

EAGLE CENTER-HUDSON RD.
CONSTRUCTION BOOK

1922

FIELD BOOK

369

38

KEUFFEL & ESSER CO.

DRAWING MATERIALS

AND

SURVEYING INSTRUMENTS.

NEW YORK.

CHICAGO. ST. LOUIS. SAN FRANCISCO. MONTREAL.

TABLES FOR EXCAVATIONS AND EMBANKMENTS.

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

ROADWAY 18 FEET WIDE. SIDE SLOPES 1 TO 1.

FOR SINGLE TRACK EXCAVATION.

"Copyright, 1895, by Keuffel & Esser Co."

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	0
1	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	1
2	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	2
3	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	3
4	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	4
5	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	5
6	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	6
7	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	7
8	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	8
9	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	9
10	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	10
11	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	11
12	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	12
13	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	13
14	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	14
15	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	15
16	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	16
17	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	17
18	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	18
19	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	19
20	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	20
21	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	21
22	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	22
23	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	23
24	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	24
25	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	25
26	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	26
27	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	27
28	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	28
29	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	29
30	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	30
31	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	31
32	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	32
33	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	33
34	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	34
35	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	35
36	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	36

Calculated by Julien A. Hall, M. Am. Soc. C. E.

For Keith's Railroad Curve Tables see end of book.

Eagle Center-Hudson Rd.

BK. 738

Const.

1922

Property of
County Engineers Office
Court House
Waterloo Iowa

Entered 1923 CRH

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001

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Sec 28+29 - 88-14		55-58

Tile Grades - Eagle Center - South Side

Hudson Road - 1922

003

Sta	Gro	Gro El	Stk	Stk El	Grade	Stk. Cut	Gro Cut.
B.M.	8.73	206.44		197.74		Center - N. Headwall	Stem box Sta 131+07 5/20/22
#			12.95	193.52			Hoff Tarbell Mathews
131+03	10.5	195.07	9.51	196.96	193.75	3.21	2.22
+50	9.9	196.57	9.31	197.16	194.07	3.09	
132	9.6	196.87	8.92	197.55	194.40	3.15	1.25
+50	8.3	198.17	7.51	198.96	194.72	4.24	1.62 1/2 37 1/2
133	7.6	198.87	6.90	199.57	195.05	4.52	
+50	6.7	199.77	6.12	200.35	196.12	4.23	
134	5.7	200.77	5.08	201.39	197.20	4.19	
+50	4.7	201.77	4.05	202.42	198.27	4.15	
135	3.4	203.07	2.76	203.71	199.35	4.36	
+50	2.2	204.27	1.51	204.96	200.42	4.54	3.85
136	1.3	205.80	0.64	205.83	201.50	4.33	
+50	7.7	206.10	6.97	206.83	202.22	4.61	3.88
137	7.0	206.80	6.30	207.50	202.95	4.55	3.85
+50	6.3	207.50	5.66	208.14	203.67	4.47	3.83
138	5.7	208.10	5.08	208.72	204.40	4.32	
+50	5.1	208.70	4.39	209.41	205.12	4.29	
139	4.6	209.20	4.05	209.75	205.85	3.90	
+50	3.8	210.00	3.17	210.63	206.83	3.80	
140	2.9	210.90	2.27	211.53	207.80	3.73	
+50	1.8	212.00	1.16	212.64	208.78	3.86	
141	12.4	212.69	11.54	213.55	209.75	3.80	
+50	11.5	213.59	10.65	214.44	210.73	3.71	
142	10.5	214.59	9.83	215.26	211.70	3.56	
+50	9.6	215.40	8.89	216.20	212.68	3.52	

No. Overdepth

North Side

Sta.	Gro	Gr El	StK	StK El.	Grade	St Cut	Gro Cut.
B. 17.	8.73	(206.47)		197.74			
E			12.73	193.74			
131+17	10-20		9.85	197.12	193.90	3.22	
+50	10-6		9.80	196.67	194.10	2.57	
132	9.8		9.15	197.32	194.42	2.90	
+50	8.8		8.16	198.31	194.73	3.58	
133	7.8		7.18	199.29	195.05	4.24	
+50	6.9		6.17	200.30	196.12	4.18	
134	5.5	200.97	4.75	201.72	197.20	4.52	3.77
+50	4.2	202.27	3.32	203.15	198.27	4.88	4.00
135	3.10	203.37	2.24	204.23	199.35	4.88	4.02
+50	2.1	204.37	1.22	205.25	200.42	4.83	3.95
136	1.1	205.37	0.34	206.13	201.50	4.63	3.87
		(213.80)					
+50	7.7	206.10	6.95	206.85	202.22	4.63	3.88
137	7.1	206.70	6.38	207.42	202.95	4.47	3.75
+50	6.4	207.40	5.71	208.09	203.67	4.42	3.73
138	5.9	207.90	5.13	208.67	204.40	4.27	3.60
+50	5.2	208.60	4.41	209.39	205.12	4.27	
139	4.5		3.74	210.06	205.85	4.21	
+50	3.6		2.92	210.88	206.83	4.05	
140	2.7		2.05	211.75	207.80	3.95	
+50	1.7		1.10	212.70	208.78	3.92	
	(225.09)						
141	12.1		11.37	213.72	209.75	3.97	
+50	11.2		10.50	214.57	210.73	3.86	
142	10.3		9.63	215.46	211.70	3.76	
+50	9.2		8.60	216.49	212.68	3.81	

No Overcut

(228.09)

143	8.5	7.87	217.22	213.65	3.57
150	7.3	6.52	218.57	214.63	3.94
144	6.0	5.26	219.83	215.60	4.23
B.M.		2.61	222.48	cm. 222.50	

Spike E Gate post N Sta 145+58

Mr. Carver

	3.43	201.17		197.74			
131	5.2	4.63	196.54	193.20			
130+50	6.1	5.54	195.63	193.30			
130	6.3	5.76	195.47	190.1			
129+50	6.4	194.77	5.95	195.22	190.4	4.82	
129	6.3	194.87	5.69	195.48	190.7	4.78	
128+50	5.5	195.67	4.97	196.20	191.0	5.20	
128	5.1	196.07	4.49	196.68	191.3	5.38	
127+50	5.3	195.87	4.64	196.53	191.6	4.93	
127	5.5	195.67	4.90	196.27	191.9	4.37	
126+50	5.4	195.77	4.78	196.39	192.2	4.19	
126	5.4	195.77	4.74	196.43	192.5	3.93	
125+50	5.2	195.97	4.59	196.58	192.8	3.78	
125	4.7	196.47	4.13	197.04	193.1	3.94	

50' to Jct.

Jct on Line 130+50 .160e

.30e

.40e

.50e

225.89

143	8.3		7.65	217.44	213.65	3.79	
150	7.1		6.52	218.57	214.63	3.94	
144	5.8	209.29	4.97	220.12	215.60	4.52	3.69
	3.43	(201.17)		197.74			
131+11	4.9	196.3	4.34	196.83	192.8	4.03	
				192.6			
130+50	5.8	195.7	5.22	195.95	191.6	4.35	51 feet to Jet.
130	6.0		5.35	195.82	190.6		
129+50	5.9	195.3	5.32	195.85	191.1	4.75	4.2
129	5.7	195.5	5.12	196.05	191.6	4.45	3.9
128+50	5.5	195.7	4.90	196.27	191.8	4.47	3.9
128	5.1	196.1	4.55	196.62	192.0	4.62	4.1
127+50	5.1	196.1	4.47	196.70	192.2	4.5	3.9
127	5.3	195.9	4.72	196.45	192.4	4.05	3.5
126+50	5.2	196.0	4.50	196.67	192.6	4.07	
126	5.1	196.1	4.45	196.72	192.8	3.92	
125+50	4.8	196.4	4.12	197.05	193.0	4.05	
125	4.5	196.67	3.90	197.27	193.2	4.07	

No Out

No Out

Out et
2.31 100.05

130	4.5	195.55	3.93	196.12	190.6	5.52	4.95
130+50	6.2	193.85	5.49	194.56	190.1	4.46	3.75
131	7.0	193.05	6.49	193.56			
131+47	7.6	192.45	7.05	193.00			
	9.96	196.05					
	9.96	196.05					

Out let changed

	4.81	201.85		197.04	193.1	
124+50	5.1	196.75	4.44	197.41	193.4	4.01
124	4.9	196.95	4.33	197.52	193.7	3.82
123+50	4.7	197.15	4.10	197.75	194.0	3.75
123	4.8	197.05	4.29	197.56	193.67	3.89
122+50	5.1	196.75	4.48	197.37	193.33	4.04
122	5.4	196.45	4.80	197.05	193.0	4.05
121+50	5.7	196.15	5.07	196.78	192.5	4.28
121	6.0	195.85	5.34	196.51	192.0	4.51
		197.91				
120+50	2.7	195.2	2.11	195.80	191.5	4.30 ✓
120	3.8	194.11	3.13	194.78	191.00	3.78 ✓
119+50	4.9	193.01	4.01	193.90	189.38	4.52 ✓
119	6.5	191.41	5.67	192.24	189.75	4.49 ✓
118+50	8.2	189.71	7.57	190.34	186.12	4.22 ✓
118	10.1	187.81	9.38	188.53	184.50	4.03 ✓
		185.91				
117+50	12.0	187.40	11.54	186.37	182.87	3.50 ✓
	1.03					
117	3.3	184.1	2.63	184.77	181.25	3.52 ✓
116+50	5.0	180.4	4.39	183.01	179.63	3.38 ✓
116	6.5	180.9	5.81	181.59	178.00	3.59 ✓
115+50	7.7	179.7	7.11	180.29	177.58	2.71 ✓
115	8.6	178.8	7.88	179.52	177.15	2.37 ✓
114+50	9.3	178.1	8.62	178.78	176.72	2.06 ✓
114	9.8	177.6	9.00	178.40	176.24	2.11 ✓
		183.81				
113+50	6.6	177.2	5.82	177.99	175.86	2.13 ✓
113	6.8	177.0	6.02	177.79	175.43	2.36 ✓
112+50	5.2	178.6	4.54	179.27	175.00	4.27 ✓

no current

	201.85		193.2	
124+50	4.9	4.22	197.63	193.4
124	4.6	3.92	197.93	193.6
123+50	4.5	3.93	197.92	193.8
123	4.6	197.25	3.77	198.08
122+50	4.8	4.16	197.69	193.27
122	5.1	4.42	197.43	193.00
121+50	5.3	4.73	197.12	192.5
121	5.9	5.24	196.61	192.0
120+50	2.8	2.24	195.67	191.5
120	3.9	3.28	194.63	191.00
119+50	5.4	4.78	193.13	189.38
119	6.6	6.18	191.73	187.75
118+50	8.3	7.91	190.00	186.12
118	9.9	9.26	188.65	184.50
117+50	11.9	11.22	186.69	182.87
117	3.3	2.67	184.73	181.25
116+50	5.0	4.43	182.97	179.63
116	—	—	178.00	—
115+50	7.7	7.12	180.28	177.58
115	9.1	8.48	178.92	177.15
114+50	10.0	9.24	178.16	176.72
114	10.3	9.74	177.66	176.29
113+50	6.5	6.50	177.31	175.86
113	7.9	6.84	176.97	175.43
112+50	7.8	7.38	176.43	175.00
112+32	7.5	6.61	177.20	174.84

4.23

4.33

4.12

4.54

4.42

4.43

4.62

4.61

4.17

3.63

3.75

3.98

3.88

4.15

3.82

3.48

3.34

2.70

1.77

1.44

1.37

1.45

1.54

1.43

2.36

No Quercus

Change Outlet East of
Gro outlet line 3+K

Skew Culv Sta 131+07

BM.	2.55	200.29	197.74
6" Tile Top E Outlet		11 2 3	10 6 5
0	7.4	7.06	193.23 189.09 4.14
0+25	7.1	193.19 6.40	193.89 189.34 4.55
0+50	6.8	193.49 6.10	194.19 189.59 4.60 80
0+75	6.4	193.89 5.79	194.50 189.84 4.66 1.00
1	5.4	194.89 5.01	195.28 190.09 5.19
1+15=0	4.6	195.69 3.91	196.38 190.24 6.14

12 6" Farm Tile 50' Hwy

3 85

3 90

4.05

4.80

5.45

25' - .400

15' - 1.200

= Inct

N. side - Line W

200.29

190.25

130+10	4.9	195.39 4.03	196.26 190.54 5.74 1.45
130+25	5.0	195.29 4.46	195.83 190.94 4.89 2.10
130+50	5.4	194.89 4.33	195.96 191.61 4.35

4.85 130+10 15 10' from Inct

4.35 15' - .600

3.28

N. side - Line E

200.29

190.25

130	4.9	195.39 4.27	196.02 190.39 5.63 1.42
129+75	5.0	195.29 4.24	196.05 190.75 5.30
129+50	5.0	195.29 4.44	196.85 191.10 4.75

5.00 130 15 6' from Inct

4.67 10' - 1.500

4.19 25' - .800

4.19 25' - .400

130+05 = Inct = 1400 outlet line

S. side - Line E

190.09 5.19

130	5.4	200.29 4.67	195.22 190.125 5.0 0.67
129+50	5.5	194.89 5.07	195.22 190.424 82

4.80

4.77

4.37

130 15 5' from Sta 1 - outlet

.600

BM 3.03 (187.26)

184.23

Spike S. side Trans Pole Sta 105496

104	0.7	0.09	187.17	183.20	3.97
+SD	1.7	1.26	186.00	182.15	3.85
105	2.8	2.31	184.95	181.10	3.85
+SD	3.9	3.32	183.94	180.05	3.89
106	4.8	4.29	182.97	179.00	3.97
+SD	5.9	5.39	181.87	177.95	3.92
107	6.7	6.16	181.10	176.90	4.20
+SD	7.3	6.72	180.54	176.60	3.94
108	5.0	4.33	179.89	176.30	3.59
+SD	5.5	4.98	179.24	176.00	3.74
109	6.0	5.55	178.67	175.70	2.97
+SD	6.4	5.84	178.38	175.40	2.98
110	6.7	6.12	178.10	175.10	3.00
+SD	6.8	6.20	178.02	174.80	3.22
111	6.9	6.42	177.80	174.50	3.30
+SD					

No Current

2.10%
0.6%

N. Side

178

011

BM	3.03	187.26	187.23	
		-0.		
104	0.30	-0.30	187.52	188.20
+SD	1.6	1.02	186.24	182.15
105	2.4	1.77	185.49	181.10
+SD	3.3	2.86	184.40	180.05
106	4.5	3.95	183.31	179.00
+SD	5.7	5.00	182.26	177.95
107	6.5	5.88	181.38	176.90
+SD	7.2	6.65	180.61	176.60
108	4.6	4.08	180.14	176.30
+SD	5.2	4.62	179.60	176.00
109	5.7	5.15	179.07	175.40
+SD	6.2	5.70	178.62	175.40
110	6.7	6.23	177.99	175.10
+SD	7.1	6.57	177.65	174.80
111	7.4	6.76	177.46	174.50
+SD				

No Overcast

BM 10.83 195.06 187.23

104	8.5		7.78	187.28	183.20
103+50	7.4		6.62	188.44	184.26
103	6.4		5.67	189.49	185.32
102+50	5.8		4.55	190.51	186.38
102	4.2		3.32	191.73	187.44
101+50	3.1		2.45	192.61	188.50
101	1.9		1.25	193.81	189.56
100+50	10.27 9.9	(204.08)	9.29	194.79	190.62
100	8.7	195.4	7.89	196.19	191.68
99+50	7.5	196.59	6.64	197.44	192.89
99	6.0		5.05	199.03	194.11
98+50	4.8		4.13	199.95	195.32
98	3.8		3.15	200.93	196.53
97+50	2.8		2.38	201.70	197.74
97	2.0		1.50	202.58	198.96
96+50	10.45 10.7	(213.53)	10.04	203.49	200.17
96	9.6		9.08	204.45	201.38
95+50	8.5		7.81	205.72	202.60
95	7.4		6.86	206.67	203.81
94+50	6.1		5.57	207.99	205.03
94	5.0		4.30	209.23	206.24
93+50	3.6		2.86	210.67	207.46
93	2.0		1.72	212.41	209.68
92+50	0.0		-0.50	214.03	209.89

4.08

4.18

4.17

4.13

4.29

4.11

4.25

4.17

4.51

4.55

4.92

4.63

4.40

3.96

3.62

3.32

3.07

3.12

2.86

2.96

2.99

3.21

3.73

4.14

No Overcut

3.42

3.69

Road tile outlet E Lichtys

Private - Relay

013

34
1.90
23BM 4.95 208.04
12.50

203.09

Center N wall Culv Sta 69+5-1

0 Top 6" tile	12.20	195.24 = Grade
0 10.9	10.17	197.87 195.25 2.62
+50 10.6	9.88	198.16 195.40 2.76
1 10.2	9.52	198.50 195.55 2.95
+50 9.7	198.3	8.89 199.15 195.90 3.45
1+50 9.6	8.50	199.54 195.70 3.84

S. Side

69+84	9.7	(208.04)	8.89	199.15	195.70	3.46
69+75	9.8		9.11	198.93	195.77	3.16
Hwy D	9.5	198.5				
69+50	6.8	201.2	5.70	202.34	196.00	6.34
69+25	6.9		6.21	201.83	197.00	4.83
69	6.8		6.70	201.94	198.00	3.94
68+50	6.2		5.48	202.56	198.75	3.81
68	5.4		4.83	203.21	199.50	3.71
67+50	4.4		3.81	204.23	200.25	3.98
67	3.3	204.74	2.70	205.34	201.00	4.34
66+50	2.1	205.94	1.36	206.68	201.75	4.93

2.60 = 69+84 - 5 Line
and = 69+185 Line
W of Culv

201
198.00
21 3.00
1.5

Inc +
= 69+38 N. Line

Note - These tile
lead to junction
By Bob Carroll
(Reduced 34')

3.74

4.19

N. Side

69+72 = Inset Private 6" Line

(208.04)

69+38	7.0	w 1.04	5.79	w 2.34	196.00	6.34
69+75						
69+100	6.7	w 1.34	6.13	201.91	198.00	3.91
68+50	6.4		5.87	202.17	198.75	3.42
68	5.8		5.02	203.02	199.50	3.52
67+50	4.6		3.91	204.13	200.25	3.88
67	3.4	w 1.64	2.69	205.35	201.00	4.35
66+50	2.3	w 5.74	1.64	206.40	201.75	4.65

5.04 = 69+50 S side
38' - .200

3.34

3.64

3.99

note - 34' additional
laid by Nels Sorenson
to Stealy's private line

S. Side

3. 32 100

015

BM	4.95	(208.02)		203.09			
69+18	9.6		8.50	199.64	195.70	3.84	
69+25	9.4	198.64	8.25	199.79	195.75	4.04	2.89 = 1450 Relay Light/sprink
Hwy D	9.5	198.5					
69+50	7.3	200.74	6.15	201.89	196.00	5.89	4.74 = 69+65 N Line
69+76	7.0	201.04	6.40	201.64	196.50	5.14	4.54 1.70
70	7.4	200.64	6.73	201.31	197.00	4.31	3.64 1.20
+50	7.3	200.94	6.70	201.34	197+25	4.09	
71	7.1	200.94	6.51	201.53	197+50	4.03	
+50	6.7	201.34	6.12	201.92	197+75	4.17	
72				198.00			
	4.01	(207.10)		203.09			
72	5.3		4.89	202.21	198.00	4.21	
+50	5.2		4.67	202.43	198.15	4.28	
73	5.1		4.57	202.53	198.30	4.23	
+50	5.1		4.68	202.42	198.45	3.97	
74	5.0		4.54	202.56	198.60	3.96	
+50	4.7		4.16	202.94	198.75	4.19	
75	4.5		3.81	203.29	198.90	4.39	
T.D	9.53	(212.84)	3.81	203.29			
+50	9.7		9.34	203.50	199.55	3.95	
76	9.1		8.48	204.36	200.20	4.16	
+50	8.2		7.64	205.20	200.85	4.35	
77	7.5		7.05	205.79	201.50	4.29	
+50	6.6		6.20	206.64	202.70	3.94	

No Cont No Cont

N. side

$$\begin{array}{r} 201.80 \\ 198.20 \\ \hline 3.60 \end{array}$$

BM 4.95 208.04

203.09

69+65-

70 7.5 6.84 201.20 197.00 4.20

+50 7.5 7.01 201.03 197.25 3.83 $\frac{1}{2}$ 71 7.6 7.11 200.93 197.50 3.43 $\frac{1}{2}$

+50 7.3 6.60 201.44 197.75 3.69

72 198.00

4.01 (207.10)

203.09

72 5.5 5.02 202.08 198.00 4.08

+50 5.1 4.93 202.17 198.15 4.02

73 5.2 4.73 202.37 198.35 4.02

+50 5.2 4.78 202.32 198.45 3.87

74 5.3 4.75 202.35 198.60 3.75

+50 5.1 4.65 202.45 198.75 3.70

75 4.8 4.23 202.87 198.90 3.97

T.P 9.55 (212.84) 3.81 203.29 1.26

+50 10.1 9.50 203.36 199.55 3.79

76 9.6 8.79 204.05 200.20 3.85

+50 8.7 8.20 204.64 200.85 3.79

77 7.8 7.26 205.28 201.50 4.08

+50 7.1 6.53 206.31 202.70 3.61

No Cont

No Cont

No Cont

0.30%

1.30%

5 Side
(212.84)

260 017

78	5.5		5.00	209.84	203.90	3.94
+50	4.5		3.91	208.93	205.10	3.83
79	3.6		2.75	210.09	206.30	3.79
+50	2.0		1.57	211.27	207.50	3.77
80	9.34	(220.98)	1.20	211.64	—	
80	8.8		8.38	212.60	208.70	3.90
+50	7.3	213.68	6.88	214.10	209.50	4.60
81	6.0	214.98	5.52	215.46	210.30	5.16
+50	4.9	216.08	4.30	216.68	210.50	6.18
82	4.8	216.18	3.98	217.00	210.70	6.30
+50	5.3	215.68	4.72	216.26	210.90	5.36
83	5.6	215.38	5.12	215.86	211.10	4.76
+50	6.0	214.98	5.50	215.48	211.30	4.18
84	6.1		5.44	215.54	211.50	4.04
+50	6.1		5.41	215.57	211.70	3.87
85	5.9		5.23	215.75	211.90	3.85
86	6.70	(222.45)	5.23	215.75	—	
+50	7.1		6.53	215.92	212.10	3.82
86	6.6		6.06	216.39	212.30	4.09
+50	6.1		5.49	216.96	212.65	4.31
87	6.0		5.34	217.11	213.00	4.11
+50	5.8		5.20	217.25	213.35	3.90
88	5.4		4.90	217.55	213.70	3.85
+50	5.0		4.47	217.98	214.05	3.93
89	4.5		3.97	218.48	214.40	4.08
+50					214.78	
90	3.5		3.06	219.39	215.10	4.29

7.60
201.50 7.80
210.20 201.10
210.20 209.30
201.50

4.18
4.68
5.58
5.48
4.78
4.28
3.68
4.00
1.100
1.500
1.200
1.600

no card

N Side

018

(212.84)

210.10

78	6.0	5.15	207.69	203.90	3.79
+50	1.7	4.03	208.81	205.10	3.71
79	3.4	2.75	210.04	206.30	3.74
+50	2.0	1.20	211.04	207.50	4.14

T.P	4.34	(220.98)	1.20	211.64	—
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80	9.0	8.34	212.64	208.70	3.94
----	-----	------	--------	--------	------

+50	7.5	213.48	6.82	214.16	209.50
-----	-----	--------	------	--------	--------

81	6.4	214.58	5.62	215.36	210.30
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+50	5.1	215.88	4.72	216.26	210.50
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82	5.1	215.88	4.72	216.28	210.70
----	-----	--------	------	--------	--------

+50	5.8	215.18	5.28	215.70	210.90
-----	-----	--------	------	--------	--------

83	6.0	214.98	5.56	215.42	211.10
----	-----	--------	------	--------	--------

+50	6.4	214.58	5.93	215.05	211.30
-----	-----	--------	------	--------	--------

84	6.4	214.58	5.97	215.01	211.50
----	-----	--------	------	--------	--------

+50	6.4		5.94	215.00	211.70
-----	-----	--	------	--------	--------

85	6.2		5.62	215.36	211.90
----	-----	--	------	--------	--------

T.P	6.70	(222.46)	5.23	215.75	—
-----	------	----------	------	--------	---

+50	7.1		6.65	215.80	212.10
-----	-----	--	------	--------	--------

86	6.7		6.18	216.27	212.30
----	-----	--	------	--------	--------

+50	6.2		5.77	216.68	212.65
-----	-----	--	------	--------	--------

87	6.1		5.82	216.93	213.00
----	-----	--	------	--------	--------

+50	5.9		5.47	216.98	213.35
-----	-----	--	------	--------	--------

88	5.6		5.07	217.38	213.70
----	-----	--	------	--------	--------

+50	5.0		4.41	218.04	214.05
-----	-----	--	------	--------	--------

89	4.4		3.85	218.60	214.40
----	-----	--	------	--------	--------

+50	3.7	218.75	3.12	219.33	214.75
-----	-----	--------	------	--------	--------

90	3.1	219.35	2.55	219.90	215.10
----	-----	--------	------	--------	--------

208.70

1.40

do

do

2

3.98

4.28

5.38

5.18

4.28

3.88

do

do

do

do

do

do

do

do

do

do

do

do

do

do

do

.200

.800

1.200

.700

4.00

4.25

.100

BM. 4.90 (203.98) 199.08

Relay Miller's 4"

0 top 4" tile 11⁺⁴⁰/₃₀ 192.28

0 9.3 8.66 195.32

+25 8.9 8.46 195.52

0 +50 top 4" tile 10⁺⁴⁰/₅₇ 193.01

(203.98)

E top 4" tile 10⁺⁴⁰/₅₇ 193.01 193.10

Culv Floor 9.63 194.35 —

48 8.2 7.67 196.31 193.10 3.21

47+50 7.7 6.99 196.99 193.20 3.69

47 7.2 6.70 197.28 193.50 3.78

46+50 6.2 5.47 198.57 194.25 4.26

46 5.2 4.57 199.41 195.00 4.41

45+50 4.8 4.15 199.83 195.35 4.48

45 4.5 3.75 200.23 195.70 4.53

44+50 4.5 4.01 199.97 196.05 3.92

44 4.7 4.05 199.93 196.40 3.53

BM 4.05 (203.13) 199.08

E top 4" tile 9⁺⁴⁰/₇₁ 193.02

48 7.4 6.73 196.40 193.10 3.30

+50 6.2 5.62 197.57 193.55 3.96

Gen. N. Howard & Culv Sta 47+90

At Sta 48.5 side = 0+50 Relay

= 0+50 Relay

no cont

note

N. Side

BM 4.90 (203.98) 199.08

.40
108
0032194.00
193.60

020

.40
42
80
160
1680

Top 4" tile	10.40	193.50	
Culv Floor	9.20	194.68	
48+08 6.9	6.42	197.56	193.57 3.99
48 6.8	6.30	197.68	193.69 4.08
+50 7.8	6.88	197.10	193.80 3.30
47 7.1	6.38	197.60	194.00 3.60
+50 5.8	5.20	198.68	194.50 4.18
46 5.0	198.98 4.57	199.41	195.00 4.41
+50 4.4	199.58 3.91	200.07	195.35 4.72
45 4.3	199.68 3.61	200.37	195.70 4.67
+50 4.2	199.78 3.46	200.52	196.05 4.47
44 4.4	3.48	200.50	196.40 4.10

398
4.23
3.98
1.00
1.00

BM 4.05 (203.13) 199.08

Top 4" tile	9.22	X 193.51
48+08 6.2	5.60	197.53 193.62 3.91
48+50 6.6	5.66	197.47 193.80 6.67

S-Side

194.00
193.10

021

203.13

49	5.2	197.93	4.48	198.65	194.00	4.65	3.93
+50	5.1	198.03	4.30	198.83	194.20	4.63	3.83
50	5.3	197.83	4.78	198.35	194.40	3.95	
+50	5.5	197.63	4.74	198.39	194.60	3.79	
51	5.4	197.73	4.83	198.30	194.80	3.50	
+50	5.2	197.93	4.34	198.79	195.00	3.79	
52	4.3	198.83	3.51	199.62	195.20	4.42	
+50	3.7	199.43	3.00	200.13	195.95	4.18	3.49
T.P.	9.94	210.71	2.36	200.77	—		
53	9.8	200.91	9.12	201.59	196.70	4.89	4.21
+50	9.5	201.21	8.67	202.04	197.45	4.59	3.76
54	9.1		8.27	202.44	198.20	4.22	
+50	8.4		7.70	202.97	198.95	4.02	
55	7.6		6.88	203.83	199.70	4.13	
+50	6.6		5.92	204.79	200.45	4.34	
56	5.9		5.15	205.56	201.20	4.36	
+50	5.1		4.40	206.27	201.95	4.32	
57	4.4		3.68	207.03	202.70	4.33	
+50	3.8		3.20	207.51	203.20	4.31	
58	3.5		2.90	207.81	203.70	4.11	

No Current

(203.13)

49	5.5		4.42	198.71	194.00	471	
+50	5.1		3.85	199.28	194.20	508	
50	5.5		4.55	198.58	194.40	518	
+50	5.6		4.54	198.59	194.60	599	
51	5.7		4.87	198.26	194.80	546	
+50	5.3		4.59	198.54	195.00	554	
52	4.4		3.62	199.51	195.20	531	
+50	3.1	200.03	2.36	200.77	195.95	582	4.08
T.P	9.94	(210.71)	2.36	200.77	—	—	4.71
53	9.3	201.41	8.80	201.91	196.70	521	
+50	9.3	201.41	8.57	202.14	197.45	569	3.96
54	8.7	202.01	7.90	202.81	198.20	561	3.81
+50	8.0	202.71	7.57	203.14	198.95	519	
55	7.3		6.66	204.05	199.70	535	
+50	6.4		5.75	204.96	200.45	551	
56	5.5	205.21	4.95	205.76	201.20	556	4.01
+50	4.8	205.91	4.02	206.69	201.95	574	3.96
57	4.1	206.61	3.42	207.29	202.70	559	3.91
+50	3.7	207.01	3.02	207.69	203.20	549	
58	3.3		2.72	207.99	203.70	529	

510
4.

—

4.08
4.71400
400

1.50

4.01
3.96
3.91

700000

1.00

13M 3.61 (226.10) 22250 Spike E Gate post N. side Sta 145+58

144	6.6	219.51	5.93	220.18	215.60	4.58	3.91
+50	5.8	220.31	5.25	220.86	216.10	4.76	4.21
145	5.6	220.51	5.08	221.03	216.60	4.43	3.91
+50	5.1	221.01	4.53	221.56	216.70	4.86	4.31
146	5.1	221.01	4.54	221.57	216.80	4.77	4.21
+50	4.8	221.31	4.32	221.79	216.90	4.89	4.41
147	4.9	221.21	4.30	221.81	217.00	4.81	4.21
+50	4.7	221.41	4.24	221.87	217.10	4.77	4.31
148	4.6	221.51	4.09	222.02	217.20	4.82	4.31
+50	4.6	221.51	4.08	222.03	217.30	4.73	4.21
149	4.5	221.61	3.88	222.23	217.40	4.83	4.21
+50	4.1	222.01	3.43	222.68	217.60	5.08	4.41
150	4.1	222.01	3.55	222.56	217.80	4.76	4.21
T.P.	9.10	(231.76)	3.55	(222.56)			
+50	9.5	222.26	8.73	223.03	218.00	5.03	4.26
151	9.1	222.66	8.48	223.28	218.20	5.08	4.46
+50	8.6	223.16	8.06	223.70	218.80	4.90	4.36
152	7.7	224.06	7.15	224.61	219.40	5.21	4.66
+50	7.4	224.36	6.79	224.97	220.30	4.61	4.06
153	6.5	225.26	6.05	225.71	221.20	4.51	4.06
+50	5.6	226.16	5.00	226.76	222.10	4.66	4.06
154	4.5	227.26	3.98	227.78	223.00	4.78	4.26
+50	3.7	228.06	3.31	228.45	223.90	4.53	4.16
155	2.9	228.86	2.33	229.43	224.80	4.63	4.06

T.P. 1.36 2296.5 3.47 228.29

No Current

BM	3.61	(226.11)		222.50					
144	6.5	219.61	5.94	220.17	215.60	4.57	do	4.01	.100
+50	5.9	220.21	5.40	220.71	216.10	4.61	8	4.11	
145	5.7	220.41	4.88	221.23	216.60	4.63		3.81	
+50	5.2	220.91	4.50	221.61	216.70	4.91		4.21	.200
146	5.1	221.01	4.53	221.58	216.80	4.78		4.21	.300
+50	4.8	221.31	4.34	221.77	216.90	4.84		4.41	.300
147	4.8	221.31	4.25	221.86	217.00	4.86	do	4.31	.300
+50	4.7	221.41	4.11	222.00	217.10	4.90	N	4.31	.100
148	5.0	221.11	4.22	221.89	217.20	4.69	0	3.91	.100
+50	4.5	221.61	3.70	222.41	217.30	5.11		4.81	.500
149	4.1	222.01	3.62	222.49	217.40	5.09		4.61	.200
+50	4.7	221.41	3.97	222.14	217.60	4.54	do	3.81	
150	4.9	221.21	4.05	222.06	217.80	4.26	do	3.21	
T.P.	9.10	(231.66)	8.55	222.56	217.80	4.26	do	3.21	
+50	9.3	222.33	8.81	222.45	218.00	4.45	0	4.33	.300
151	9.2	222.46	8.49	223.17	218.20	4.97	do	4.26	.300
+50	8.6	223.06	7.82	223.84	218.80	5.04	do	4.26	.300
152	8.0	223.66	7.40	224.26	219.40	4.86		4.26	.200
+50	7.3	224.33	6.84	224.82	220.30	4.52		4.03	
153	6.6	225.06	5.96	225.70	221.20	4.50		3.86	
+50	5.5	226.16	4.82	226.84	222.10	4.74	do	4.06	.300
154	4.1	227.56	3.76	227.90	223.00	4.90		4.56	.400
+50	3.6	228.06	3.15	228.51	223.90	4.61		4.16	
155	3.1	228.66	2.54	229.12	224.80	4.32		3.76	

229.65

156	1.4	228.25	0.87	228.78	224.00	4.78	4.25
+50	2.3	227.35	1.84	227.81	223.10	4.71	4.25
157	3.3	226.35	2.82	226.83	222.20	4.63	4.15
+50	4.5	225.15	3.96	225.69	221.30	4.39	3.85
158	5.6	224.05	5.06	224.59	220.40	4.19	3.65
+50	6.4	223.25	5.81	223.85	219.50	4.35	3.75
159	7.3	222.35	6.74	222.91	218.60	4.31	3.75
+50	8.0	221.65	7.42	222.23	217.95	4.28	3.70
160	9.2	220.45	8.69	220.96	217.30	3.66	3.15
+50	9.9	219.75	9.32	220.33	217.20	3.13	
+85	10.4	219.25	9.89	219.76	217.13	3.63	
161	10.5	219.16	9.92	219.73	217.10	2.63	
161+08	10.1	219.55	9.31	220.34	217.08	3.26	
± Colv.			12.65	217.00			
B.M.			8.53	221.12			

3.2
3.2
3.2

S. Side

(183.82)

026

111 $\pm$		⁺⁶⁰ 8.77	174.55			
111 6.6		5.64	178.18	174.50	3.68	5.0
+50 6.2	177.62	5.46	178.42	174.18	4.24	6.4
112 3.8	180.02	3.05	180.79	193.86	6.91	0
+09 $\pm$		10.02	173.80			

3.44

6.16

8000

(183.82)

112130 $\pm$ 4.2		9.70	174.12	174.12		
+50 5.1		4.20	179.62	174.41	5.21	
113 6.8		6.06	177.76	175.14	2.62	
+50 6.7		6.11	179.71	175.86	3.85	

1.4170

No

(183.82)

N. Side

111450 $\pm$		⁺⁶⁰ 9.66	174.76			
111+50 7.2		6.46	177.42	174.16	3.26	
112 8.6		7.72	176.10	173.80	2.30	
+08 $\pm$		10.10	173.72	173.7		

0.7650

No

183.82

112131 $\pm$		9.60	174.02			
+50 7.7		7.03	176.79	174.40	2.39	
113 7.9		7.05	176.82	175.48	1.42	
1131 $\pm$ 8.02		⁺⁶⁰ 8.02	175.20			

0.7650

No

South Side

B.M. 633 (196.90) 19063

At Top Millers 4" line across (R) ⁺⁴⁰ 11.83 184.73

39+28

184.90

+50 77 189.26 6.82 190.14 185.45 4.69

40 72 189.76 6.20 190.76 186.80 3.96

40+50 60 190.96 5.07 191.89 188.15 3.74

41 4.5 3.64 193.32 189.50 3.82

+50 2.5 1.69 195.27 191.00 4.27

I.P. 8.12 (203.36) 1.72 195.24 —

42 7.5 6.79 196.57 192.50 4.07

+50 59 5.26 198.10 194.00 4.10

43 4.8 4.14 199.22 195.50 3.72

+50 4.2 3.31 200.05 196.00 4.05

44 4.1 3.30 200.06 196.50 3.56

2.70% 3.81

2.96

3.81

3.00%

1.00%

No Dent

No Dent

North Side

BM 6.33 196.96 190.63 Gen. N. H. Wall, Conc. 6-11-39+30

+ 4.0
11.53 185.01

FE 39+31 185.08 5/6

+50 8.1 7.24 189.72 185.60 4.12 5/6

40 7.3 6.54 190.42 186.90 3.52 N

+60 6.3 5.44 191.52 188.20 3.82

41 4.1 3.89 193.07 189.50 3.54

+50 2.5 1.72 195.24 191.00 4.24

T.P. 8.12 203.30 1.72 196.24

42 6.8 196.66 6.05 197.31 192.50 4.81 3.00 4.06

+50 5.3 198.06 4.67 198.69 194.00 4.69 3.00 4.06

43 4.4 3.73 199.63 195.50 4.13

+50 3.9 3.01 200.35 196.00 4.35

44 3.6 2.76 200.60 196.50 4.10 1.00

W. L. Wall

.100

B.M. 7.21 197.84 190.63

At top of 12⁴⁰ 184.73

39+28

39 9.0

8.32 189.52 185.20 4.32 1.60

38 8.9

8.12 189.72 186.00 3.72

38 8.5

7.84 190.10 186.80 3.20 1.60

37+50 7.2

6.63 191.21 187.60 3.61

37 6.0

5.04 192.80 188.40 4.40

36+50 5.0

4.35 193.49 189.35 4.14

36 3.9

3.18 194.66 190.30 4.36

35+50 3.3

2.42 195.42 191.25 4.17

T.P. 8.82

(204.24) 2.42 195.42

35 9.0

8.44 195.80 192.20 3.60 1.90

34+50 8.2

7.63 196.61 193.15 3.46

34 7.2

6.73 197.51 194.10 3.41

33+50 6.1

5.44 198.80 195.05 3.75

33 5.1

199.14 4.23 200.01 196.00 4.01

32+50 4.0

200.01 3.24 201.00 196.20 4.80 4.01

No Overcut

3.14

4.01

13711	7.21	197.84		190.63	
17 top 4"		^{+ .40} 12.48	184.99		
39+31					
39	8.7		8.12	189.72	185.60 4.12
38+50	8.6		7.82	190.02	186.30 3.72
38	7.7		7.15	190.69	187.02 3.69
37+50	7.0		6.39	191.45	187.70 3.75
37	5.9		5.38	192.46	188.40 4.06
36+50	4.5	193.34	4.05	193.79	189.35 4.44
36	3.6	194.24	2.95	194.89	190.30 4.59
35+50	2.5	195.34	1.96	195.88	191.25 4.63
35	8.82	(204.24)	2.42	195.42	
35	8.2	196.04	7.59	196.65	192.20 4.45
34+50	7.4		6.65	197.59	193.15 4.44
34	6.6		5.97	198.27	194.10 4.17
33+50	5.6		4.88	199.36	195.05 4.31
33	4.2		3.49	200.75	196.00 4.75
32+50	3.4		2.81	201.43	196.20 5.23

3.99

3.94

17.09

1.90

No Overcut

B.M. S. 40 (19690) 191.50 Nail S side trans pole 27402

LE		8.40		188.50			
27401	7.2	6.60	190.30	188.60	1.70		
+SD	7.3	6.72	190.18	188.77	1.41		
28	7.0	6.39	190.51	188.95	1.56		
+SD	6.5	5.80	191.10	189.12	1.98		
29	5.7	5.12	191.78	189.30	2.48		
+SD	4.5	3.81	193.09	190.05	3.04		
30	3.1	2.39	194.51	190.80	3.71		
+SD	10.1	9.25	195.82	192.05	3.77		
31	8.3	7.55	197.52	193.30	4.22	3.47	
+SD	6.3	5.45	199.62	194.55	5.07	4.22	.100
32	5.3	4.41	200.66	195.80	4.86	3.97	.100
+SD	4.8	4.05	201.02	196.05	5.02	7.27	

BM 5.40 (196.92) 191.50

ft		8.10	188.50		
27+01	7.0	6.27	190.63	188.90	1.73
+50	7.1	6.32	190.58	189.00	1.58
28	6.7	6.50	190.90	189.10	1.80
+50	6.5	5.80	191.10	189.20	1.90
29	5.9	5.25	191.65	189.30	2.35
+50	4.6	3.83	193.07	190.05	3.02
30	3.2	2.39	194.57	190.80	3.71
+50	9.9	9.09	195.98	192.05	3.93
31	8.1	7.26	197.81	193.30	4.51
+50	6.3	5.52	199.55	194.65	5.00
32	4.7	3.75	201.32	195.80	5.52
+50	4.2	3.52	201.55	196.00	5.55

BM 5.50 (197.00) 191.50

ft		8.20	188.50		
26+99	7.0	6.33	190.67	188.90	.77
26+50	7.1	6.40	190.60	189.00	1.60
26	6.7	5.88	191.12	189.10	2.02
25+50	5.7	5.03	191.97	189.20	.77
25	5.1	4.36	192.64	189.30	3.34
24+50	4.1	3.42	193.58	189.65	3.93
24	3.4	2.62	194.38	190.00	.38

Est 700 / Includes Labor

13/10 8.34 170.44 162.10 500 W Wall Culv W 100 Eagle C. Rd

0+20=0	11.0		10.22	160.22	157.85	2.47	1.8%	
0+50	10.0		9.20	161.24	157.81	3.43		
1	9.6		8.92	161.52	157.90	3.62		
+50	8.4		7.77	162.67	158.70	3.97	1.60%	
2	7.1	163.34	6.34	164.10	159.50	1.60		3.84
+50	5.7	164.74	5.14	165.30	160.80	1.60		3.94
3	4.7	165.74	3.94	166.50	162.10	1.40	3.64	
+50	3.5		2.96	167.48	163.40	1.08		
4	2.1		1.43	169.01	164.70	1.31		
+50	10.0	(179.69)	9.18	170.51	166.00	1.51		
5	8.6		8.02	171.67	167.30	1.37		
+50	7.3	172.39	6.60	173.09	168.60	1.49	3.79	
6	5.8	173.89	5.21	174.48	169.90	1.58	3.99	
+50	4.2	175.49	3.58	176.11	171.20	1.91	4.29	
7	3.0	176.69	2.50	177.19	172.50	1.69	4.19	
+50	1.8	177.89	1.11	178.58	173.25	1.33	4.64	
8	4.6	(182.87)	4.10	178.77	174.00	1.77	4.27	
+50	4.8	178.27	4.20	178.67	174.18	1.49	3.89	
9	5.3		4.72	178.15	174.36	1.79		
+50	5.3		4.69	178.18	174.54	1.64		
10	5.5		4.92	177.95	174.72	1.23		

1.00%

2.00%

3.00%

4.00%

5.00%

Cont. on page 67

BMO	8.34	(170.44)	162.10		
± colr			12.83	157.61	
0+10	10.0		9.25	161.19	157.70 3.49
0+20	10.4		9.64	160.80	157.72 3.08 1.0
0+35.0	11.0		10.22	160.22	157.75 2.47 N
0+50	11.0		10.30	160.14	157.80 2.34
1	10.1		8.97	161.47	157.90 3.57
+50	8.6		7.78	162.66	158.70 3.96
2	7.6		6.76	163.68	159.50 4.18 1.60
+50	6.3		5.61	164.83	160.80 4.03
3	5.7		4.88	165.56	162.10 3.46
+50	4.5		3.68	166.76	163.40 3.36 2.60
4	3.0		2.47	167.97	164.70 3.27
+50	10.6	(179.69)	9.88	169.81	166.00 3.81
5	9.0		8.39	171.30	167.30 4.00
+50	7.9		7.12	172.57	168.60 3.97
6	6.3		5.61	174.08	169.90 4.18
+50	4.9		4.09	175.60	171.20 4.40
7	3.7	176.0	2.91	196.78	172.50 4.28
+50	2.3	177.39	1.60	178.07	173.25 4.84
8	5.4	(182.87)	4.67	178.20	174.00 4.20 1.50
+50	5.4	177.47	4.85	178.02	174.18 3.84
9	6.0		5.36	177.57	174.36 3.15
+50	5.9		5.23	177.64	174.54 3.10 2.60
10	5.7		5.01	177.86	174.73 3.14

No Overlap

Sta Grade Station Dist. to
Cut Fill Fill Cut Back Slope Lt Rt

161+203

160+50 $\frac{C23 F20}{26 \ 157} \frac{F18}{15.5} - 26-10 \text{ cut } 218.80 \ 219.80$

160 $\frac{C29 F18}{25 \ 15} \frac{F13}{14.8} = 25-70 \text{ cut } 218.50 \ 220.75$

159 $\frac{C30 F17}{24 \ 154} \frac{F10}{14.5} \frac{C02}{19.174} \text{ Set } 0.0 \ 220.00 \ 222.60 \ 20.00$

158 $\frac{C21 F21}{24 \ 16} \text{ not set } \frac{C03}{14.5} \text{ Set } 0.0 \ 221.50 \ 224.45 \ 15.0$

T.P. $1.96 \ (225.78) \ 10.95 \ 223.82$

157 $\frac{C23 F11}{24 \ 145} \frac{F02}{133} \frac{C04}{203} \text{ Set } 0.0 \ 224.20 \ 226.30 \ 4.20$

156 $\frac{C33 F05}{24 \ 136} \text{ not set } \frac{C16}{21.6} \text{ Set } 0.0 \ 226.00 \ 228.15 \ 26.00$

+50

155 $\frac{C30 F08}{24 \ 17} \text{ not set } \frac{C06}{21} \text{ Set } 0.0 \ 227.00 \ 228.97 \ 27.00$

+50

154 $\frac{C24 F14}{24 \ 15} \frac{F07}{140} \frac{00}{215} \text{ Set } 0.0 \ 225.5 \ 227.71 \ 25.5$

T.P. $8.43 \ (234.77) \ 1.64 \ 226.34$

227.98

$\frac{220.5}{5.3}$	$\frac{220.0}{5.8}$	$\frac{218.0}{7.8}$	$\frac{216.1}{7.7}$	$\frac{214.2}{6.2}$	$\frac{212.6}{6.2}$	$\frac{210.5}{7.3}$	$\frac{208.5}{7.3}$	$\frac{206.5}{7.3}$	$\frac{204.5}{7.3}$
$\frac{221.9}{3.9}$	$\frac{221.2}{5.6}$	$\frac{219.6}{7.2}$	$\frac{218.6}{7.2}$	$\frac{220.1}{5.7}$	$\frac{220.6}{5.2}$	$\frac{220.7}{5.1}$	$\frac{220.0}{5.8}$	$\frac{218.5}{5.8}$	$\frac{216.4}{5.8}$
$\frac{223.5}{2.3}$	$\frac{222.6}{3.2}$	$\frac{220.2}{5.6}$	$\frac{220.1}{5.7}$	$\frac{221.8}{4.0}$	$\frac{222.5}{3.3}$	$\frac{222.6}{4.2}$	$\frac{220.2}{5.6}$	$\frac{220.2}{5.6}$	$\frac{221.4}{4.4}$
$\frac{224.0}{1.8}$	$\frac{223.5}{2.3}$	$\frac{221.5}{4.0}$	$\frac{221.5}{4.0}$	$\frac{223.3}{2.3}$	$\frac{223.8}{2.0}$	$\frac{223.9}{4.4}$	$\frac{223.5}{4.4}$	$\frac{221.8}{4.0}$	$\frac{223.3}{4.0}$
$\frac{226.6}{5.2}$	$\frac{226.6}{5.2}$	$\frac{224.5}{6.3}$	$\frac{224.4}{6.3}$	$\frac{225.9}{5.9}$	$\frac{226.4}{5.4}$	$\frac{226.5}{4.3}$	$\frac{225.9}{4.6}$	$\frac{224.5}{4.6}$	$\frac{223.0}{2.8}$
$\frac{229.5}{5.3}$	$\frac{229.5}{5.3}$	$\frac{227.2}{7.6}$	$\frac{227.2}{7.6}$	$\frac{229.7}{5.5}$	$\frac{229.3}{5.5}$	$\frac{229.2}{5.4}$	$\frac{228.9}{5.9}$	$\frac{227.5}{7.3}$	$\frac{229.7}{5.1}$
$\frac{230.4}{4.4}$	$\frac{230.2}{4.6}$	$\frac{230.3}{4.5}$	$\frac{227.8}{7.0}$	$\frac{229.4}{5.2}$	$\frac{230.2}{4.6}$	$\frac{230.1}{4.4}$	$\frac{229.5}{5.0}$	$\frac{228.0}{5.5}$	$\frac{230.3}{4.5}$
$\frac{230.4}{4.7}$	$\frac{230.9}{4.8}$	$\frac{227.6}{7.2}$	$\frac{229.2}{5.6}$	$\frac{229.7}{5.7}$	$\frac{229.9}{4.9}$	$\frac{229.2}{5.6}$	$\frac{227.5}{7.3}$	$\frac{227.5}{5.1}$	$\frac{229.7}{5.1}$
$\frac{229.0}{5.6}$	$\frac{228.8}{6.0}$	$\frac{229.5}{5.8}$	$\frac{226.6}{8.2}$	$\frac{228.1}{5.7}$	$\frac{228.6}{6.2}$	$\frac{228.7}{6.1}$	$\frac{228.1}{6.7}$	$\frac{226.5}{8.3}$	$\frac{228.7}{6.1}$
$\frac{228.0}{6.8}$	$\frac{227.9}{8.9}$	$\frac{225.5}{9.3}$	$\frac{227.5}{7.0}$	$\frac{227.2}{7.6}$	$\frac{227.5}{7.2}$	$\frac{226.8}{8.0}$	$\frac{225.0}{9.3}$	$\frac{227.5}{7.3}$	$\frac{227.7}{7.0}$

450

115 $\frac{2.1}{29}$ $\frac{3.0}{17.2}$ $\frac{3.6}{18}$ $\frac{1.0}{29}$ 29.29 176.5 180.19

450

114 $\frac{1.0}{29}$ $\frac{4.4}{19}$ $\frac{4.4}{19}$ $\frac{1.5}{29}$ 29.29 175.20 180.00

~~118~~

~~29 29 175.0 180.0 0.0~~

~~450~~

~~112~~

BM 5.84 (186.11) 180.27

144 $\frac{4.1}{25}$ $\frac{1.3}{148}$ $\frac{0.1}{13.222}$ $\frac{0.7}{0.7}$ 25.2500 217.00 219.61500

143 $\frac{3.6}{25}$ $\frac{2.3}{16.4}$ $\frac{0.7}{14}$ $\frac{0.0}{21}$ 25.2500 215.00 217.64500

TD 8.08 (222.68) 3.32 214.60

142 $\frac{3.2}{25}$ $\frac{2.2}{16.4}$ $\frac{1.0}{18.4}$ $\frac{0.0}{20}$ 25.2500 213.00 215.68300

141 $\frac{3.2}{25}$ $\frac{2.3}{16.4}$ $\frac{0.8}{14.2}$ $\frac{1.4}{25}$ 25' 25' 213.72400

140 $\frac{3.1}{25}$ $\frac{2.3}{16.1}$ $\frac{0.9}{14.2}$ $\frac{2.1}{25}$ 25' 25' 209.20 211.76920

(217.92)

Handwritten calculations and corrections on the right side of the page, including various numbers and fractions, some crossed out, and a large '038' written vertically.

124	1.4 28	0.3 13.5	0.2 13.3	3.0 28	28 - 28	194.5	197.00	195.6 195.9 196.1 196.6 197.1 197.6 197.5 196.6 195.9 197.1 197.3 197.5
123	1.6 29	0.3 13.5	0.2 13.3	3.1 29	29 - 29	194.2	197.00	195.6 195.9 196.1 196.6 197.1 197.6 197.5 196.6 195.9 197.1 197.3 197.5
122	1.4 29	0.8 14.2	0.6 13.9	2.6 29	29 - 29	194.00	197.00	195.6 195.9 196.1 196.6 197.1 197.6 197.5 196.6 195.9 197.1 197.3 197.5
+50								
121.0	1.2 29	0.6 13.8	0.7 14	2.2 29	29 - 29	193.7	196.23	195.6 195.9 196.1 196.6 197.1 197.6 197.5 196.6 195.9 197.1 197.3 197.5
+50								
T.D	7.2	201.93	1.69	194.41				
120	1.9 29	2.4 29	2.9 - 29	191.3				
119	4.4 29	2.6 29	29 - 29	188.3				
118.0	4.6 29	2.1 29	29 - 29	185.00				
117	12.45 3.5 29	196.10 0.7 13.9	2.46 0.9 14.2	183.65 2.9 29	29 - 29	182.00	184.64	195.6 195.9 196.1 196.6 197.1 197.6 197.5 196.6 195.9 197.1 197.3 197.5
+50								
116	2.6 29	0.9 14.2	0.8 13	2.0 29	29 - 29	179.0	181.74	195.6 195.9 196.1 196.6 197.1 197.6 197.5 196.6 195.9 197.1 197.3 197.5

91450

91

 $\frac{1.5}{23} \quad \frac{2.3}{16.1} \quad \frac{0.4}{13.6} \quad \frac{2.2}{23} \quad \text{to strike} \quad 23-23 \quad 215.8$

217.88

90+50

90

 $\frac{3.2}{233} \quad \frac{0.0}{13} \quad - \quad \frac{1.3}{22} \quad \text{Bottom} \quad 20-20 \quad 216.90$

218.94

89+50

~~88~~ 89
 $\frac{1.6}{15.2} \quad \frac{0.7}{14.0} \quad -$

218.50

B.M.

9.24 (223.02)

213.78

like S. side Trans pole Sta 93+43

129

29 29 193.5 197.00

128

 $\frac{0.7}{28} \quad \frac{1.1}{14.8} \quad \frac{1.6}{15.2} \quad \frac{1.7}{28} \quad 28 \quad 28 \quad 194.0$

197.00

127

 $\frac{0.8}{28} \quad \frac{1.6}{15.3} \quad \frac{1.8}{15.6} \quad \frac{1.9}{28} \quad 28 \quad -28 \quad 194.2$

197.00

126

 $\frac{0.4}{28} \quad \frac{1.4}{15} \quad \frac{1.2}{15} \quad \frac{1.7}{28} \quad 28 \quad 28 \quad 194.5$

197.00

125

 $\frac{1.2}{28} \quad \frac{0.7}{14} \quad \frac{0.6}{13.7} \quad \frac{2.5}{28} \quad 28 \quad -28 \quad 194.5$

197.00

B.M.

3.63 (201.37)

197.74

enter N. Wall Conc Curb Sta 13+07

$\frac{215.6}{24}$	$\frac{215.6}{22}$	$\frac{214.6}{15}$	$\frac{216.2}{12}$	$\frac{216.8}{62}$	$\frac{216.3}{13}$	$\frac{215.2}{16}$	$\frac{215.1}{18}$	$\frac{216.2}{21}$	$\frac{217.6}{28}$	$\frac{218.0}{30}$	
$\frac{217.2}{26}$	$\frac{217.3}{22}$	$\frac{216.0}{17}$	$\frac{215.9}{15}$	$\frac{217.2}{12}$	$\frac{218.2}{48}$	$\frac{217.7}{13}$	$\frac{216.3}{17}$	$\frac{216.2}{18}$	$\frac{217.2}{20}$	$\frac{217.8}{23}$	$\frac{218.7}{26}$
$\frac{216.1}{28}$	$\frac{215.1}{24}$	$\frac{215.3}{16}$	$\frac{218.1}{12}$	$\frac{219.0}{16}$	$\frac{219.0}{13}$	$\frac{217.4}{17}$	$\frac{217.4}{19}$	$\frac{217.7}{20}$	$\frac{217.2}{21}$	$\frac{217.6}{22}$	
$\frac{219.2}{38}$	$\frac{218.9}{41}$	$\frac{217.8}{32}$	$\frac{219.0}{40}$	$\frac{219.8}{32}$	$\frac{219.2}{37}$	$\frac{217.8}{18}$	$\frac{217.7}{20}$	$\frac{218.4}{23}$	$\frac{219.3}{26}$	$\frac{219.32}{30}$	
$\frac{219.6}{34}$	$\frac{219.1}{37}$	$\frac{218.9}{17}$	$\frac{218.8}{12}$	$\frac{219.2}{13}$	$\frac{218.5}{12}$	$\frac{217.0}{18}$	$\frac{217.0}{20}$	$\frac{218.6}{24}$	$\frac{218.4}{26}$		
$\frac{219.1}{29}$	$\frac{218.5}{23}$	$\frac{217.0}{17}$	$\frac{217.0}{12}$	$\frac{218.2}{13}$	$\frac{218.5}{13}$	$\frac{218.1}{18}$	$\frac{216.9}{22}$	$\frac{217.1}{22}$	$\frac{217.7}{25}$	$\frac{217.66}{30}$	
$\frac{194.8}{42}$	$\frac{195.1}{33}$	$\frac{195.3}{25}$	$\frac{195.6}{76}$	$\frac{196.3}{51}$	$\frac{196.5}{49}$	$\frac{196.3}{8}$	$\frac{196.1}{10}$	$\frac{195.9}{14}$	$\frac{194.6}{17}$	$\frac{195.7}{24}$	$\frac{197.1}{30}$
$\frac{195.8}{53}$	$\frac{195.4}{44}$	$\frac{194.1}{20}$	$\frac{194.0}{23}$	$\frac{195.7}{14}$	$\frac{196.2}{52}$	$\frac{196.5}{49}$	$\frac{196.2}{79}$	$\frac{195.9}{14}$	$\frac{194.8}{17}$	$\frac{195.3}{21}$	$\frac{196.2}{30}$
$\frac{195.5}{53}$	$\frac{195.9}{25}$	$\frac{194.6}{23}$	$\frac{194.2}{18}$	$\frac{196.4}{14}$	$\frac{196.2}{10}$	$\frac{197.1}{42}$	$\frac{196.4}{6}$	$\frac{196.2}{17}$	$\frac{195.7}{22}$	$\frac{196.9}{25}$	$\frac{198.2}{30}$
$\frac{195.5}{32}$	$\frac{195.9}{26}$	$\frac{194.6}{21}$	$\frac{194.2}{19}$	$\frac{196.4}{14}$	$\frac{196.2}{8}$	$\frac{197.1}{42}$	$\frac{196.4}{6}$	$\frac{196.2}{17}$	$\frac{195.7}{22}$	$\frac{196.9}{25}$	$\frac{198.2}{30}$

T.P.	0.88	189.54	8.35	189.46	189.51	189.71	187.1	188.7	189.2	186.5	187.6	190.8	190.69					
103	$\frac{2.2}{29}$ $\frac{2.4}{16.3}$ $\frac{1.2}{14.5}$ $\frac{3.7}{29}$	29-29	189.00	189.56	7.0	32	23	18	16	13	84	9	15	17	23	7.74	33	
102	$\frac{2.2}{29}$ $\frac{1.8}{15.5}$ $\frac{1.7}{15.4}$ $\frac{2.9}{29}$	29-29	189.50	191.69	2.50	32	30	24	18	17	12	62	9	10	18	22	5.33	33
101	$\frac{1.7}{28}$ $\frac{2.2}{16.0}$ $\frac{0.9}{14.2}$ $\frac{2.6}{28}$	28-28	191.80	193.81	1.80	32	22	18	16	14	39	42	13	13	17	24	2.3	30
100	$\frac{2.0}{26}$ $\frac{0.0}{13.5}$ $\frac{0.7}{14}$ $\frac{3.0}{26}$	25-26	193.50	195.94	3.50	33	22	18	15	13	17	9	14	17	24	2.8	28	
T.P.	0.25	(197.81)	7.57	197.56	199.44	196.9	196.8	196.2	198.9	198.5	197.8	196.5	199.0	199.24				
99	$\frac{2.6}{25}$ $\frac{0.0}{13}$ $\frac{0.3}{13.4}$ $\frac{3.1}{25}$	25-25	196.0	198.06	6.00	31	22	17	16	13	63	6	13	17	22	5.89	33	
98	$\frac{2.4}{25}$ $\frac{0.0}{13}$ $\frac{0.0}{13}$ $\frac{3.3}{25}$	25-25	198.00	200.19	8.00	32	22	17	16	12	42	44	14	17	22	3.9	31	
97	$\frac{2.1}{25}$ $\frac{0.7}{14}$ $\frac{0.4}{13.6}$ $\frac{2.8}{25}$	25-25	200.00	202.31	0.00	33	22	18	16	13	20	26	10	14	17	23	2.3	25
T.P.	1.88	(205.13)	7.94	203.25	204.5	203.9	203.6	204.4	203.8	202.6	202.5	204.1	204.4	204.4				
96	$\frac{2.5}{25}$ $\frac{2.4}{16.3}$ $\frac{1.2}{14.7}$ $\frac{2.4}{25}$	25-25	202.00	204.44	2.00	23	22	17	16	13	66	9	14	16	18	22	6.8	30
95	$\frac{2.4}{25}$ $\frac{2.7}{16.8}$ $\frac{0.7}{14}$ $\frac{2.4}{25}$	25-25	204.50	206.9	2.50	33	23	17	16	11	45	47	9	14	17	21	4.5	30
94	$\frac{2.0}{25}$ $\frac{2.7}{17.0}$ $\frac{1.5}{15.0}$ $\frac{2.4}{25}$	25-25	207.00	209.70	1.00	22	23	18	15	11	18	26	13	17	21	24	1.8	30
93	0.15	(211.19)	11.98	211.04	211.9	211.0	210.0	211.7	212.1	211.9	210.3	212.4	212.4	213.1				
92	$\frac{2.7}{24}$ $\frac{2.8}{16.9}$ $\frac{2.0}{15.9}$ $\frac{2.6}{24}$	24-24	210.00	212.50	0.00	24	20	17	15	11	10	9	11	12	16	22	10.2	28
91	$\frac{1.4}{14}$ $\frac{2.2}{16}$ $\frac{0.6}{13.8}$ $\frac{2.4}{24}$	24-24	213.00	215.36	0.00	8.0	8.6	9.1	9.6	8.1	17	8.2	9.4	9.3	8.0	6.9	6.5	6.5
90			223.02			26	21	18	15	12	17	14	17	21	22	25	30	

[illegible]

450

T.P

2.56 (213.33) 3.96 210.97

63

 $\frac{3.1}{27} \frac{2.1}{15.9} \frac{2.3}{16.1} \frac{2.2}{2.5}$ 27-25 208.00 210.75

62

 $\frac{3.3}{27} \frac{2.4}{16.5} \frac{2.8}{16.9} \frac{2.3}{2.5}$ 27-25 207.50 210.50

450

61

 $\frac{3.3}{27} \frac{1.4}{15.0} \frac{3.2}{17.5} \frac{2.9}{2.5}$ 27-25 207.00 210.22

450

60

 $\frac{3.3}{27} \frac{1.7}{15.4} \frac{3.0}{18.2} \frac{3.2}{2.5}$ 27 25 206.50 209.69

450

59

 $\frac{2.4}{27} \frac{2.7}{16} \frac{2.9}{17} \frac{3.3}{2.5}$ 27-25 205.80 208.88

450

58

 $\frac{2.0}{27} \frac{1.7}{15.4} \frac{1.0}{14.5} \frac{2.5}{2.5}$ 27-25 205.30 207.83

TLESTKNA

6.74

(214.73)

201.99

TLESTK53

6.92

(214.73)

201.81

2111 2107 2106 2105 2103 2082 2061 2117 2106
 $\frac{2.2}{29} \frac{2.4}{24} \frac{4.5}{19} \frac{4.7}{19} \frac{2.7}{13} \frac{2.5}{2.5} \frac{3.0}{12} \frac{5.1}{18} \frac{5.2}{19} \frac{2.4}{24} \frac{2.7}{2.8}$

vbst 63+00

2112 2101 2089 2086 2104
 $\frac{3.5}{28} \frac{4.2}{24} \frac{5.8}{20} \frac{6.1}{17} \frac{4.3}{13} \frac{2.08}{39} \frac{2.04}{12} \frac{2.08}{17} \frac{2.08}{19} \frac{2.06}{24} \frac{2.07}{2.96}$

2105 203 2082 2089 2101 2106 2100 2109 2078 2101 2107
 $\frac{4.2}{28} \frac{4.2}{26} \frac{4.4}{25} \frac{6.5}{19} \frac{6.5}{17} \frac{4.6}{12} \frac{2.06}{42} \frac{2.07}{12} \frac{2.08}{17} \frac{2.08}{18} \frac{2.06}{23} \frac{2.07}{2.96}$

2108 2102 2080 2083 2099 2104 2097 2071 2071 2092 2099 2100
 $\frac{3.9}{28} \frac{4.5}{25} \frac{6.7}{20} \frac{6.5}{17} \frac{4.5}{13} \frac{2.04}{43} \frac{2.09}{12} \frac{2.07}{17} \frac{2.07}{18} \frac{2.08}{22} \frac{2.09}{26} \frac{2.00}{2.7}$

2106 2099 2071 2078 2071 2101 2094 2074 2073 2099 2099 2091
 $\frac{4.1}{28} \frac{4.5}{25} \frac{7.0}{20} \frac{6.9}{18} \frac{5.5}{13} \frac{2.01}{46} \frac{2.09}{12} \frac{2.07}{17} \frac{2.07}{18} \frac{2.08}{22} \frac{2.09}{26} \frac{2.00}{2.7}$

2101 2101 2089 2074 2076 2091 2102 2093 2074 2073 2099 2099
 $\frac{4.6}{28} \frac{4.6}{25} \frac{5.5}{23} \frac{7.3}{19} \frac{7.2}{17} \frac{5.5}{12} \frac{2.02}{47} \frac{2.02}{12} \frac{2.07}{17} \frac{2.07}{18} \frac{2.08}{22} \frac{2.09}{26} \frac{2.00}{2.7}$

2098 2082 2070 2069 2090 2096 2071 2070 2069 2088 2098 2101
 $\frac{4.9}{27} \frac{6.4}{24} \frac{7.2}{20} \frac{7.2}{18} \frac{5.7}{13} \frac{2.07}{51} \frac{2.07}{12} \frac{2.07}{17} \frac{2.07}{18} \frac{2.08}{22} \frac{2.09}{26} \frac{2.00}{2.7}$

2084 2071 2064 2066 2084 2091 2093 2086 2066 2094 2096
 $\frac{5.0}{27} \frac{6.0}{24} \frac{7.1}{20} \frac{7.3}{18} \frac{5.2}{13} \frac{2.08}{51} \frac{2.08}{12} \frac{2.08}{17} \frac{2.08}{18} \frac{2.09}{22} \frac{2.09}{26} \frac{2.00}{2.7}$

2084 2082 2084 2081 2089 2083 2086 2086 2086 2086 2086
 $\frac{6.3}{32} \frac{6.5}{27} \frac{8.8}{20} \frac{6.6}{18} \frac{6.5}{13} \frac{2.08}{41} \frac{2.08}{11} \frac{2.08}{17} \frac{2.08}{18} \frac{2.09}{22} \frac{2.09}{26} \frac{2.00}{2.7}$

2078 2076 2066 2066 2081 2084 2086 2060 2060 2083 2089
 $\frac{6.1}{29} \frac{7.2}{25} \frac{7.1}{20} \frac{9.7}{18} \frac{7.0}{13} \frac{2.08}{63} \frac{2.08}{12} \frac{2.08}{17} \frac{2.08}{18} \frac{2.09}{23} \frac{2.09}{26} \frac{2.00}{2.7}$

2071 2070 2051 2053 2073 2071 2070 2060 2060 2083 2089
 $\frac{7.1}{31} \frac{7.7}{26} \frac{9.6}{20} \frac{9.4}{18} \frac{7.4}{12} \frac{2.07}{68} \frac{2.07}{11} \frac{2.07}{16} \frac{2.07}{18} \frac{2.08}{25} \frac{2.08}{27} \frac{2.00}{2.7}$

T.P. 5.54 207.96 3.87 20242

72 $\frac{3.6}{29} \frac{2.1}{16.0} \frac{3.2}{17.4} \frac{3.0}{2.9}$ 29-29 199.00 202.50

71 $\frac{2.7}{29} \frac{3.3}{17.6} \frac{3.7}{18.1} \frac{1.9}{2.9}$ 29-29 199.00 202.50

70 $\frac{2.1}{29} \frac{3.8}{18.3} \frac{2.2}{16} \frac{0.7}{2.9}$ 29-29 199.00 202.50

BM 3.20 (206.29) 203.09

69 $\frac{2.2}{29} \frac{3.3}{17.5} \frac{1.1}{14.6} \frac{1.7}{2.9}$ 29-29 199.00 202.62

+50

68 $\frac{2.6}{28} \frac{0.9}{14.4} \frac{2.7}{16.4} \frac{3.4}{2.8}$ 29-28 200.30 203.56

T.P. 2.03 (206.35) 9.01 204.32

+50

67 $\frac{3.3}{27} \frac{0.9}{14.2} \frac{1.0}{14.4} \frac{2.7}{2.7}$ 27-27 202.80 206.33

66 $\frac{2.5}{27} \frac{0.9}{14.4} \frac{1.4}{15.0} \frac{3.2}{2.6}$ 27-26 205.00 208.22

65 $\frac{3.0}{37} \frac{1.3}{14.8} \frac{1.4}{15} \frac{3.5}{2.5}$ 27-25 206.3 209.11

+50

64 $\frac{3.4}{27} \frac{0.9}{14.2} \frac{1.1}{14.5} \frac{2.4}{2.5}$ 27-25 207.39 210.46

(213.33)

Bar 203.09 - Elev

044

2026 2022 1999 1999 2016 2021 2014 2020 2009 1996 2018 20207
 $\frac{3.7}{29} \frac{4.1}{33} \frac{6.4}{19} \frac{6.4}{17} \frac{4.8}{13} \frac{4.2}{10} \frac{3.9}{12} \frac{4.3}{12} \frac{5.4}{14} \frac{6.8}{17} \frac{4.5}{23} \frac{4.22}{33}$
 2017 2016 1996 1996 2007 2012 2016 2016 2004 1990 1994 2009 20096
 $\frac{4.1}{27} \frac{4.8}{24} \frac{6.7}{20} \frac{6.8}{17} \frac{5.6}{13} \frac{5.1}{11} \frac{4.8}{10} \frac{3.3}{10} \frac{5.7}{14} \frac{7.3}{17} \frac{5.9}{19} \frac{5.4}{24} \frac{5.33}{33}$
 2011 2010 1993 1989 2006 2008 2011 2009 2006 1988 2002 199.09
 $\frac{6.2}{29} \frac{3.3}{25} \frac{7.0}{20} \frac{7.4}{17} \frac{5.7}{13} \frac{5.3}{10} \frac{5.2}{9} \frac{5.4}{9} \frac{5.8}{14} \frac{7.8}{19} \frac{6.1}{24} \frac{7.0}{33}$
 2012 1997 1998 2012 2018 2020 2016 2014 1993 2004 208.59
 $\frac{5.5}{29} \frac{6.7}{20} \frac{5.6}{17} \frac{5.2}{13} \frac{4.6}{10} \frac{4.4}{11} \frac{4.8}{11} \frac{3.0}{14} \frac{7.1}{19} \frac{6.0}{24} \frac{5.16}{33}$
 2014 2016 2003 2002 2018 2020 2023 2020 2016 2000 1999 2021 2021
 $\frac{3.0}{30} \frac{1.9}{25} \frac{6.1}{21} \frac{6.2}{18} \frac{4.6}{14} \frac{4.4}{9} \frac{4.1}{10} \frac{4.4}{10} \frac{4.8}{14} \frac{6.4}{18} \frac{5.5}{19} \frac{4.3}{24} \frac{4.3}{29}$
 2029 2029 2010 2010 2026 2028 2032 2028 2022 2007 2007 2032 20247
 $\frac{3.5}{29} \frac{3.5}{33} \frac{5.4}{20} \frac{5.4}{19} \frac{3.8}{14} \frac{3.5}{10} \frac{3.2}{10} \frac{3.6}{10} \frac{4.2}{13} \frac{5.7}{17} \frac{5.7}{19} \frac{3.2}{24} \frac{2.89}{33}$
 2042 2037 2020 2014 2034 2039 2042 2036 2032 2016 2016 2034 2049
 $\frac{9.1}{29} \frac{7.6}{24} \frac{11.3}{19} \frac{11.4}{18} \frac{7.9}{14} \frac{7.4}{10} \frac{7.1}{10} \frac{9.6}{10} \frac{10.1}{14} \frac{11.7}{18} \frac{11.7}{19} \frac{9.9}{23} \frac{2.1}{28}$
 2066 2046 2029 2030 2046 2046 2042 2049 2041 2043 2030 2047 20659
 $\frac{7.8}{29} \frac{5.9}{23} \frac{10.4}{19} \frac{10.3}{17} \frac{5.8}{14} \frac{8.3}{10} \frac{8.4}{10} \frac{5.6}{10} \frac{8.6}{12} \frac{9.0}{14} \frac{10.3}{18} \frac{8.4}{21} \frac{6.74}{33}$
 2077 2076 2072 2066 2064 2070 2077 2070 2051 2062 2073 20864
 $\frac{5.6}{29} \frac{3.5}{27} \frac{6.1}{24} \frac{7.8}{19} \frac{7.9}{17} \frac{6.9}{13} \frac{5.6}{12} \frac{6.3}{12} \frac{8.2}{17} \frac{9.1}{18} \frac{4.0}{22} \frac{4.27}{33}$
 2093 2091 2068 2068 2087 2093 2090 2089 2068 2048 2107
 $\frac{6.0}{29} \frac{4.2}{26} \frac{1.0}{19} \frac{6.5}{18} \frac{4.1}{14} \frac{4.1}{10} \frac{4.0}{12} \frac{4.3}{12} \frac{2.4}{17} \frac{6.0}{18} \frac{3.5}{24} \frac{3.02}{33}$
 2101 2096 2077 2073 2095 2100 2096 2076 2076 2101 2104
 $\frac{3.2}{30} \frac{3.7}{25} \frac{5.6}{20} \frac{5.5}{19} \frac{3.8}{13} \frac{3.3}{12} \frac{3.7}{12} \frac{5.8}{18} \frac{5.8}{19} \frac{3.2}{24} \frac{2.9}{27}$
 2107 2106 2084 2082 2101 2103 2100 2079 2079 2107 21095
 $\frac{2.6}{28} \frac{2.8}{25} \frac{4.7}{21} \frac{1.1}{18} \frac{3.2}{13} \frac{21.03}{30} \frac{3.3}{11} \frac{5.4}{18} \frac{5.4}{19} \frac{2.6}{24} \frac{2.36}{33}$

150

78 $\frac{3.0}{26}$ $\frac{0.4}{13.6}$ $\frac{1.0}{14.5}$ $\frac{1.9}{26}$ 26-26 205.80 207.77

150

77 $\frac{3.0}{27}$ $\frac{0.3}{13.4}$ $\frac{1.1}{14.5}$ $\frac{1.9}{27}$ 27-27 203.30 205.58
T.P. 13.04 216.66 434 202.62

150

76 $\frac{0.1}{27}$ $\frac{0.3}{13.5}$ $\frac{1.1}{14.6}$ $\frac{2.1}{27}$ 27-27 201.30 204.18

150

75 $\frac{2.5}{28}$ $\frac{0.3}{13.5}$ $\frac{1.0}{14.7}$ $\frac{1.1}{28}$ 28-28 200.50 203.08

150

74 $\frac{2.9}{28}$ $\frac{1.4}{15}$ $\frac{0.9}{14}$ $\frac{2.0}{28}$ 28-28 199.55 202.57

150

73 $\frac{3.5}{29}$ $\frac{2.1}{15.9}$ $\frac{0.9}{14.3}$ $\frac{2.9}{29}$ 28-28 199.30 202.50

207.9.6

209.2 208.4 206.3 208.3 208.5 208.7 208.9 207.9 206.0 208.6 208.8 ✓
 $\frac{7.5}{27}$ $\frac{5.3}{23}$ $\frac{7.4}{18}$ $\frac{5.2}{13}$ $\frac{5.2}{9}$ $\frac{5.2}{20}$ $\frac{5.2}{10}$ $\frac{5.2}{14}$ $\frac{10.7}{19}$ $\frac{5.1}{24}$ $\frac{7.9}{27}$
 208.3 205.1 205.6 207.2 207.4 207.6 207.3 206.9 204.9 207.2 207.46 ✓
 $\frac{1.8}{9}$ $\frac{11.3}{26}$ $\frac{11.1}{19}$ $\frac{9.3}{17}$ $\frac{7.3}{10}$ $\frac{7.1}{71}$ $\frac{9.2}{10}$ $\frac{9.7}{14}$ $\frac{11.8}{19}$ $\frac{9.5}{24}$ $\frac{7.20}{33}$
 207.3 204.4 204.5 206.1 206.5 206.7 206.2 205.8 204.1 206.2 206.2 ✓
 $\frac{2.4}{28}$ $\frac{9.4}{24}$ $\frac{12.3}{19}$ $\frac{12.2}{17}$ $\frac{10.6}{13}$ $\frac{10.2}{9}$ $\frac{10.7}{100}$ $\frac{10.5}{9}$ $\frac{10.9}{15}$ $\frac{12.6}{19}$ $\frac{10.3}{24}$ $\frac{10.5}{27}$
 203.6 203.5 204.3 205.6 205.9 205.5 204.8 203.3 205.2 205.27 ✓
 $\frac{10.6}{27}$ $\frac{13.1}{24}$ $\frac{13.2}{19}$ $\frac{11.4}{17}$ $\frac{11.1}{13}$ $\frac{10.9}{9}$ $\frac{11.2}{108}$ $\frac{11.9}{10}$ $\frac{11.9}{15}$ $\frac{11.3}{19}$ $\frac{11.5}{24}$ $\frac{11.39}{33}$
 205.4 201.9 203.8 204.4 204.8 204.9 204.6 203.9 202.2 204.1 205.3 ✓
 $\frac{2.7}{29}$ $\frac{2.6}{24}$ $\frac{5.1}{19}$ $\frac{5.0}{17}$ $\frac{3.6}{13}$ $\frac{3.2}{9}$ $\frac{3.1}{31}$ $\frac{3.4}{11}$ $\frac{4.1}{15}$ $\frac{5.8}{19}$ $\frac{3.9}{24}$ $\frac{3.7}{27}$
 204.3 202.3 202.2 203.5 204.1 204.3 203.8 203.1 201.5 205.2 205.27 ✓
 $\frac{3.5}{27}$ $\frac{3.7}{25}$ $\frac{5.7}{20}$ $\frac{3.8}{17}$ $\frac{4.5}{13}$ $\frac{3.2}{9}$ $\frac{3.7}{37}$ $\frac{4.2}{10}$ $\frac{4.9}{15}$ $\frac{6.9}{18}$ $\frac{6.5}{19}$ $\frac{4.9}{24}$ $\frac{4.9}{33}$
 201.8 201.7 205.3 203.7 203.2 202.4 201.0 201.0 201.0 201.0 201.0 ✓
 $\frac{1.4}{28}$ $\frac{2.5}{23}$ $\frac{6.2}{18}$ $\frac{6.3}{15}$ $\frac{5.2}{13}$ $\frac{4.7}{9}$ $\frac{4.3}{43}$ $\frac{4.8}{10}$ $\frac{5.6}{15}$ $\frac{7.0}{18}$ $\frac{7.0}{20}$ $\frac{3.5}{23}$ $\frac{5.5}{27}$
 201.2 201.2 201.2 202.4 202.8 202.2 202.8 201.9 200.5 200.7 201.5 201.8 ✓
 $\frac{0.8}{28}$ $\frac{5.3}{22}$ $\frac{6.8}{18}$ $\frac{6.8}{17}$ $\frac{5.6}{13}$ $\frac{5.2}{9}$ $\frac{5.2}{48}$ $\frac{5.2}{10}$ $\frac{6.1}{14}$ $\frac{7.3}{18}$ $\frac{7.3}{20}$ $\frac{6.5}{24}$ $\frac{6.5}{33}$
 202.7 202.5 202.9 202.2 202.6 202.7 202.4 201.7 201.2 201.4 201.1 ✓
 $\frac{5.3}{28}$ $\frac{5.7}{23}$ $\frac{7.1}{19}$ $\frac{5.8}{13}$ $\frac{5.5}{9}$ $\frac{5.2}{52}$ $\frac{5.4}{10}$ $\frac{6.2}{14}$ $\frac{7.8}{19}$ $\frac{6.6}{23}$ $\frac{6.9}{28}$
 201.7 201.7 201.4 201.8 201.5 202.6 202.4 201.2 200.6 201.6 201.6 ✓
 $\frac{5.3}{30}$ $\frac{5.5}{24}$ $\frac{7.3}{18}$ $\frac{7.6}{15}$ $\frac{6.2}{13}$ $\frac{5.3}{9}$ $\frac{5.7}{57}$ $\frac{5.6}{10}$ $\frac{6.3}{15}$ $\frac{5.0}{19}$ $\frac{5.4}{23}$ $\frac{6.32}{33}$
 203.0 202.0 202.0 201.6 202.4 202.7 202.3 201.6 200.1 201.4 202.2 ✓
 $\frac{5.0}{34}$ $\frac{6.0}{23}$ $\frac{8.0}{17}$ $\frac{6.4}{13}$ $\frac{5.6}{9}$ $\frac{5.3}{53}$ $\frac{5.7}{10}$ $\frac{6.4}{14}$ $\frac{7.9}{18}$ $\frac{6.1}{23}$ $\frac{5.8}{29}$
 202.9 202.5 201.3 201.7 202.3 202.7 202.5 201.4 200.7 202.2 202.34 ✓
 $\frac{5.2}{29}$ $\frac{5.5}{23}$ $\frac{7.7}{17}$ $\frac{6.3}{13}$ $\frac{5.2}{10}$ $\frac{5.3}{53}$ $\frac{5.5}{10}$ $\frac{6.6}{15}$ $\frac{8.5}{18}$ $\frac{5.8}{23}$ $\frac{5.62}{33}$

88 $\frac{3.3}{17.5}$ $\frac{3.8}{18.2}$ no cut 217.83

87 $\frac{3.4}{17.7}$ $\frac{4.4}{19.0}$ no cut 217.17

84 $\frac{0.9}{14.2}$ $\frac{0.7}{14}$ no cut 216.83

85 $\frac{2.2}{16.0}$ $\frac{2.3}{16.2}$ no cut 216.08

T.P. 6.98 221.96 5.96 214.98

84 $\frac{2.7}{24}$ $\frac{1.4}{15.0}$ $\frac{1.4}{15.0}$ — 24 - 20.5 213.00 215.67

83 $\frac{3.2}{25.3}$ $\frac{0.2}{13.3}$ $\frac{0.9}{14.2}$ $\frac{1.2}{23.0}$ cut 24 - full Rt 20.5 - 20.5 212.75 215.25

82 $\frac{4.9}{26.19}$ $\frac{3.9}{26.4}$ 20.5 to 212.33 214.83

456 $\frac{4.3}{26.5}$ — $\frac{3.4}{25.6}$ who bottom 20.5 - 20.5 212.12 214.62

81 $\frac{4.3}{26.5}$ — $\frac{3.4}{25.6}$ who bottom 20.5 - 20.5 211.90 214.41

+50
T.P. 7.94 220.94 3.66 213.00

80 $\frac{3.2}{26}$ $\frac{0.6}{14}$ $\frac{1.0}{14.4}$ $\frac{2.4}{26}$ 26 - 26 210.30 212.90

79 $\frac{2.9}{26}$ $\frac{0.6}{13.9}$ $\frac{1.2}{14.4}$ $\frac{2.7}{26}$ 26 - 26 207.50 210.30

216.66

217.2 215.7 216.0 217.5 217.6 217.0 216.8 214.7 215.9 216.6
38 48 63 54 48 44 50 52 7.3 61 5.4
23 21 16 14 9 11 14 20 25 28

17.9 217.4 215.1 216.2 216.8 217.0 216.2 216.3 214.2 215.7
41 46 69 58 52 5.0 5.7 7.2 6.3 6.3
26 22 17 14 9 14 19 24 28

217.3 217.2 214.8 214.7 216.3 216.6 216.2 215.5 213.8 213.2 215.3 215.2
47 48 23 14 6.3 5.7 5.2 5.8 6.3 8.2 6.7 6.8
28 23 11 14 9 5.2 9 14 18 22 27

216.2 215.5 217.5 214.7 215.6 215.7 215.2 214.6 213.7 214.9 214.4
58 6.3 8.3 7.3 6.4 6.1 6.8 7.4 7.3 7.1 7.6
26 22 17 13 9 6.1 10 14 19 23 28

215.7 214.7 213.3 214.6 215.2 215.4 214.9 214.1 213.8 213.8 213.7
52 6.7 7.6 6.3 5.7 5.4 6.0 6.8 8.3 7.1 7.2
24 21 17 13 10 5.5 9 14 19 24 28

216.0 215.4 213.4 215.1 215.5 215.6 215.3 214.5 213.8 214.5 214.5
49 5.3 7.3 5.8 5.4 5.8 5.7 6.2 8.3 6.4 6.2
29 23 17 13 9 5.8 9 14 19 24 28

217.1 215.6 214.4 215.0 216.9 216.5 216.1 215.4 213.7 214.8 215.8 215.9
38 5.3 6.5 5.3 4.6 4.4 4.8 5.3 7.2 6.3 5.1 5.0
24 22 18 14 9 4.4 10 14 19 23 25 28

216.1 215.8 214.4 215.6 216.2 216.4 216.2 215.6 213.7 215.9 216.3
48 5.1 6.5 5.3 4.7 4.5 4.7 5.3 7.2 6.3 5.1 5.0
24 22 18 14 9 4.5 9 15 20 25 28

16.1 215.9 213.1 214.8 215.1 215.2 215.1 214.5 213.9 215.2 215.4
48 5.0 4.8 6.1 5.8 5.7 5.7 6.0 8.3 6.3 5.3 5.1
28 21 19 14 9 5.7 9 15 19 23 28

4.2 214.5 213.2 214.2 213.5 213.8 213.4 213.8 212.2 211.6 213.9 214.3
6.3 6.4 7.7 9.2 7.8 7.1 7.1 7.1 7.7 7.3 7.0 6.6
28 24 22 18 13 9 7.0 9 14 18 23 28

214.5 213.2 214.2 213.5 213.8 213.4 213.8 212.2 211.6 213.9 214.3
3.4 5.2 4.9 6.4 4.7 4.2 4.2 4.2 4.8 5.3 3.8 3.8
26 25 21 18 13 9 4.1 9 14 18 24 28

210.4 210.8 207.7 207.6 207.8 207.5 207.7 207.2 207.4 210.1 210.1
26 24 18 13 9 6.9 10 14 18 24 33

T.P. 10.41 27/84 4.12 194.43

42 32 0.9 0.2 3.3
27 14.2 135 26 27-26 194.00

41 3.2 2.2 1.1 6.8
26 16.0 145 26 26 26 190.80

+50

40 1.7 2.5 1.2 1.9
26 16.5 16.3 26 26-26 188.00

B.M. 7.92 198.55 190.63

Gen. N. wall Culv 39+30

57 2.5 0.8 0.6 3.8
27 13.8 13.9 25 27-25 204.00

56 2.5 0.8 0.1 3.4
27 14.2 14 25 27-25 202.50

55 2.5 6.8 0.5 2.8
27 14.3 13.8 25 27-25 201.0

54 0.8 6.4 1.8
14.1 13.6 25 25-25 199.50

+50

53+09.8

B.M. 5.28 209.01 203.13

Ad. S. side Trans pole R. 54. 53+76

047

27 22 20 18 14 12 22 2.0 2.0 2.0 1.1 1.1 1.0
12 12 12 18 23 25 28
58.94.0 191.7 190.9 191.3 191.6 191.8 192.5 192.1 190.9 193.1 193.6
84.6 59 77 63 60 58 61 65 77 5.5 5.0 5.0
7.6 22 18 14 12 58 61 65 77 22 26 28
191.9 192.0 187.4 190.8 191.4 191.5 191.1 190.7 189.3 191.0 191.6 191.3
6.7 6.6 7.2 7.8 7.2 7.5 7.5 8.4 8.3 7.6 7.0 7.3
28 23 18 14 10 71 12 14 18 22 25 29
188.9 189.6 188.1 187.4 190.2 190.5 187.9 189.3 187.9 187.4 187.6 189.7
87 90 103 92 84 87 87 93 107 92 90 89
25 22 18 13 10 81 12 14 19 23 24 26

206.5 205.0 205.9 206.3 206.8 206.6 204.9 207.4 208.3
2.5 4.0 5.1 2.7 2.1 2.4 2.7 1.6 2.7
27 23 20 13 21 13 18 23 25

205.1 205.4 204.6 204.6 204.9
3.9 6.2 4.2 205.5 3.9 5.1 4.0 2.1 2.1
27 23 18 13 35 13 19 21 24 25

201.4 201.2 200.8 200.0 201.8 202.2 202.1 200.4 200.6
7.6 8.0 8.2 7.0 7.2 6.8 6.9 8.6 8.4
27 24 22 18 13 68 12 19 21

200.9 201.2 199.7 201.4 201.4 201.1 200.4 201.4
8.1 7.8 9.3 7.6 202.0 7.6 8.9 8.6 7.6
31 24 18 11 70 12 18 21 24

202.3 202.8 200.9 201.5 201.5 201.5
8.7 8.2 8.1 7.5 7.5 7.5 7.5
50 24 15 75 18 24

49	$\frac{2.6}{26}$ $\frac{1.0}{14.4}$ $\frac{1.1}{14.5}$ $\frac{3.2}{26}$	26-26	195.5	198.29	$\frac{97.5}{35}$ $\frac{197.7}{29}$ $\frac{195.0}{22}$ $\frac{195.5}{19}$ $\frac{197.4}{14}$ $\frac{197.9}{12}$ $\frac{198.7}{19}$ $\frac{195.1}{11}$ $\frac{196.8}{14}$ $\frac{196.6}{17}$ $\frac{197.0}{22}$ $\frac{198.7}{30}$ ✓ $\frac{68}{8}$ $\frac{197.2}{6.4}$ $\frac{197.2}{6.4}$ $\frac{194.7}{8.9}$ $\frac{196.3}{7.3}$ $\frac{197.0}{6.6}$ $\frac{197.5}{6.6}$ $\frac{197.0}{14}$ $\frac{196.2}{8.1}$ $\frac{195.5}{5.8}$ $\frac{197.8}{6.7}$ $\frac{197.5}{2.9}$ ✓ $\frac{195.2}{32}$ $\frac{195.6}{25}$ $\frac{195.5}{21}$ $\frac{195.7}{13}$ $\frac{196.6}{12}$ $\frac{197.3}{63}$ $\frac{197.2}{10}$ $\frac{196.6}{14}$ $\frac{195.1}{20}$ $\frac{196.3}{25}$ $\frac{196.2}{29}$ ✓ $\frac{194.8}{30}$ $\frac{195.5}{24}$ $\frac{194.1}{21}$ $\frac{196.0}{15}$ $\frac{196.4}{7.2}$ $\frac{197.2}{64}$ $\frac{196.6}{12}$ $\frac{196.8}{10}$ $\frac{195.7}{18}$ $\frac{196.9}{22}$ $\frac{197.1}{27}$ ✓
+50					
48	$\frac{3.0}{17}$ $\frac{1.5}{15.0}$			no cut 198.74	$\frac{195.2}{32}$ $\frac{195.6}{25}$ $\frac{195.5}{21}$ $\frac{195.7}{13}$ $\frac{196.6}{12}$ $\frac{197.3}{63}$ $\frac{197.2}{10}$ $\frac{196.6}{14}$ $\frac{195.1}{20}$ $\frac{196.3}{25}$ $\frac{196.2}{29}$ ✓ $\frac{194.8}{30}$ $\frac{195.5}{24}$ $\frac{194.1}{21}$ $\frac{196.0}{15}$ $\frac{196.4}{7.2}$ $\frac{197.2}{64}$ $\frac{196.6}{12}$ $\frac{196.8}{10}$ $\frac{195.7}{18}$ $\frac{196.9}{22}$ $\frac{197.1}{27}$ ✓
+50					
47	$\frac{1.3}{28}$ $\frac{4.2}{18.5}$ $\frac{3.2}{17.2}$ $\frac{3.3}{26}$	28-26	196.0	198.67	$\frac{196.1}{7.5}$ $\frac{196.7}{24}$ $\frac{194.7}{19}$ $\frac{196.6}{14}$ $\frac{196.9}{12}$ $\frac{197.5}{61}$ $\frac{197.1}{12}$ $\frac{196.6}{10}$ $\frac{195.5}{18}$ $\frac{197.9}{22}$ $\frac{198.40}{33}$ ✓ $\frac{196.1}{7.5}$ $\frac{196.7}{24}$ $\frac{194.7}{19}$ $\frac{196.6}{14}$ $\frac{196.9}{12}$ $\frac{197.5}{61}$ $\frac{197.1}{12}$ $\frac{196.6}{10}$ $\frac{195.5}{18}$ $\frac{197.9}{22}$ $\frac{198.40}{33}$ ✓
T.P.	5.23	203.58	6.49	198.35	
46	$\frac{1.7}{28}$ $\frac{1.2}{14.7}$ $\frac{0.6}{14}$ $\frac{3.0}{26}$	28-26	197.0	199.33	$\frac{198.0}{30}$ $\frac{198.8}{27}$ $\frac{195.2}{23}$ $\frac{198.1}{19}$ $\frac{198.8}{14}$ $\frac{199.2}{12}$ $\frac{198.8}{56}$ $\frac{198.5}{12}$ $\frac{196.9}{14}$ $\frac{198.6}{18}$ $\frac{200.2}{22}$ $\frac{200.3}{33}$ ✓ $\frac{198.0}{30}$ $\frac{198.8}{27}$ $\frac{195.2}{23}$ $\frac{198.1}{19}$ $\frac{198.8}{14}$ $\frac{199.2}{12}$ $\frac{198.8}{56}$ $\frac{198.5}{12}$ $\frac{196.9}{14}$ $\frac{198.6}{18}$ $\frac{200.2}{22}$ $\frac{200.3}{33}$ ✓
45	$\frac{1.8}{27}$ $\frac{1.0}{14.4}$ $\frac{0.6}{18.0}$ $\frac{3.2}{26}$	27-26	197.5	200.00	$\frac{199.3}{30}$ $\frac{199.4}{27}$ $\frac{199.2}{20}$ $\frac{199.1}{19}$ $\frac{199.7}{14}$ $\frac{200.1}{12}$ $\frac{199.6}{47}$ $\frac{199.3}{12}$ $\frac{197.9}{18}$ $\frac{200.8}{23}$ $\frac{200.7}{28}$ $\frac{200.8}{29}$ ✓ $\frac{199.3}{30}$ $\frac{199.4}{27}$ $\frac{199.2}{20}$ $\frac{199.1}{19}$ $\frac{199.7}{14}$ $\frac{200.1}{12}$ $\frac{199.6}{47}$ $\frac{199.3}{12}$ $\frac{197.9}{18}$ $\frac{200.8}{23}$ $\frac{200.7}{28}$ $\frac{200.8}{29}$ ✓
+50					
44	$\frac{1.4}{15.1}$ $\frac{1.0}{14.4}$			freelind no. 44	$\frac{199.1}{30}$ $\frac{199.2}{26}$ $\frac{197.0}{19}$ $\frac{199.2}{14}$ $\frac{199.6}{12}$ $\frac{200.1}{47}$ $\frac{199.8}{12}$ $\frac{199.3}{14}$ $\frac{198.1}{18}$ $\frac{200.6}{23}$ $\frac{200.6}{28}$ $\frac{200.8}{29}$ ✓ $\frac{199.1}{30}$ $\frac{199.2}{26}$ $\frac{197.0}{19}$ $\frac{199.2}{14}$ $\frac{199.6}{12}$ $\frac{200.1}{47}$ $\frac{199.8}{12}$ $\frac{199.3}{14}$ $\frac{198.1}{18}$ $\frac{200.6}{23}$ $\frac{200.6}{28}$ $\frac{200.8}{29}$ ✓
+50					
43	$\frac{2.4}{27}$ $\frac{1.1}{14.5}$ $\frac{0.9}{14.2}$ $\frac{2.8}{26}$	27-26	197.00	199.27	$\frac{198.3}{30}$ $\frac{197.5}{27}$ $\frac{195.6}{25}$ $\frac{197.2}{19}$ $\frac{197.4}{14}$ $\frac{197.9}{12}$ $\frac{198.4}{56}$ $\frac{197.3}{12}$ $\frac{197.9}{14}$ $\frac{199.9}{18}$ $\frac{199.8}{23}$ $\frac{199.7}{28}$ ✓ $\frac{198.3}{30}$ $\frac{197.5}{27}$ $\frac{195.6}{25}$ $\frac{197.2}{19}$ $\frac{197.4}{14}$ $\frac{197.9}{12}$ $\frac{198.4}{56}$ $\frac{197.3}{12}$ $\frac{197.9}{14}$ $\frac{199.9}{18}$ $\frac{199.8}{23}$ $\frac{199.7}{28}$ ✓
42+50					$\frac{198.3}{30}$ $\frac{197.5}{27}$ $\frac{195.6}{25}$ $\frac{197.2}{19}$ $\frac{197.4}{14}$ $\frac{197.9}{12}$ $\frac{198.4}{56}$ $\frac{197.3}{12}$ $\frac{197.9}{14}$ $\frac{199.9}{18}$ $\frac{199.8}{23}$ $\frac{199.7}{28}$ ✓ $\frac{198.3}{30}$ $\frac{197.5}{27}$ $\frac{195.6}{25}$ $\frac{197.2}{19}$ $\frac{197.4}{14}$ $\frac{197.9}{12}$ $\frac{198.4}{56}$ $\frac{197.3}{12}$ $\frac{197.9}{14}$ $\frac{199.9}{18}$ $\frac{199.8}{23}$ $\frac{199.7}{28}$ ✓

(204.38)

T.P. 4.15 (194.87) 7.64 190.72
+50

37 2.5 0.8 0.6 3.1
25 14.2 13.9 26 25-26 190.00 192.41

36 2.1 0.7 0.1 3.2
25 14 13.2 26 25-26 192.00 194.32

T.P. 2.33 (198.36) 7.72 196.03

35 2.3 1.2 0.3 3.2
24 14.7 13.6 25 24-25 193.5 196.22

34 2.1 2.6 0.6 3.0
24 16.6 13.8 24-25 195.5 198.13

33 2.6 2.1 - 3.3
24 16.6 13.8 24-25 195.5 198.13

T.P. 4.15 (203.75) 0.52 199.60

B.M. 8.62 200.12 191.50

+50

52 2.3 1.6 1.2 2.2
26 15.2 14.7 26 26-28 197.0 199.78

+50

51 1.2 1.7 1.3 2.6
26 15.2 16.3 26 26-26 196.0 198.93

T.P. 6.57 (204.66) 5.49 198.09

50 1.8 1.7 1.5 2.9
26 15.4 16.1 26 26-26 195.5 198.57

(203.58)

190.8	191.1	191.1	190.3	190.8	191.5	190.9	190.8	191.4	191.9	192.1	
25	22	17	14	24	69	15	76	70	67	63	
27	22	17	14	24	69	15	76	70	67	63	
192.2	192.4	191.0	191.6	192.0	192.5	192.2	191.6	190.5	192.8	193.3	193.2
28	22	18	14	13	57	62	68	79	56	51	52
28	22	18	14	13	57	62	68	79	56	51	52
194.5	193.9	192.4	193.6	194.4	194.6	194.4	194.3	192.5	195.0	195.3	
3.9	4.5	6.0	4.8	4.0	3.8	4.0	4.1	5.9	3.4	3.1	
28	23	18	14	12	38	12	14	19	24	28	
5.8	195.9	195.3	194.0	195.0	195.4	196.5	196.2	196.0	194.2	196.4	196.7
8.0	1.9	8.5	7.8	8.8	8.4	7.3	7.6	7.8	9.6	7.8	7.1
28	25	22	18	14	12	73	76	78	96	78	28
1.6	197.7	196.8	195.5	196.7	197.3	198.0	197.9	197.5	195.9	198.1	198.3
2	6.1	2.0	8.3	7.1	6.5	5.8	5.9	6.3	7.9	5.7	5.3
28	23	21	14	12	58	12	14	18	23	25	28
0.4	199.7	199.9	199.2	199.8	200.2	200.5	200.3	199.5	198.1	200.5	201.1
3.4	3.4	5.9	4.6	4.0	3.7	3.3	3.5	4.3	5.7	5.3	2.7
26	22	17	15	12	8	33	12	14	18	22	26
200.0	200.4	199.9	199.2	199.8	200.2	200.5	200.3	199.5	198.1	200.5	201.1
4.7	4.5	6.7	5.6	5.1	4.4	4.9	5.0	5.9	6.2	4.4	4.4
31	25	18	14	12	44	71	14	17	22	32	
199.0	199.1	196.6	198.4	198.7	199.3	199.6	198.3	197.7	199.2	199.3	
5.7	5.6	8.1	6.3	6.0	5.4	6.1	6.4	7.0	5.5	5.5	
32	24	19	14	12	54	72	74	17	22	30	
197.6	197.7	196.0	197.9	198.7	198.9	197.6	197.0	198.2	196.5	198.5	
7.1	7.0	8.7	6.8	6.8	6.8	7.1	7.5	6.5	6.2	6.2	
32	24	18	12	60	12	14	18	21	26	26	
196.6	197.2	196.4	195.9	197.5	198.7	197.3	197.1	196.6	198.2	198.5	
8.1	7.5	8.3	8.8	7.3	6.0	7.4	7.6	8.1	6.3	6.2	
33	25	23	19	14	60	72	74	16	21	29	
198.1	197.8	195.4	196.9	197.8	198.6	197.9	197.3	196.6	198.6	198.5	
6.5	5.8	8.2	6.7	5.8	5.0	5.1	6.3	6.8	5.0	4.6	
32	24	19	15	12	50	12	15	17	21	30	

30	$\frac{2.0}{29}$	$\frac{2.7}{16.6}$	$\frac{2.2}{16.0}$	$\frac{3.1}{29}$	29 - 29	191.80	194.96
T.P.	12.05	<u>203.46</u>		4.27		191.41	
29	$\frac{1.9}{29}$	$\frac{4.2}{18.7}$	$\frac{3.3}{17.7}$	$\frac{3.1}{29}$	29 - 29	189.00	193.33
28	$\frac{0.8}{29}$	$\frac{4.6}{19.3}$	$\frac{3.8}{18.3}$	$\frac{2.5}{29}$	noted 29	188.80	192.36
27	$\frac{0.0}{29.0}$		$\frac{2.1}{29}$	not - 29	188.20 ¹⁰⁺		192.02
26	$\frac{1.1}{29}$	$\frac{4.0}{18.5}$	$\frac{3.0}{16.8}$	$\frac{3.7}{29}$	29 - 29	189.00	192.32
25		$\frac{2.7}{16.7}$	$\frac{2.6}{16.6}$	$\frac{3.7}{29}$	not - 28	191.00 ^{R+}	193.17
BM	4.18	<u>195.68</u>				191.50	
BM				4.21		190.66	

Vol. Reim. 1 sec

450

39 $-\frac{12}{14.8}$ $\frac{1.5}{15.1}$ $\frac{19}{29}$ hect-27 187.50 190.50

752

28 $\frac{2.0}{24}$ $\frac{2.4}{163}$ $\frac{1.6}{148}$ $\frac{3.1}{26}$ 24-26 188.00 190.98

194.87

$\frac{187.2}{7.7}$ 30	$\frac{187.9}{7.0}$ 23	$\frac{187.3}{7.6}$ 21	$\frac{188.7}{6.2}$ 14	$\frac{189.3}{5.6}$ 12	$\frac{190.0}{4.9}$ 1	$\frac{189.1}{5.8}$ 12	$\frac{188.6}{6.3}$ 14	$\frac{187.1}{7.1}$ 19	$\frac{189.2}{5.7}$ 20	$\frac{189.0}{5.1}$ 28
$\frac{187.0}{7.9}$ 28	$\frac{187.7}{7.1}$ 22	$\frac{187.1}{7.8}$ 19	$\frac{188.9}{6.0}$ 14	$\frac{189.1}{5.8}$ 12	$\frac{189.7}{5.2}$ 1	$\frac{189.6}{5.3}$ 12	$\frac{189.0}{5.9}$ 14	$\frac{187.3}{7.0}$ 19	$\frac{189.0}{5.9}$ 24	$\frac{189.0}{5.5}$ 27
$\frac{188.0}{6.9}$ 28	$\frac{188.3}{6.6}$ 23	$\frac{187.6}{7.3}$ 19	$\frac{188.9}{6.1}$ 14	$\frac{189.3}{5.6}$ 12	$\frac{189.9}{5.0}$ 1	$\frac{189.0}{5.3}$ 12	$\frac{189.0}{5.0}$ 14	$\frac{188.0}{6.9}$ 19	$\frac{188.0}{5.3}$ 22	$\frac{189.0}{5.1}$ 27
$\frac{189.8}{5.1}$ 27	$\frac{189.4}{5.0}$ 23	$\frac{188.2}{6.7}$ 18	$\frac{189.4}{5.5}$ 14	$\frac{189.7}{5.2}$ 12	$\frac{190.6}{4.3}$ 1	$\frac{190.0}{4.5}$ 12	$\frac{189.8}{5.1}$ 14	$\frac{188.6}{6.3}$ 18	$\frac{190.6}{4.3}$ 23	$\frac{191.0}{3.6}$ 28

+ 52

19	$\frac{0.0}{16.6}$	$\frac{48}{2720.0}$	20 total	188.80	190.80
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752

18	—	$\frac{0.7}{140}$	$\frac{0.9}{142}$	$\frac{40.2}{27}$	2000 27	25	186.5	188.66
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T.P	10.14	195.80	2.05	185.66	
17	$\frac{3.0}{7.5}$	$\frac{3.0}{17.0}$	$\frac{3.0}{25.0}$	25	183.80
					186.33

16	$\frac{1.6}{18.2}$	$\frac{1.6}{15}$	—	no cut	182/00
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150

15	$\frac{1.9}{15.7}$	$\frac{1.2}{14.6}$	—	no cut	181.79
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BM 5.46 (187.71) 182.25

Nail N Sid Trans pole sta 12+60

32 + 40

32 $\frac{2.3}{25}$ — — $\frac{2.9}{26}$ rotodetol 197.50 $\frac{m}{199.43}$

31	$\frac{3.7}{27.5}$	$-\frac{4.2}{28.3}$	22 to day 194. 20	tail(?) 197.17
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Use Rebin
x sec

1	$\frac{0.6}{22.6}$	$\frac{0.9}{14.3}$	$\frac{1.2}{14.8}$	$\frac{1.7}{22}$	slip 22	159.3	161.75	$\frac{160.5}{29}$	$\frac{161.7}{24}$	$\frac{160.9}{22}$	$\frac{160.6}{18}$	$\frac{160.7}{14}$	$\frac{160.9}{12}$	$\frac{161.1}{10.5}$	$\frac{161.5}{12}$	$\frac{162.1}{14}$	$\frac{161.9}{17}$	$\frac{160.0}{19}$	$\frac{160.9}{22}$	$\frac{161.1}{25}$	$\frac{162.1}{32}$
+50	$\frac{0.5}{21.4}$	$\frac{0.7}{14.0}$	$\frac{1.5}{15.1}$	$\frac{1.9}{24}$	slip 24	158.6	160.88	$\frac{159.7}{27}$	$\frac{158.6}{22}$	$\frac{159.4}{17}$	$\frac{161.1}{18}$	$\frac{160.4}{12}$	$\frac{160.4}{11}$	$\frac{159.4}{10}$	$\frac{159.3}{15}$	$\frac{159.3}{19}$	$\frac{160.4}{22}$	$\frac{160.6}{33}$			

Q.

160.00

Use Prelim X Sec

BM.O 9.53 (171.63) 16210

+50

$\frac{1}{31}$	$\frac{191.2}{83}$	$\frac{191.4}{81}$	$\frac{190.3}{92}$	$\frac{190.3}{72}$	$\frac{192.5}{70}$	$\frac{193.2}{63}$	$\frac{192.9}{66}$	$\frac{192.5}{72}$	$\frac{191.7}{28}$	$\frac{191.7}{48}$	$\frac{195.1}{44}$	$\frac{195.4}{41}$
----------------	--------------------	--------------------	--------------------	--------------------	--------------------	--------------------	--------------------	--------------------	--------------------	--------------------	--------------------	--------------------

24

- $\frac{1.8}{15.5}$ - $\frac{1.4}{26.6}$

not to include

192.00

194.00

$\frac{1}{8}$	$\frac{192.1}{74}$	$\frac{192.2}{86}$	$\frac{190.4}{86}$	$\frac{192.6}{69}$	$\frac{193.2}{63}$	$\frac{194.0}{58}$	$\frac{193.7}{72}$	$\frac{192.5}{14}$	$\frac{191.3}{17}$	$\frac{190.3}{22}$	$\frac{190.4}{27}$	$\frac{190.9}{33}$
---------------	--------------------	--------------------	--------------------	--------------------	--------------------	--------------------	--------------------	--------------------	--------------------	--------------------	--------------------	--------------------

+50

$\frac{1}{48}$	$\frac{192.3}{69}$	$\frac{192.6}{82}$	$\frac{191.3}{82}$	$\frac{192.0}{74}$	$\frac{193.6}{59}$	$\frac{194.6}{49}$	$\frac{194.3}{52}$	$\frac{193.6}{14}$	$\frac{193.8}{18}$	$\frac{196.1}{22}$	$\frac{196.6}{26}$	$\frac{197.2}{29}$
----------------	--------------------	--------------------	--------------------	--------------------	--------------------	--------------------	--------------------	--------------------	--------------------	--------------------	--------------------	--------------------

28

 $\frac{0.0}{182}$ $\frac{5.5}{28.2}$ not to include

191.80

193.80

$\frac{1}{29}$	$\frac{192.4}{71}$	$\frac{192.7}{68}$	$\frac{191.4}{81}$	$\frac{192.0}{78}$	$\frac{193.8}{57}$	$\frac{194.5}{50}$	$\frac{194.4}{12}$	$\frac{193.8}{14}$	$\frac{193.7}{18}$	$\frac{196.5}{22}$	$\frac{197.3}{28}$	$\frac{197.7}{33}$
----------------	--------------------	--------------------	--------------------	--------------------	--------------------	--------------------	--------------------	--------------------	--------------------	--------------------	--------------------	--------------------

22

 $\frac{2.5}{16.5}$ $\frac{2.4}{16.3}$ $\frac{3.9}{26}$

not 26

190.50

193.10

$\frac{1}{26}$	$\frac{191.3}{92}$	$\frac{191.1}{104}$	$\frac{189.1}{104}$	$\frac{190.5}{20}$	$\frac{191.5}{8.0}$	$\frac{192.1}{74}$	$\frac{191.3}{12}$	$\frac{190.5}{14}$	$\frac{193.3}{20}$	$\frac{194.0}{21}$	$\frac{194.2}{25}$	$\frac{194.2}{26}$
----------------	--------------------	---------------------	---------------------	--------------------	---------------------	--------------------	--------------------	--------------------	--------------------	--------------------	--------------------	--------------------

21

 $\frac{4.8}{19.6}$ $\frac{3.1}{17.4}$ $\frac{3.7}{26}$

not 26

189.20

192.40

$\frac{1}{29}$	$\frac{189.7}{108}$	$\frac{188.9}{106}$	$\frac{188.1}{114}$	$\frac{188.1}{114}$	$\frac{190.1}{24}$	$\frac{190.9}{86}$	$\frac{191.0}{12}$	$\frac{190.2}{14}$	$\frac{189.4}{17}$	$\frac{192.3}{22}$	$\frac{193.2}{26}$	$\frac{193.7}{29}$
----------------	---------------------	---------------------	---------------------	---------------------	--------------------	--------------------	--------------------	--------------------	--------------------	--------------------	--------------------	--------------------

T.P.

1.76 (199.52)

7.04

188.76

191.70

$\frac{1}{30}$	$\frac{188.8}{64}$	$\frac{189.2}{79}$	$\frac{187.9}{79}$	$\frac{190.0}{5.2}$	$\frac{191.1}{47}$	$\frac{190.5}{58}$	$\frac{190.6}{14}$	$\frac{189.8}{16}$	$\frac{192.6}{23}$	$\frac{193.5}{23}$	$\frac{193.5}{31}$	$\frac{193.5}{31}$
----------------	--------------------	--------------------	--------------------	---------------------	--------------------	--------------------	--------------------	--------------------	--------------------	--------------------	--------------------	--------------------

20

- $\frac{4.1}{18.3}$ $\frac{2.0}{15.7}$ $\frac{3.8}{26}$

not 26

189.70

191.70

(195.80)

10	-	$\frac{1.7}{15.2}$	$\frac{1.9}{15.5}$	$\frac{3.5}{25}$	no cut 25	176.8	178.89	$\frac{176.8}{2.59}$ $\frac{176.6}{6.1}$ $\frac{176.3}{4.2}$ $\frac{175.5}{9.2}$ $\frac{174.7}{5.6}$ $\frac{174.1}{5.0}$ $\frac{173.7}{12}$ $\frac{173.2}{47}$ $\frac{172.8}{9}$ $\frac{172.0}{57}$ $\frac{171.7}{56}$ $\frac{171.0}{27}$ $\frac{170.0}{27}$ $\frac{169.3}{27}$ $\frac{168.4}{32}$
9		$\frac{0.0}{18.5}$	$\frac{0.7}{14}$	$\frac{1.5}{15.0}$	$\frac{3.6}{25}$	100 25	176.50	$\frac{176.5}{5.54}$ $\frac{176.8}{5.9}$ $\frac{175.6}{21}$ $\frac{174.0}{67}$ $\frac{173.6}{5.1}$ $\frac{173.1}{5.1}$ $\frac{172.6}{12}$ $\frac{172.1}{46}$ $\frac{171.6}{10}$ $\frac{171.1}{12}$ $\frac{170.6}{13}$ $\frac{170.1}{16}$ $\frac{169.6}{20}$ $\frac{169.1}{27}$ $\frac{168.6}{30}$
T.P.	5.23	(182.73)	3.16			177.50		$\frac{177.5}{1.1}$ $\frac{177.4}{6}$ $\frac{177.1}{26}$ $\frac{176.4}{33}$ $\frac{178.4}{26}$ $\frac{178.1}{23}$ $\frac{177.6}{26}$ $\frac{177.1}{30}$ $\frac{176.6}{12}$ $\frac{176.1}{30}$ $\frac{175.6}{38}$ $\frac{175.1}{29}$ $\frac{174.6}{17}$ $\frac{174.1}{20}$ $\frac{173.6}{26}$
+50								$\frac{178.2}{2.5}$ $\frac{178.1}{2.8}$ $\frac{178.0}{2.6}$ $\frac{177.8}{2.9}$ $\frac{178.2}{2.5}$ $\frac{177.8}{2.9}$ $\frac{177.4}{12}$ $\frac{177.0}{20}$ $\frac{176.6}{10}$ $\frac{176.2}{14}$ $\frac{175.8}{17}$ $\frac{175.4}{20}$ $\frac{175.0}{23}$ $\frac{174.6}{27}$
8		$\frac{0.5}{20}$	$\frac{0.2}{13.7}$	$\frac{0.7}{14.0}$	$\frac{4.7}{27}$	20 27	176.00	$\frac{176.0}{2.9}$ $\frac{175.9}{2.5}$ $\frac{175.8}{2.1}$ $\frac{175.7}{14}$ $\frac{175.6}{12}$ $\frac{175.5}{20}$ $\frac{175.4}{10}$ $\frac{175.3}{14}$ $\frac{175.2}{17}$ $\frac{175.1}{20}$ $\frac{175.0}{23}$ $\frac{174.9}{27}$
+50								$\frac{175.1}{7}$ $\frac{175.0}{2.6}$ $\frac{174.9}{3.2}$ $\frac{174.8}{4.6}$ $\frac{174.7}{5.1}$ $\frac{174.6}{3.1}$ $\frac{174.5}{2.8}$ $\frac{174.4}{3.1}$ $\frac{174.3}{3.3}$ $\frac{174.2}{2.3}$ $\frac{174.1}{1.0}$ $\frac{174.0}{0.2}$ $\frac{173.9}{2.5}$
7		$\frac{0.0}{19.5}$	$\frac{0.0}{13.2}$	$\frac{0.7}{14.1}$	$\frac{4.0}{26}$	30 26	174.50	$\frac{174.5}{3.1}$ $\frac{174.4}{4.1}$ $\frac{174.3}{4.5}$ $\frac{174.2}{6.0}$ $\frac{174.1}{6.3}$ $\frac{174.0}{4.1}$ $\frac{173.9}{3.5}$ $\frac{173.8}{12}$ $\frac{173.7}{42}$ $\frac{173.6}{49}$ $\frac{173.5}{5.0}$ $\frac{173.4}{3.8}$ $\frac{173.3}{2.6}$ $\frac{173.2}{2.2}$ $\frac{173.1}{2.8}$
+50								$\frac{174.1}{4.6}$ $\frac{174.0}{4.3}$ $\frac{173.9}{4.3}$ $\frac{173.8}{5.3}$ $\frac{173.7}{5.0}$ $\frac{173.6}{4.8}$ $\frac{173.5}{5.6}$ $\frac{173.4}{6.4}$ $\frac{173.3}{6.7}$ $\frac{173.2}{3.9}$ $\frac{173.1}{3.4}$
6		$\frac{0.0}{18.9}$	$\frac{0.0}{13.2}$	$\frac{1.1}{14.5}$	$\frac{2.1}{24}$	30 24	172.00	$\frac{172.0}{5.3}$ $\frac{171.9}{6.0}$ $\frac{171.8}{2.1}$ $\frac{171.7}{2.8}$ $\frac{171.6}{6.9}$ $\frac{171.5}{6.7}$ $\frac{171.4}{12}$ $\frac{171.3}{64}$ $\frac{171.2}{12}$ $\frac{171.1}{18}$ $\frac{171.0}{16}$ $\frac{170.9}{20}$ $\frac{170.8}{22}$ $\frac{170.7}{26}$
5		$\frac{0.0}{18.6}$	$\frac{0.6}{13.9}$	$\frac{1.1}{14.5}$	$\frac{2.6}{24}$	30 24	169.00	$\frac{169.0}{7.1}$ $\frac{168.9}{9.6}$ $\frac{168.8}{11.6}$ $\frac{168.7}{11.6}$ $\frac{168.6}{18}$ $\frac{168.5}{14}$ $\frac{168.4}{12}$ $\frac{168.3}{93}$ $\frac{168.2}{99}$ $\frac{168.1}{10.3}$ $\frac{168.0}{11.3}$ $\frac{167.9}{17}$ $\frac{167.8}{22}$ $\frac{167.7}{24}$
4		$\frac{0.0}{17.5}$	$\frac{0.4}{13.5}$	$\frac{2.0}{15.5}$	$\frac{2.3}{23}$	00 23	166.00	$\frac{166.0}{10.4}$ $\frac{165.9}{11.2}$ $\frac{165.8}{13.8}$ $\frac{165.7}{12.5}$ $\frac{165.6}{13}$ $\frac{165.5}{12.2}$ $\frac{165.4}{11}$ $\frac{165.3}{12}$ $\frac{165.2}{1.1}$ $\frac{165.1}{13.0}$ $\frac{165.0}{13.6}$ $\frac{164.9}{14.2}$ $\frac{164.8}{13}$ $\frac{164.7}{17}$ $\frac{164.6}{21}$ $\frac{164.5}{22}$ $\frac{164.4}{31}$
T.P.	12.15	(180.66)	3.12			166.51		$\frac{166.5}{10.9}$ $\frac{166.4}{10.6}$ $\frac{166.3}{10.1}$ $\frac{166.2}{10.2}$ $\frac{166.1}{10.5}$ $\frac{166.0}{10.8}$ $\frac{165.9}{10.9}$ $\frac{165.8}{10.7}$ $\frac{165.7}{10.6}$ $\frac{165.6}{10.5}$ $\frac{165.5}{10.4}$ $\frac{165.4}{10.3}$ $\frac{165.3}{10.2}$ $\frac{165.2}{10.1}$ $\frac{165.1}{10.0}$
3		$\frac{0.0}{18.1}$	$\frac{0.8}{14.0}$	$\frac{2.0}{15.6}$	$\frac{1.7}{22}$	00 22	163.5	$\frac{163.5}{4.7}$ $\frac{163.4}{5.0}$ $\frac{163.3}{7.5}$ $\frac{163.2}{7.1}$ $\frac{163.1}{6.1}$ $\frac{163.0}{5.8}$ $\frac{162.9}{12}$ $\frac{162.8}{57}$ $\frac{162.7}{12}$ $\frac{162.6}{14}$ $\frac{162.5}{17}$ $\frac{162.4}{21}$ $\frac{162.3}{22}$ $\frac{162.2}{22}$ $\frac{162.1}{33}$
2		$\frac{0.0}{18.9}$	$\frac{0.0}{13.2}$	$\frac{0.9}{14.3}$	$\frac{1.9}{22}$	30 22	161.50	$\frac{161.5}{13.2}$ $\frac{161.4}{16.8}$ $\frac{161.3}{10.2}$ $\frac{161.2}{10.2}$ $\frac{161.1}{8.0}$ $\frac{161.0}{8.2}$ $\frac{160.9}{12}$ $\frac{160.8}{81}$ $\frac{160.7}{12}$ $\frac{160.6}{14}$ $\frac{160.5}{17}$ $\frac{160.4}{20}$ $\frac{160.3}{23}$ $\frac{160.2}{32}$
		(171.63)						

BM

253 182.26 182.25 pipe in pole 11 Sta 12+60

750

14

$\frac{00}{20.6}$ $\frac{09}{142}$ $\frac{06}{139}$ $\frac{41}{25}$ 25 178.50 180 15

+ sv

13

— $\frac{1.2}{14.7}$ $\frac{0.9}{14.2}$ $\frac{3.6}{25}$ no incl 25 178.00 179.97

12

— $\frac{2.4}{16.3}$ $\frac{1.5}{15.1}$ $\frac{3.2}{25}$ need 25 177.30 17961

T. P.

540 (184.79) 3.34 179.39

11

-	$\frac{2.1}{15.8}$	$\frac{1.2}{15.4}$	$\frac{3.3}{25}$	no cool 25	177.00	179.25
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152.73

77.3	79.6	78.6	180.2	180.4	180.3	180.8	180.4	179.8	181.9	182.9	183.2
55	52	63	48	45	40	40	44	50	29	19	16
27	24	18	14	12	40	12	16	18	21	25	30

$$\begin{array}{r} 1912 \\ 56 \\ \hline 21 \end{array}$$

$$\begin{array}{r} 1819 \\ 59 \\ \hline 23 \end{array}$$

$$\begin{array}{r} 1821 \\ 67 \\ \hline 18 \end{array}$$

$$\begin{array}{r} 1916 \\ 52 \\ \hline 13 \end{array}$$

$$\begin{array}{r} 1821 \\ 48 \\ \hline 12 \end{array}$$

$$\begin{array}{r} 1822 \\ 46 \\ \hline 12 \end{array}$$

$$\begin{array}{r} 1824 \\ 44 \\ \hline 12 \end{array}$$

$$\begin{array}{r} 1919 \\ 49 \\ \hline 14 \end{array}$$

$$\begin{array}{r} 1914 \\ 54 \\ \hline 18 \end{array}$$

$$\begin{array}{r} 1823 \\ 25 \\ \hline 23 \end{array}$$

$$\begin{array}{r} 1825 \\ 23 \\ \hline 30 \end{array}$$

$$\begin{array}{r} 178.6 \\ 62 \\ \hline 26 \end{array}$$

$$\begin{array}{r} 178.6 \\ 62 \\ \hline 26 \end{array}$$

$$\begin{array}{r} 22.8 \\ 90 \\ \hline 18 \end{array}$$

$$\begin{array}{r} 179.1 \\ 57 \\ \hline 14 \end{array}$$

$$\begin{array}{r} 179.5 \\ 53 \\ \hline 12 \end{array}$$

$$\begin{array}{r} 179.8 \\ 50 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 179.8 \\ 53 \\ \hline 14 \end{array}$$

$$\begin{array}{r} 179.3 \\ 53 \\ \hline 18 \end{array}$$

$$\begin{array}{r} 178.8 \\ 60 \\ \hline 18 \end{array}$$

$$\begin{array}{r} 181.8 \\ 30 \\ \hline 22 \end{array}$$

$$\begin{array}{r} 182.1 \\ 27 \\ \hline 25 \end{array}$$

$$\begin{array}{r} 182.3 \\ 25 \\ \hline 31 \end{array}$$

178.3	178.6	177.2	178.6	179.1	179.4	179.5	179.0	178.3	178.0	178.6	178.8
63	72	76	62	57	54	53	56	65	38	3.2	3.0
27	21	19	14	12	52	12	14	18	22	25	31

$$\begin{array}{r}
 76.0 \\
 9.8 \\
 30 \\
 \hline
 177.7
 \end{array}
 +
 \begin{array}{r}
 16.4 \\
 26.5 \\
 20 \\
 \hline
 62.9
 \end{array}
 +
 \begin{array}{r}
 26.3 \\
 8.5 \\
 18 \\
 \hline
 71.1
 \end{array}
 +
 \begin{array}{r}
 72.7 \\
 68 \\
 12 \\
 \hline
 152.7
 \end{array}
 +
 \begin{array}{r}
 18.0 \\
 6.3 \\
 61 \\
 \hline
 82.3
 \end{array}
 +
 \begin{array}{r}
 52.8 \\
 7.0 \\
 14 \\
 \hline
 75.8
 \end{array}
 +
 \begin{array}{r}
 17.8 \\
 4.4 \\
 18 \\
 \hline
 30.0
 \end{array}
 +
 \begin{array}{r}
 18.4 \\
 4.2 \\
 22 \\
 \hline
 24.6
 \end{array}
 +
 \begin{array}{r}
 18.6 \\
 5.7 \\
 53 \\
 \hline
 29.3
 \end{array}
 +
 \begin{array}{r}
 0.4 \\
 0.7 \\
 0.7 \\
 \hline
 1.8
 \end{array}$$

174.9	176.3	176.6	175.8	177.4	177.7	178.3	178.1	177.3	177.3	178.7	180.1	180.2	180.7
18	6.4	6.1	6.9	5.3	5.8	4.4	4.6	5.2	5.2	4.0	2.6	2.5	2.0
30	21	24	18	14	12	14	12	14	16	21	23	27	32

W.C. Brand horse Gravel Pit
and Rt of Way to same.

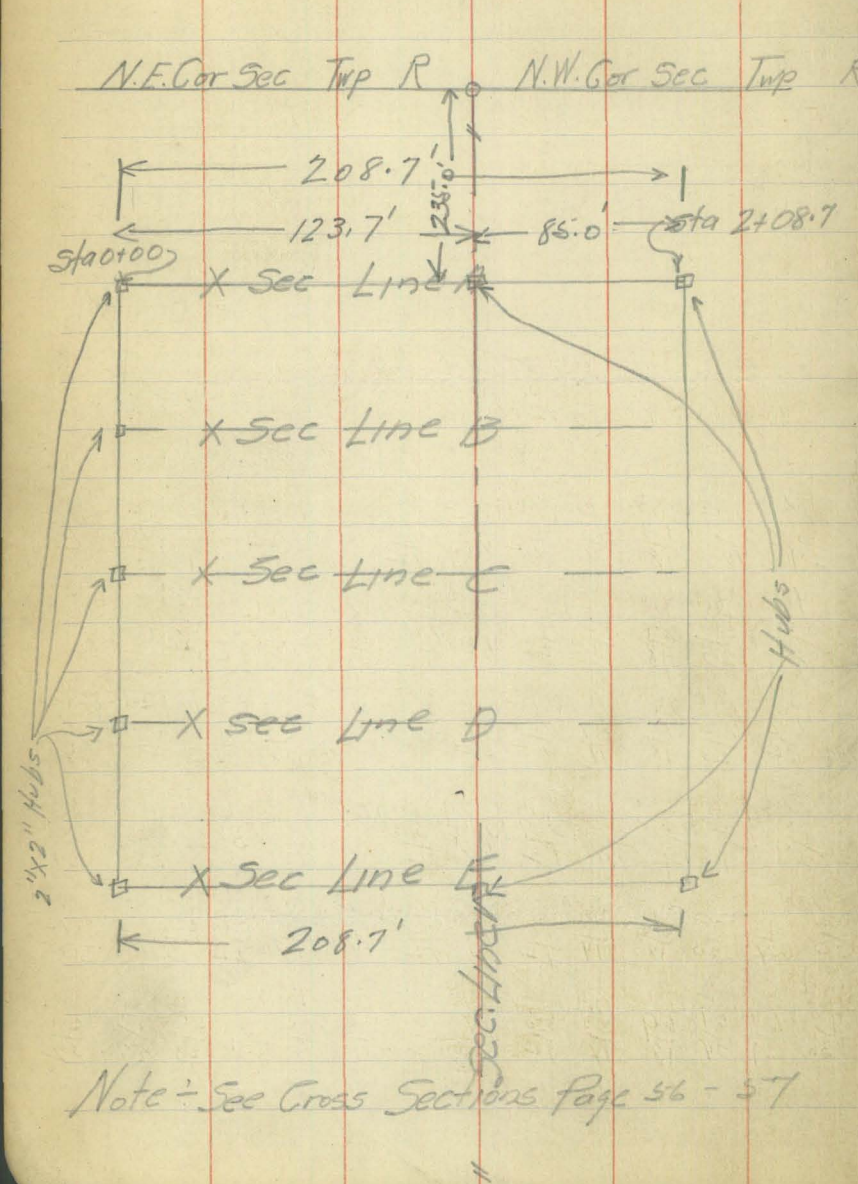
Secs 28+29 Twp 88 Rng 14

NE. Cor Sec 29

NW cor Sec 28

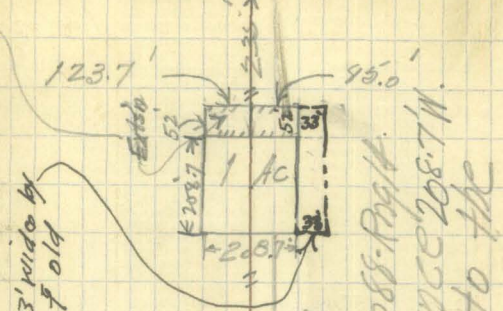
7/12/22
055

Hoff
Made
Francis



Note: On May 11th Miller, LeFevre & Decker & Johnston arranged for purchase of extension to original pit. bore at tract 52' wide by 209' in width comprising 14¹/₂ acres situated at 125.000.

No to: On Aug. 9-1927 - purchased astrip 33' wide by 266.7' in length abutting east side of old Grave! pr. consideration = 225.00



Section Line 2017 cut 1903
Right of Way to pit 2 Rods Wide

Description: Beginning at a point
235' S of the NE cor. of Sec. 29-Twp.
thence S5°E, thence 208.7' S-thence
thence 208.7' N, thence 123.7'E to
point of Beginning - 1 Acre.

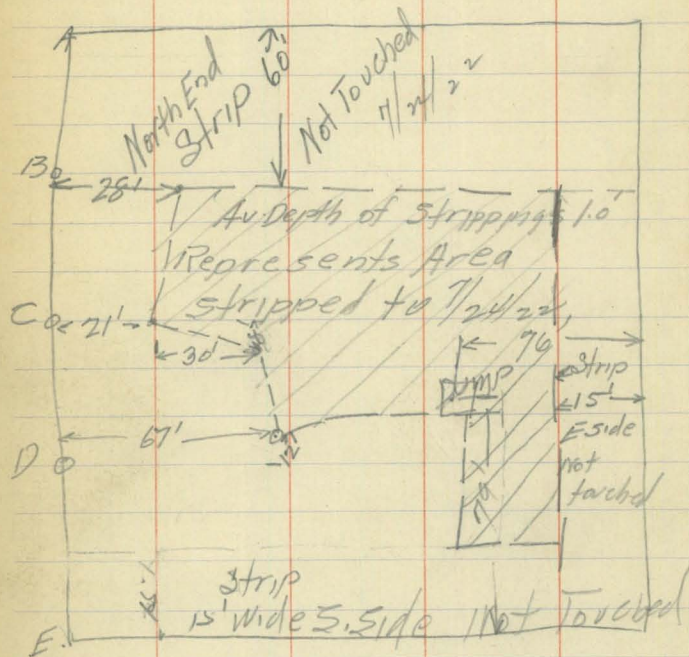
lease duration 10 yrs from date - Consideration \$
17. of way 2 Rods with W. line sec 28 from S. line of
Pit to Highway South.

Highway

Notes on Stripping - Brand horse wit 7/24/22

76
79

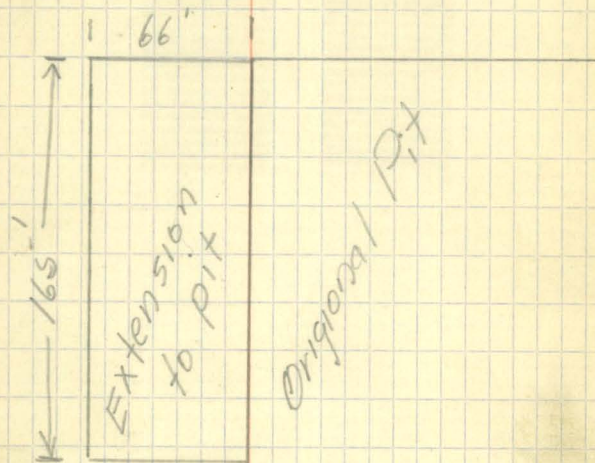
057



Extension to 1st W. C. Brandhars
Gravel Pit.

Sec 28 Twp 88 Rng 14

058
7/12/22
Hott
Wade
Francis



Description: Beginning at the N.W. Cor
of original pit, thence 66' W. thence
165' S. thence 66' E. thence 165' N. to
point of beginning - $\frac{1}{4}$ of 1 Acre.

Sept. 22, 1922

Staked 15" x 36' pipe Culv. at
Lichty Cor. Hudson to Eagle Center to
Spencer.

Truck Body Dimensions

Chaney's Trucks Hauling Gravel

on Hudson Eagle Center Road

Truck No	Make	Driver	Length	Width	Ht
5	Ford		6'-0"	3'-0"	1'-6" - Flange
1	"		6'-0	3.0	1'-6"

6" Board Front + Sides Top 3.6' Load Level

Note: Dist from Brand horse Pit to Wm Str Cor = End of Gravel pit = 4.9 Mi - Miller's Car.

Milage Schedule - Gravel Haul Hudson Eagle Center Road from Brand Horse Pit

Sta to Sta Miles Haul

0+00-23+67

8

23+67-50+27

7 $\frac{1}{2}$

50+27-76+67

7

76+67-103+07

6 $\frac{1}{2}$

103+07-129+47

6

129+47-155+87

5 $\frac{1}{2}$

155+87 161+15 End

5

16 s) 165.0 10.

Tile Check South

065

Used spade 1.62' on tile top

BM 0 9.91 172.01 162.10

~~0.10~~

1 11.63
2 10.36
3 7.70
4 5.07
5 2.65'

T.P 12.08 183.37 072 171.29

6 11.32
7 8.75
8 7.19
9 6.83
10 6.48

T.P 6.08 184.23 5.22 178.15

11 7.02
12 6.68
13 6.32
14
15
16

Tite CK
North

BM 0	9.91	172.01	162.10
0+50		12.05	
1		11.80	
2		10.28	
3		7.70	
4		5.05	
5		2.46	
T.P.	12.08	183.37	0.72 171.29
6		11.25	
7		8.73	
8		7.22	
9		6.86	
10		6.48	
T.P.	6.08	184.23	5.22 178.15
11		6.98	
12		1.52	
13		6.22	
14			
15			
16			

Tile Stakes
S Side

(82.87)

10 + 50	5.3		4.80	178.07	174.90	3.17
11	5.2		4.64	178.13	175.08	3.05
+ 50	5.2		4.65	178.22	175.26	2.96
12	4.9		4.36	178.51	175.41	3.07
+ 50	4.5		3.69	179.18	175.72	3.46
	7.25	(86.43)				
13	7.3		6.86	179.57	175.80	3.77
+ 50	7.0		6.35	180.08	175.98	4.10
14	6.5		6.06	180.37	176.16	4.21
+ 50	6.1		5.45	180.98	176.93	4.05
15	5.4		4.84	181.59	177.70	3.89
+ 50	4.7		3.93	182.50	178.85	3.65
16	3.9		3.12	183.31	180.00	3.31
		(94.02)				
+ 50	10.4		9.87	184.15	181.15	3.00
17	8.8		8.18	185.84	182.30	3.54
+ 50	7.0		6.42	187.60	183.45	4.15
18	5.6		4.83	189.19	184.60	4.59
+ 50	4.2		3.62	190.40	185.75	4.65
19	3.8		3.15	190.87	186.90	3.97

0.36

1.5210

2.30

3.67

3.82

4.01

No Overcut

(182.87)

10+50	5.3		4.69	175.18	174.90	3.28		
11	5.0		4.20	178.67	175.08	3.69		
+50	5.1		4.23	178.64	175.26	3.38	do	
12	4.5		3.65	179.22	175.44	3.78	N	
+50	4.2		3.34	179.53	175.62	3.91	30	
13	7.0	(186.43)	6.29	180.14	175.80	4.34	0	
+50	6.7	179.73	6.19	180.24	175.98	4.26		3.75
14	6.2	180.23	5.53	180.90	176.16	4.74		4.07
+50	5.8	180.63	5.10	181.33	176.93	4.40	154	3.70
15	5.2		4.43	182.00	177.80	4.20		
+50	4.4		3.69	182.74	178.85	3.89		
16	3.5		2.66	183.74	180.00	3.77		
+50	10.25	(194.02)	9.45	184.57	181.15	3.42	2.30%	
17	9.0		8.32	185.70	182.30	3.40		
+50	7.5		6.57	187.45	183.45	4.00		
18	5.5	188.52	4.70	189.32	184.60	4.72		3.92
+50	4.0	190.02	3.35	190.67	185.75	4.92		1.00
19	3.2	190.82	2.49	191.53	186.90	4.63		4.27
+50	5.39	(196.92)	5.29	191.63	187.10	4.53		1.00
20	6.1	190.82	5.33	191.59	187.50	4.09		3.92
+50	6.2	190.72	5.32	191.60	187.80	3.80		
21	5.9	191.02	5.20	191.72	188.10	3.62		
+50	5.7	191.22	4.97	191.95	188.40	3.55		
22	4.8	192.12	4.32	192.60	188.70	3.90		
+50	3.6	193.32	2.93	193.99	189.00	4.99		3.42
23	2.5	194.42	1.83	195.09	189.30	5.79		4.32
+50	2.5	194.42	1.64	195.28	189.60	5.68		5.12
24	3.2	193.72	2.51	194.41	189.90	4.51		4.82
								3.82

1.700
1.000
3.000

Title Check Eagle Center - Hudson Road

070
6/1/22

BM 5.05

Readings on tile top and spade length 1.75'

131+50	6.40
132	6.00
133	5.40
134	3.30
T.D. 9.23	1.40
135	8.96
136	6.83
137	5.40
138	4.02
139	

North side

131+50	6.45
132	6.05
133	5.40
134	3.40
T.D. 9.23	1.40
135	9.00
136	6.85
137	5.45
138	4.02
139	
140	

T. 168 N
S Side

8.23 215.09

206.86

138	8.33
139	6.84
140	4.87
141	2.95
T.P	6.94
142	7.50
143	5.24
144	3.68

Hub Sta 137

Used Spade Length 1.77 on Tile top

N. Side

Hub Sta 137 8.23 215.09

206.86

138	8.33
139	6.85
140	4.97
141	3.05
T.P	6.94
142	7.40
143	5.52
144	3.70

Used Tilespace L 150'

Top E piling

BM.	2.24	182.48		180.24
113+50			4.52	
114			4.20	
115			3.33	
116			2.44	
117			1.02	181.46
T.D.	11.25	(192.00)	1.73	180.75
118			5.49	330.20
119			2.30	
T.D.	10.89	(202.49)	0.40	191.60
120			9.55	
121			8.41	
122			7.46	
123	6.82		6.78	
124			6.82	
125			7.30	
126			7.93	
T.D.	5.14	(221.48)	6.15	196.34
127			7.52	
128			8.15	
129+10			8.76	

BM	2.24		Bo. 24
113150			4.58
114			4.15
115			3.34
116			
117		(192.00)	
118			5.44
119			2.26
T.P.	16.89	(202.49)	040 191.60
120			9.53
121			
122			7.49
123			7.00
124			6.87
125			7.22
126			7.69
T.P.	5.14	201.48	6.15 196.34
127			7.05
128			7.36
129 410			7.75
130			

Tile CR
S Side

074

B17	3.20	183.44	180.74
111			680
110			620
109			557
108			505
107			440
106			232
TP	11.00	193.94	0.50 (182.94)
105			1065
104			866

Used Tile Spade Length 1.55
Top E piling Sta 112 - N. Side Rd

N. Side

Used Tile Spade $L=1.55$

0.5

BM	3.20	183.44		180.24
111			6.83	
110			6.20	
109			5.53	
108			4.98	
107			4.40	
106			2.30	
T.P	11.00	193.94	0.60	192.94
105			10.68	
104			8.60	
103			6.41	
102			4.27	
101			2.27	
T.P	13.20	207.02	0.12	193.82
100			13.10	
99			10.67	
98			8.30	
97			5.93	
96			3.53	
95			0.96	

Tile CK
N side

Spade L = 1.55
~~Spade~~
S side

076

BM 3.65 20674 203.09

70 764

71 716

72 650

73 630

74 602

75 5.75

T.P 9.16 21205 3.85 20.89

76 972

77 847

78 603

79 368

80 1.22

T.P 9.24 212091 0.38 21.67

81 842

82 797

83 758

84 726

85 688

86 642

5. Side

B.M.	3.65	206.74	203.09
Tile top		9.88	
70		7.78	
71		7.12	
72		6.60	
73		6.32	
74		6.02	
75		5.50	

T.P. 9.16 21205 3.85 202.89

76 9.74

77 8.46

78 6.08

79 3.66

80 1.24

T.P. 9.24 220.91 0.38 211.67

81 8.42

82 ~~7.97~~ 8.03

83 7.62

84 7.27

85 6.85

86 6.42

Used spade - Length 1.55 077

At Inct. Lichtys private file as relaid

Tile Chk - South
Glad br Gm

Spade L 1.55

078

BM 9.11 230.16 221.05
 $\frac{2.15}{228.01}$ $\frac{1.55}{215}$

160+85	11.02	216.99	217.13
160+50	10.87	217.14	217.20
160	10.45	217.56	217.30
159+50			
159	9.08	218.93	218.60
158+50	8.52	219.49	219.50
158	7.62	220.39	220.40
157+50	6.68	221.33	221.30
157	5.52	222.49	222.70
156+50	4.50	223.51	223.10
156	3.45	224.56	224.00

North

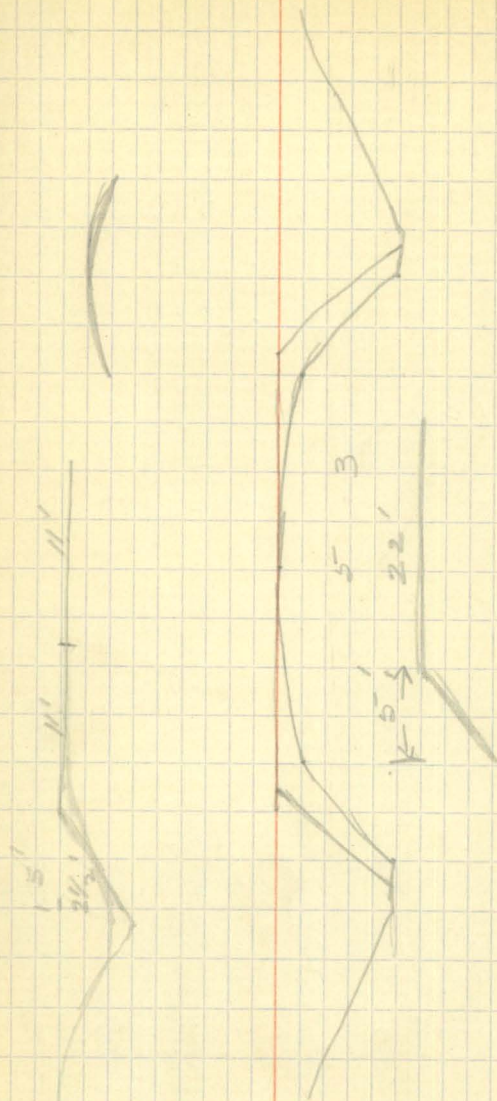
079

B.M. 4.17

48	7.60
49	7.02
50	6.72
51	6.30
52	5.90

B.M. 5.60

47	8.28
46	7.58
	6.88



South

BM 4.17

199.08

48 8.08
49 7.20
50 6.78
51 6.40
52 5.90

BM 5.60 204.68

199.08

47+50 9.12
47 8.76
46 7.54
45+90 level bottom 8.90
Hub 45 4.48 200.20

6
3
18
27

8.3
5.5
16.5
8.25

9.2
2.2
3

8" DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

ROADWAY 14 FEET WIDE. SIDE SLOPES 1 1/2 TO 1.

FOR SINGLE TRACK EMBANKMENT.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	7.0	7.2	7.3	7.5	7.6	7.8	7.9	8.1	8.2	8.4	0
1	8.5	8.7	8.8	9.0	9.1	9.3	9.4	9.6	9.7	9.9	1
2	10.0	10.2	10.3	10.5	10.6	10.8	10.9	11.1	11.2	11.4	2
3	11.5	11.7	11.8	12.0	12.1	12.3	12.4	12.6	12.7	12.9	3
4	13.0	13.2	13.3	13.5	13.6	13.8	13.9	14.1	14.2	14.4	4
5	14.5	14.7	14.8	15.0	15.1	15.3	15.4	15.6	15.7	15.9	5
6	16.0	16.2	16.3	16.5	16.6	16.8	16.9	17.1	17.2	17.4	6
7	17.5	17.7	17.8	18.0	18.1	18.3	18.4	18.6	18.7	18.9	7
8	19.0	19.2	19.3	19.5	19.6	19.8	19.9	20.1	20.2	20.4	8
9	20.5	20.7	20.8	21.0	21.1	21.3	21.4	21.6	21.7	21.9	9
10	22.0	22.2	22.3	22.5	22.6	22.8	22.9	23.1	23.2	23.4	10
11	23.5	23.7	23.8	24.0	24.1	24.3	24.4	24.6	24.7	24.9	11
12	25.0	25.2	25.3	25.5	25.6	25.8	25.9	26.1	26.2	26.4	12
13	26.5	26.7	26.8	27.0	27.1	27.3	27.4	27.6	27.7	27.9	13
14	28.0	28.2	28.3	28.5	28.6	28.8	28.9	29.1	29.2	29.4	14
15	29.5	29.7	29.8	30.0	30.1	30.3	30.4	30.6	30.7	30.9	15
16	31.0	31.2	31.3	31.5	31.6	31.8	31.9	32.1	32.2	32.4	16
17	32.5	32.7	32.8	33.0	33.1	33.3	33.4	33.6	33.7	33.9	17
18	34.0	34.2	34.3	34.5	34.6	34.8	34.9	35.1	35.2	35.4	18
19	35.5	35.7	35.8	36.0	36.1	36.3	36.4	36.6	36.7	36.9	19
20	37.0	37.2	37.3	37.5	37.6	37.8	37.9	38.1	38.2	38.4	20
21	38.5	38.7	38.8	39.0	39.1	39.3	39.4	39.6	39.7	39.9	21
22	40.0	40.2	40.3	40.5	40.6	40.8	40.9	41.1	41.2	41.4	22
23	41.5	41.7	41.8	42.0	42.1	42.3	42.4	42.6	42.7	42.9	23
24	43.0	43.2	43.3	43.5	43.6	43.8	43.9	44.1	44.2	44.4	24
25	44.5	44.7	44.8	45.0	45.1	45.3	45.4	45.6	45.7	45.9	25
26	46.0	46.2	46.3	46.5	46.6	46.8	46.9	47.1	47.2	47.4	26
27	47.5	47.7	47.8	48.0	48.1	48.3	48.4	48.6	48.7	48.9	27
28	49.0	49.2	49.3	49.5	49.6	49.8	49.9	50.1	50.2	50.4	28
29	50.5	50.7	50.8	51.0	51.1	51.3	51.4	51.6	51.7	51.9	29
30	52.0	52.2	52.3	52.5	52.6	52.8	52.9	53.1	53.2	53.4	30
31	53.5	53.7	53.8	54.0	54.1	54.3	54.4	54.6	54.7	54.9	31
32	55.0	55.2	55.3	55.5	55.6	55.8	55.9	56.1	56.2	56.4	32
33	56.5	56.7	56.8	57.0	57.1	57.3	57.4	57.6	57.7	57.9	33
34	58.0	58.2	58.3	58.5	58.6	58.8	58.9	59.1	59.2	59.4	34
35	59.5	59.7	59.8	60.0	60.1	60.3	60.4	60.6	60.7	60.9	35
36	61.0	61.2	61.3	61.5	61.6	61.8	61.9	62.1	62.2	62.4	36

Calculated by Julien A. Hall, M. Am. Soc. C. E.

MADE IN GERMANY.

19770
 3.14
 19456
 194
 19755
 106.80
 42
 673
 3.78
 195.28
 6.48
 191.50
 Rt 19770 2700 6 630 188.78 188.80
 Lt 19770 2700 6 6.11 189.17 188.80
 BM 5-95 186.22 180.27
 186.22 186.22 186.22 186.22 186.22 186.22
 180.00 180.19 181.24 181.64
 6.22 6.03 4.48 1.58
 T.P. 1308 186.22 1.60 184.62
 197.70 197.70 197.70 197.70 645 196.25
 187.73 190.52 193.91 196.23
 9.87 6.48 3.99 1.47
 6.05 202.30 202.30
 46.0
 197.70
 200.30 202.30 202.30
 197.00 197.00
 530 530

2723 85 85 85 36 1.8 5 68
 21470 21470 21470 21470 080 2075
 205.30 207.80 205.80 208.90 39.30
 9.40 6.90 8.90 5.50 7.4
 3.7 6.1 6.5 7.2 43
 2.50 17 9 62 26.78 72 43 29
 21470 21470 21470 21470 21470
 200.30 207.80 205.80 208.90 207.50
 4.40 4.50 6.7 6.5 1.8
 4.50 4.50 2.2 2.3 2.4
 21470 21470 21470 21470
 207.00 210.20 207.50 210.00
 7.70 4.50 7.20 4.20
 3.91 3.3 6.0
 3.9 2.1
 214.70 214.70
 208.00 212.80
 6.70 3.90
 3 1.9
 214.70 214.70
 200.23 204.71
 8.91
 195.80