{array}{r} 99.3 \\ 3.9 \\ \hline 3.9 \end{array} \quad \begin{array}{r} 98.7 \\ 4.5 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 99.2 \\ 4.0 \\ \hline 50 \end{array} \quad \begin{array}{r} 99.0 \\ 4.2 \\ \hline 4.2 \end{array} \quad \begin{array}{r} 98.6 \\ 4.6 \\ \hline 27 \end{array} \quad \begin{array}{r} 97.8 \\ 5.4 \\ \hline 50 \end{array}$$

103.2

20		5.7	98.2
19		5.3	98.6
B.M. and High Water			
Summer 1924	4.23		99.67
18+48	E. end Floor Br.	2.6	101.3
	Flow Line	15.9	
	Water Level	12.2	
16+95	W. end Floor	2.80	101.10
T.P.	4.23	103.90	3.40 99.67

Nail in
Oak Tree Sta. 18+75 - 20' Left

16+03

15+70

15+52

15+32

15

14

13

12+81.3

12+33

B.M.	3.78	103.07	2.42	99.29
------	------	--------	------	-------

101.71

98.9	97.1	98.0	98.0	98.5	96.6	97.0
4.2	6.0	5.1	4.6	6.5	6.1	5.0
98	34	24	12	26	50	
98.9	97.1	98.0	98.3	96.9	97.1	96.1
4.2	6.0	5.1	4.8	6.2	6.0	7.0
98	34	24	19	24	24	50
96.4	97.8	97.3	96.0	98.4	98.4	
6.7	5.3	5.8	7.1	4.7	4.9	5.0
50	44	18	27	36	50	
96.3	98.0	96.3	94.7	95.7	98.1	97.2
6.8	5.1	6.8	8.4	7.4	5.0	5.9
45	31	29	15	10	8	50
96.2	97.6	97.9	97.0			
3.9	5.5	5.2	6.1			
50	12	5.2	50			
94.9	98.1	98.0	97.9			
8.2	4.5	5.1	5.2			
50	37	5.1	50			
94.5	97.4	98.1	97.5	95.8	96.4	96.2
8.6	5.7	5.0	5.6	7.3	6.7	6.9
50	41	20	5.6	17	33	50
96.3	98.2	97.8	96.5	97.2	96.6	
6.8	4.9	5.3	6.6	5.9	6.2	5.0
50	44	24	6.0	23	43	50
93.8	93.8	94.8	99.0	98.2	98.3	
9.3	9.3	8.3	4.1	4.9	4.8	50
50	40	22	19	40	50	
			103.1			

KEITH'S RAILROAD CURVE TABLES.

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HOW TO USE KEITH'S TABLES.

EXAMPLE.

Wanted a Curve with an Ext. of about 12 ft. Angle
of Intersection or I. P.= $23^{\circ} 20'$ to the R. at Station
542+72.

Ext. in Tab. IV opposite $23^{\circ} 20' = 120.87$
 $120.87 + 12 = 10.07$. Say a 10° Curve.

Tan. in Tab. IV opp. $23^{\circ} 20' = 1183.1$
 $1183.1 + 10 = 118.81$.

Tab. V. correction for A. $23^{\circ} 20'$ for a 10° Cur. = 0.16
 $118.81 + 0.16 = 118.47 =$ corrected Tangent.

(If corrected Ext. is required find in same way)
Ang. $23^{\circ} 20' = 23.33^{\circ} + 10 = 2.3333 =$ L. C.

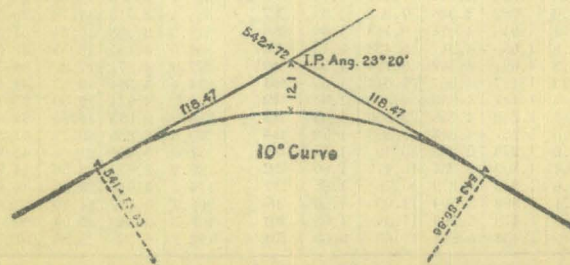
$2^{\circ} 19\frac{1}{2}' =$ def. for sta.	542	I. P. = sta.	542+72
$4^{\circ} 49\frac{1}{2}' =$ " " "	+50	Tan. =	1.18.47
$7^{\circ} 19\frac{1}{2}' =$ " " "	543	B. C. = sta.	541+53.53
$9^{\circ} 49\frac{1}{2}' =$ " " "	+50	L. C. =	2.33.33
$11^{\circ} 40' =$ " " "	543+	E. C. = sta.	543+86.86
	86.86		

$100 - 53.53 = 46.47 \times 3' (\text{def. for 1 ft. of } 10^{\circ} \text{ Cur.}) = 139.41' =$
 $2^{\circ} 19\frac{1}{2}' =$ def. for sta. 542.

Def. for 50 ft. = $2^{\circ} 30'$ for a 10° Curve.

Def. for 36.86 ft. = $1^{\circ} 50\frac{1}{2}'$ for a 10° Curve

(These tables are published in Field Books of
KEUFFEL & ESSER CO., New York, N. Y.)



B.M. T.P. 7.18 104.42 4.48 99.94
3.30 97.24

Center Overflow Br. 4.3

T.P. 4.22 100.54 9.49 96.32

T.P. 6.46 105.81 3.10 99.35

B.M. Tall NE wing
Pile sta. 25+00 3.72

28+23.3 0.0 102.5

28 1.0 101.5

27 3.8 98.7

26 4.9 97.6

25 5.7 96.8

24+97 5.7 96.8

24+47 center 5.3 97.2

24+00.5 5.7 96.8

23 6.2 96.3

T.P. 2.31 102.45 5.5 97.0

22 3.76 100.14

21 6.1 97.8

21 7.7 96.2

103.90

Table VI. Deflections for Sub Chords for Short Radius Curves.

Degree of Curve	Radius 50 sin. def. ang.	$\frac{1}{2}$ sub chord R = sin of def. angle				Length of arc for 100 ft.
		12.5 Ft.	15 Ft.	20 Ft.	25 Ft.	
30°	193.18	1° 51'	2° 17'	2° 58'	3° 43'	101.15
32°	181.39	1° 59'	2° 25'	3° 10'	3° 58'	101.33
34°	171.01	2° 06'	2° 33'	3° 21'	4° 12'	101.48
36°	161.80	2° 13'	2° 41'	3° 33'	4° 26'	101.66
38°	153.58	2° 20'	2° 49'	3° 44'	4° 40'	101.85
40°	146.19	2° 27'	2° 57'	3° 55'	4° 54'	102.06
42°	139.52	2° 34'	3° 05'	4° 07'	5° 08'	102.29
44°	133.47	2° 41'	3° 13'	4° 18'	5° 22'	102.53
46°	127.97	2° 48'	3° 21'	4° 29'	5° 36'	102.76
48°	122.92	2° 55'	3° 29'	4° 40'	5° 50'	103.00
50°	118.31	3° 02'	3° 38'	4° 51'	6° 04'	103.24
52°	114.06	3° 09'	3° 46'	5° 02'	6° 17'	103.54
54°	110.11	3° 16'	3° 54'	5° 13'	6° 31'	103.84
56°	106.50	3° 22'	4° 02'	5° 23'	6° 44'	104.14
58°	103.14	3° 29'	4° 10'	5° 34'	6° 57'	104.43
60°	100.00	3° 35'	4° 18'	5° 44'	7° 11'	104.72

CURVE FORMULAS.

$T = R \tan \frac{1}{2} I$	$R = T \cot. \frac{1}{2} I$	Chord def. = $\frac{\text{chord}^2}{R}$
$T = 50 \tan. \frac{1}{2} I$	$R = 50$	
$\text{Sin. D} = \frac{50}{R}$	$\text{Sin. D} = \frac{R}{50}$	No. chords = $\frac{1}{2} \frac{I}{D}$
$\text{Sin. D} = 50 \tan. \frac{1}{2} I$	$E = R \text{ ex. sec. } \frac{1}{2} I$	
	$E = T \tan \frac{1}{2} I$	Tan. def. = $\frac{1}{2} \text{ chord def}$

The square of any distance, divided by twice the radius, will equal the distance from tangent to curve, very nearly.

Table IV. contains Tangents and External to a 1° curve. Tan. and Ext. to any other radius may be found, nearly enough, by dividing the Tan. or Ext. opposite the given Central Angle by the given degree of curve.

To find Deg. of Curve, having the Central Angle and Tangent: Divide Tan. opposite the given Central Angle by the given Tangent.

To find Deg. of Curve, having the Central Angle and Tangent: Divide Ext. opposite the given Central Angle by the given External.

To find Nat. Tan. and Nat. Ex. Sec. for any angle by Table IV.: Tan. or Ext. of twice the given angle divided by the radius of a 1° curve will be the Nat. Tan. or Nat. Ex. Sec.

To find angle for a given distance and deflection.

Rule 1. Multiply the given distance by .01745 (def. for 1° for 1 ft.), and divide given deflection by the product.

Rule 2. Multiply given deflection by 57.3, and divide the product by the given distance.

To find deflection for a given angle and distance. Multiply the angle by .01745, and the product by the distance.

RIGHT ANGLE TRIANGLES.-- Square the altitude, divide by twice the base. Add quotient to base for hypotenuse.

Given Base 100, Alt 10. $10^2 \div 200 = .5$. $100 + .5 = 100.5$ hyp.

Given Hyp. 100, Alt. 25. $25^2 \div 200 = 3.125$. $100 - 3.125 = 96.875 =$ Base

Error in first example, .002; in last, .045.

To find Tons of Rail in one mile of track: multiply weight per yard by 11, and divide by 7.

Natural Sines

deg.	0'	10'	20'	30'	40'	50'	deg.	0'	10'	20'	30'	40'	50'	deg.	
0	0000	0029	0058	0087	0116	0145	89	40	6428	6450	6472	6494	6517	6539	49
1	0175	0204	0233	0262	0291	0320	88	41	6561	6583	6604	6626	6648	6670	48
2	0349	0378	0407	0436	0465	0494	87	42	6691	6713	6734	6756	6777	6799	47
3	0523	0552	0581	0610	0640	0669	86	43	6820	6841	6862	6884	6905	6926	46
4	0698	0727	0756	0785	0814	0843	85	44	6947	6967	6988	7009	7030	7050	45
5	0872	0901	0929	0958	0987	1016	84	45	7071	7092	7112	7133	7153	7173	44
6	1045	1074	1103	1132	1161	1190	83	46	7193	7214	7234	7254	7274	7294	43
7	1219	1248	1279	1305	1334	1363	82	47	7314	7333	7353	7373	7392	7412	42
8	1392	1421	1449	1478	1507	1536	81	48	7431	7451	7470	7490	7509	7528	41
9	1564	1593	1622	1650	1679	1708	80	49	7547	7566	7585	7604	7623	7642	40
10	1736	1765	1794	1822	1851	1880	79	50	7660	7679	7698	7716	7735	7753	39
11	1908	1937	1965	1994	2022	2051	78	51	7771	7790	7808	7826	7844	7862	38
12	2079	2108	2136	2164	2193	2221	77	52	7880	7898	7916	7934	7951	7969	37
13	2250	2278	2306	2334	2363	2391	76	53	7986	8004	8021	8039	8056	8073	36
14	2419	2447	2476	2504	2532	2560	75	54	8090	8107	8124	8141	8158	8175	35
15	2588	2616	2644	2672	2700	2728	74	55	8192	8208	8225	8241	8258	8274	34
16	2756	2784	2812	2840	2868	2896	73	56	8290	8307	8323	8339	8355	8371	33
17	2924	2952	2979	3007	3035	3062	72	57	8387	8403	8418	8434	8450	8465	32
18	3090	3118	3145	3173	3201	3228	71	58	8480	8496	8511	8526	8542	8557	31
19	3256	3283	3311	3338	3365	3393	70	59	8572	8587	8601	8616	8631	8646	30
20	3420	3448	3475	3502	3529	3557	69	60	8660	8675	8689	8704	8718	8732	29
21	3584	3611	3638	3665	3692	3719	68	61	8746	8760	8774	8788	8802	8816	28
22	3746	3773	3800	3827	3854	3881	67	62	8829	8843	8857	8870	8884	8897	27
23	3907	3934	3961	3987	4014	4041	66	63	8910	8923	8936	8949	8962	8975	26
24	4067	4094	4120	4147	4173	4200	65	64	8988	9001	9013	9026	9038	9051	25
25	4226	4253	4279	4305	4331	4358	64	65	9063	9075	9088	9100	9112	9124	24
26	4384	4410	4436	4462	4488	4514	63	66	9135	9147	9159	9171	9182	9194	23
27	4540	4566	4592	4617	4643	4669	62	67	9205	9216	9228	9239	9250	9261	22
28	4695	4720	4746	4772	4797	4823	61	68	9272	9283	9293	9304	9315	9325	21
29	4848	4874	4899	4924	4950	4975	60	69	9336	9346	9356	9367	9377	9387	20
30	5000	5025	5050	5075	5100	5125	59	70	9397	9407	9417	9426	9436	9446	19
31	5150	5175	5200	5225	5250	5275	58	71	9455	9465	9474	9483	9492	9502	18
32	5299	5324	5348	5373	5398	5422	57	72	9511	9520	9528	9537	9546	9555	17
33	5446	5471	5495	5519	5544	5568	56	73	9563	9572	9580	9588	9596	9605	16
34	5592	5616	5640	5664	5688	5712	55	74	9613	9621	9628	9636	9644	9652	15
35	5736	5760	5783	5807	5831	5854	54	75	9659	9667	9674	9681	9689	9696	14
36	5878	5901	5925	5948	5972	5995	53	76	9703	9710	9717	9724	9730	9737	13
37	6018	6041	6065	6088	6111	6134	52	77	9744	9750	9757	9763	9769	9775	12
38	6157	6180	6202	6225	6248	6271	51	78	9781	9787	9793	9799	9805	9811	11
39	6293	6316	6338	6361	6383	6406	50	79	9816	9822	9827	9833	9838	9843	10
deg.	0'	50'	40'	30'	20'	10'	deg.	60'	50'	40'	30'	20'	10'	deg.	

deg.	0'	10'	20'	30'	40'	50'	deg.
80	9848	9853	9858	9863	9868	9872	9
81	9877	9881	9886	9890	9894	9899	8
82	9903	9907	9911	9914	9918	9922	7
83	9925	9929	9932	9936	9939	9942	6
84	9945	9948	9951	9954	9957	9959	5
85	9962	9964	9967	9969	9971	9974	4
86	9976	9978	9980	9981	9983	9985	3
87	9986	9988	9989	9990	9992	9993	2
88	9994	9995	9996	9997	9997	9998	1
89	9998	9999	9999	9999	1.0000	1.0000	0

Natural Cosines

Natural Tangents

min	0'	10'	20'	30'	40'	50'	sec	0'	10'	20'	30'	40'	50'	sec
0	0000	0029	0058	0087	0116	0145	89	40	8391	8441	8491	8541	8591	8642
1	0175	0204	0233	0262	0291	0320	88	41	8693	8744	8796	8847	8899	8952
2	0349	0378	0407	0437	0466	0495	87	42	9004	9057	9110	9163	9217	9271
3	0524	0553	0582	0612	0641	0670	86	43	9325	9380	9435	9490	9545	9601
4	0699	0729	0758	0787	0816	0846	85	44	9657	9713	9770	9827	9884	9942
5	0875	0904	0934	0963	0992	1022	84	45	1.0000	1.0058	1.0117	1.0176	1.0235	1.0295
6	1051	1080	1110	1139	1169	1198	83	46	1.0355	1.0416	1.0477	1.0533	1.0590	1.0661
7	1228	1257	1287	1317	1346	1376	82	47	1.0724	1.0786	1.0850	1.0913	1.0977	1.1041
8	1405	1435	1465	1495	1524	1554	81	48	1.1106	1.1171	1.1237	1.1303	1.1369	1.1436
9	1584	1614	1644	1673	1703	1733	80	49	1.1504	1.1571	1.1640	1.1708	1.1778	1.1847
10	1763	1793	1823	1853	1883	1914	79	50	1.1918	1.1988	1.2059	1.2131	1.2203	1.2276
11	1944	1974	2004	2035	2065	2095	78	51	1.2340	1.2423	1.2497	1.2572	1.2647	1.2723
12	2126	2156	2186	2217	2247	2278	77	52	1.2799	1.2876	1.2954	1.3032	1.3111	1.3190
13	2300	2330	2370	2401	2432	2462	76	53	1.3270	1.3351	1.3435	1.3514	1.3597	1.3680
14	2493	2524	2555	2586	2617	2648	75	54	1.3764	1.3848	1.3934	1.4019	1.4106	1.4193
15	2679	2711	2742	2773	2805	2836	74	55	1.4281	1.4370	1.4460	1.4550	1.4641	1.4733
16	2867	2899	2931	2962	2994	3026	73	56	1.4826	1.4919	1.5013	1.5108	1.5204	1.5301
17	3057	3089	3121	3153	3185	3217	72	57	1.5399	1.5497	1.5597	1.5697	1.5798	1.5900
18	3249	3281	3314	3346	3378	3411	71	58	1.6003	1.6107	1.6212	1.6319	1.6426	1.6534
19	3443	3476	3508	3541	3574	3607	70	59	1.6643	1.6753	1.6864	1.6977	1.7090	1.7205
20	3640	3673	3706	3739	3772	3805	69	60	1.7321	1.7437	1.7556	1.7675	1.7797	1.7917
21	3839	3872	3906	3939	3973	4006	68	61	1.8040	1.8165	1.8291	1.8418	1.8546	1.8676
22	4040	4074	4108	4142	4176	4210	67	62	1.8807	1.8940	1.9074	1.9210	1.9347	1.9486
23	4245	4279	4314	4348	4383	4417	66	63	1.9626	1.9768	1.9912	2.0057	2.0204	2.0353
24	4452	4487	4522	4557	4592	4628	65	64	2.0503	2.0655	2.0809	2.0965	2.1123	2.1283
25	4663	4699	4734	4770	4806	4841	64	65	2.1445	2.1609	2.1775	2.1943	2.2113	2.2286
26	4877	4913	4950	4986	5022	5059	63	66	2.2460	2.2637	2.2817	2.2998	2.3183	2.3369
27	5095	5132	5169	5206	5243	5280	62	67	2.3559	2.3750	2.3945	2.4142	2.4342	2.4545
28	5317	5354	5392	5430	5467	5505	61	68	2.4751	2.4960	2.5172	2.5386	2.5605	2.5826
29	5543	5581	5619	5658	5696	5735	60	69	2.6051	2.6279	2.6511	2.6746	2.6985	2.7228
30	5774	5812	5851	5890	5930	5969	59	70	2.7475	2.7725	2.7980	2.8239	2.8502	2.8770
31	6009	6048	6088	6128	6168	6208	58	71	2.9042	2.9319	2.9600	2.9887	3.0178	3.0475
32	6249	6289	6330	6371	6412	6453	57	72	3.0777	3.1084	3.1397	3.1716	3.2041	3.2371
33	6494	6536	6577	6619	6661	6703	56	73	3.2709	3.3052	3.3402	3.3759	3.4124	3.4495
34	6745	6787	6830	6873	6916	6959	55	74	3.4874	3.5261	3.5656	3.6059	3.6470	3.6891
35	7002	7046	7089	7133	7177	7221	54	75	3.7321	3.7760	3.8208	3.8657	3.9136	3.9617
36	7265	7310	7355	7400	7445	7490	53	76	4.0108	4.0611	4.1126	4.1653	4.2193	4.2747
37	7536	7581	7627	7673	7720	7766	52	77	4.3315	4.3897	4.4494	4.5107	4.5736	4.6382
38	7813	7860	7907	7954	8002	8050	51	78	4.7046	4.7729	4.8430	4.9152	4.9894	5.0658
39	8098	8146	8195	8243	8292	8342	50	79	5.1446	5.2257	5.3093	5.3955	5.4845	5.5764
min	60'	50'	40'	30'	20'	10'	sec	60'	50'	40'	30'	20'	10'	sec

sec	0'	10'	20'	30'	40'	50'	sec
80	5.6713	5.7694	5.8708	5.9758	6.0844	6.1970	9
81	6.3135	6.4348	6.5606	6.6912	6.8269	6.9682	8
82	7.1154	7.2687	7.4287	7.5958	7.7704	7.9530	7
83	8.1443	8.3450	8.5555	8.7769	9.0098	9.2553	6
84	9.5144	9.7882	10.078	10.385	10.7111	11.0595	5
85	11.430	11.826	12.250	12.706	13.197	13.727	4
86	14.300	14.924	15.605	16.350	17.169	18.075	3
87	19.081	20.206	21.470	22.903	24.542	26.432	2
88	28.636	31.242	34.368	38.189	42.964	49.104	1
89	57.290	68.750	85.940	114.588	171.885	343.77	0
sec	60'	50'	40'	30'	20'	10'	sec

Natural Cotangents

1.72 3.16 3.19 3.20 1.78

3.28 3.23 3.14

161 7.87
 23 78
 23.3
 40
 1. 63.3
 1.87
 6.09
 104 29.2
 22.6
 104 51.8
 3.16
 1.72
 1.44
 180
 14.2
 37
 55
 292
 521
 124813

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

ROADWAY 14 FEET WIDE. SIDE SLOPES 1 1/2 to 1.

FOR SINGLE TRACK EMBANKMENT.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	7.0	7.2	7.3	7.5	7.6	7.8	7.9	8.1	8.2	8.4	0
1	8.5	8.7	8.8	9.0	9.1	9.3	9.4	9.6	9.7	9.9	1
2	10.0	10.2	10.3	10.5	10.6	10.8	10.9	11.1	11.2	11.4	2
3	11.5	11.7	11.8	12.0	12.1	12.3	12.4	12.6	12.7	12.9	3
4	13.0	13.2	13.3	13.5	13.6	13.8	13.9	14.1	14.2	14.4	4
5	14.5	14.7	14.8	15.0	15.1	15.3	15.4	15.6	15.7	15.9	5
6	16.0	16.2	16.3	16.5	16.6	16.8	16.9	17.1	17.2	17.4	6
7	17.5	17.7	17.8	18.0	18.1	18.3	18.4	18.6	18.7	18.9	7
8	19.0	19.2	19.3	19.5	19.6	19.8	19.9	20.1	20.2	20.4	8
9	20.5	20.7	20.8	21.0	21.1	21.3	21.4	21.6	21.7	21.9	9
10	22.0	22.2	22.3	22.5	22.6	22.8	22.9	23.1	23.2	23.4	10
11	23.5	23.7	23.8	24.0	24.1	24.3	24.4	24.6	24.7	24.9	11
12	25.0	25.2	25.3	25.5	25.6	25.8	25.9	26.1	26.2	26.4	12
13	26.5	26.7	26.8	27.0	27.1	27.3	27.4	27.6	27.7	27.9	13
14	28.0	28.2	28.3	28.5	28.6	28.8	28.9	29.1	29.2	29.4	14
15	29.5	29.7	29.8	30.0	30.1	30.3	30.4	30.6	30.7	30.9	15
16	31.0	31.2	31.3	31.5	31.6	31.8	31.9	32.1	32.2	32.4	16
17	32.5	32.7	32.8	33.0	33.1	33.3	33.4	33.6	33.7	33.9	17
18	34.0	34.2	34.3	34.5	34.6	34.8	34.9	35.1	35.2	35.4	18
19	35.5	35.7	35.8	36.0	36.1	36.3	36.4	36.6	36.7	36.9	19
20	37.0	37.2	37.3	37.5	37.6	37.8	37.9	38.1	38.2	38.4	20
21	38.5	38.7	38.8	39.0	39.1	39.3	39.4	39.6	39.7	39.9	21
22	40.0	40.2	40.3	40.5	40.6	40.8	40.9	41.1	41.2	41.4	22
23	41.5	41.7	41.8	42.0	42.1	42.3	42.4	42.6	42.7	42.9	23
24	43.0	43.2	43.3	43.5	43.6	43.8	43.9	44.1	44.2	44.4	24
25	44.5	44.7	44.8	45.0	45.1	45.3	45.4	45.6	45.7	45.9	25
26	46.0	46.2	46.3	46.5	46.6	46.8	46.9	47.1	47.2	47.4	26
27	47.5	47.7	47.8	48.0	48.1	48.3	48.4	48.6	48.7	48.9	27
28	49.0	49.2	49.3	49.5	49.6	49.8	49.9	50.1	50.2	50.4	28
29	50.5	50.7	50.8	51.0	51.1	51.3	51.4	51.6	51.7	51.9	29
30	52.0	52.2	52.3	52.5	52.6	52.8	52.9	53.1	53.2	53.4	30
31	53.5	53.7	53.8	54.0	54.1	54.3	54.4	54.6	54.7	54.9	31
32	55.0	55.2	55.3	55.5	55.6	55.8	55.9	56.1	56.2	56.4	32
33	56.5	56.7	56.8	57.0	57.1	57.3	57.4	57.6	57.7	57.9	33
34	58.0	58.2	58.3	58.5	58.6	58.8	58.9	59.1	59.2	59.4	34
35	59.5	59.7	59.8	60.0	60.1	60.3	60.4	60.6	60.7	60.9	35
36	61.0	61.2	61.3	61.5	61.6	61.8	61.9	62.1	62.2	62.4	36

Calculated by Julien A. Hall, M. Am. Soc. C. E.

MADE IN GERMANY.